



# **Application for resource consent or fast-track resource consent**

(Or Associated Consent Pursuant to the Resource Management Act 1991 (RMA)) (If applying for a Resource Consent pursuant to Section 87AAC or 88 of the RMA, this form can be used to satisfy the requirements of <u>Form 9</u>). Prior to, and during, completion of this application form, please refer to <u>Resource Consent Guidance Notes</u> and <u>Schedule of Fees and Charges</u> — both available on the Council's web page.

1. Pre-Lodgement Meeting			
Have you met with a council Re  Yes No	source Covnsent representative to discuss this application prior to lodgement?		
2. Type of consent being	gapplied for		
(more than one circle can be ticked):			
<b>✓</b> Land Use	O Discharge		
Fast Track Land Use*	Change of Consent Notice (s.221(3))		
<b>⊘</b> Subdivision	Extension of time (s.125)		
Consent under National El (e.g. Assessing and Managin			
Other (please specify) _			
*The fast track is for simple la	nd use consents and is restricted to consents with a controlled activity status.		
3. Would you like to opt	out of the fast track process?		
○Yes <b>⊘</b> No			
4. Consultation			
Have you consulted with lwi/Ha	ipū? <b>Yes No</b>		
If yes, which groups have you consulted with?			
Who else have you consulted with?			
For any questions or informati District Council, <u>tehonosuppor</u>	on regarding iwi/hapū consultation, please contact Te Hono at Far North		

5. Applicant details		
Name/s:	Far North Housing Limited	
Email:		
Phone number:		
Postal address: (or alternative method of service under section 352 of the act)		
Have you been the subject under the Resource Manag	of abatement notices, enforcement orders, infringement notices and/or convictions gement Act 1991? Yes V No	
If yes, please provide detail	S.	
6. Address for corres		
Name and address for service a	nd correspondence (if using an Agent write their details here)	
Name/s:	Steven Sanson - Sanson & Associates Limited	
Email:		
Phone number:  Postal address: (or alternative method of service under section 352 of the act)		
All correspondence will be sent by email in the first instance. Please advise us if you would prefer an alternative means of communication.		
Yes - please send all corres	pondence to myself and Adrian Tonks	
7. Details of property	y owner/s and occupier/s	
Name and Address of the owner please list on a separate sheet ij	r/occupiers of the land to which this application relates (where there are multiple owners or occupiers f required)	
Name/s:	Far North Holdings Limited	
Property address/ location:	84 Gillies Street, Kawakawa [Old Whangae Road]	
	Postcode	

8. Application site details				
Location and/or property street address of the proposed activity:				
Name/s:	Far North Holdings Limited			
Site address/ location:	84 Gillies Road [Old Whangae Road]			
	Postcode			
Legal description:	Lot 92, 98 Deeds Plan W 46 Val Number:			
Certificate of title:	NA523/225			
	tach a copy of your Certificate of Title to the application, along with relevant consent nts and encumbrances (search copy must be less than 6 months old)			
Site visit requirement	es:			
Is there a locked gate o	r security system restricting access by Council staff? <b>Yes  No</b>			
Is there a dog on the pr	roperty? Yes No			
•	of any other entry restrictions that Council staff should be aware of, e.g. health and safety, is important to avoid a wasted trip and having to re-arrange a second visit.			
Please contact applican	nt and agent prior to site visit.			
9. Description of t	the proposal			
	scription of the proposal here. Please refer to Chapter 4 of the <i>District Plan, and Guidance</i> s of information requirements.			
Combined land use and	d subdivision consent for a housing project comprising 30 residential units.			
If this is an application for a Change or Cancellation of Consent Notice conditions (s.221(3)), please quote relevant existing Resource Consents and Consent Notice identifiers and provide details of the change(s), with reasons for requesting them.				
10. Would you like to request public notification?				
○ Yes  No				
	required/being applied for under different legislation			
(more than one circle can be				
Building Consent Enter BC ref # here (if known)				
Regional Council Consent (ref # if known)  Ref # here (if known)  National Environmental Standard Consent Consent bore (if known)				
National Environmental Standard Consent   Consent here (if known)				
Other (please specify) Specify 'other' here				

12. National Environmental Standard for Assessing and Managing Contaminants in Soil to Protect Human Health:				
The site and proposal may be subject to the above NES. In order to determine whether regard needs to be had to the NES please answer the following:				
Is the piece of land currently being used or has it historically ever been used for an activity or industry on the Hazardous Industries and Activities List (HAIL)? Yes No Don't know				
Is the proposed activity an activity covered by the NES? Please tick if any of the following apply to your proposal, as the NESCS may apply as a result? <b>Yes No Don't know</b>				
<b>⊘</b> Subdividing land				
Changing the use of a pi	iece of land	Removing or replacing a fuel storage system		
13. Assessment of env	vironmental effects:			
Every application for resource consent must be accompanied by an Assessment of Environmental Effects (AEE). This is a requirement of Schedule 4 of the Resource Management Act 1991 and an application can be rejected if an adequate AEE is not provided. The information in an AEE must be specified in sufficient detail to satisfy the purpose for which it is required. Your AEE may include additional information such as written approvals from adjoining property owners, or affected parties.				
Your AEE is attached to this	application 🗹 Yes			
44 Dyaft conditions				
14. Draft conditions:				
Do you wish to see the draft conditions prior to the release of the resource consent decision? <b>Yes No</b>				
enable consideration for the	•	nded for 5 working days as per s107G of the RMA to		
15. Billing Details:				
		e for paying any invoices or receiving any refunds also refer to Council's Fees and Charges Schedule.		
Name/s: (please write in full)	Far North Housing Limited			
Email:				
Phone number:				
Postal address: (or alternative method of service under section 352 of the act)				
Fees Information  An instalment fee for processing this application is payable at the time of lodgement and must accompany your application in order for it to be lodged. Please note that if the instalment fee is insufficient to cover the actual and reasonable costs of work undertaken to process the application you will be required to pay any additional costs. Invoiced amounts are payable by the 20th of the month following invoice date. You may also be required to make additional payments if your application requires notification.				

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#### 15. Billing details continued...

#### **Declaration concerning Payment of Fees**

I/we understand that the Council may charge me/us for all costs actually and reasonably incurred in processing this application. Subject to my/our rights under Sections 357B and 358 of the RMA, to object to any costs, I/we undertake to pay all and future processing costs incurred by the Council. Without limiting the Far North District Council's legal rights if any steps (including the use of debt collection agencies) are necessary to recover unpaid processing costs I/we agree to pay all costs of recovering those processing costs. If this application is made on behalf of a trust (private or family), a society (incorporated or unincorporated) or a company in signing this application I/we are binding the trust, society or company to pay all the above costs and guaranteeing to pay all the above costs in my/our personal capacity.

Name: (please write in full)	Adrian Tonks	
Signature:	Albe	Date 05-Dec-0202
(signature of bill payer)		MANDATORY

#### 16. Important Information:

#### Note to applicant

You must include all information required by this form. The information must be specified in sufficient detail to satisfy the purpose for which it is required.

You may apply for 2 or more resource consents that are needed for the same activity on the same form.

You must pay the charge payable to the consent authority for the resource consent application under the Resource Management Act 1991.

#### Fast-track application

Under the fast-track resource consent process, notice of the decision must be given within 10 working days after the date the application was first lodged with the authority, unless the applicant opts out of that process at the time of lodgement.

A fast-track application may cease to be a fast-track application under section 87AAC(2) of the RMA.

#### **Privacy Information:**

Once this application is lodged with the Council it becomes public information. Please advise Council if there is sensitive information in the proposal. The information you have provided on this form is required so that your application for consent pursuant to the Resource Management Act 1991 can be processed under that Act. The information will be stored on a public register and held by the Far North District Council. The details of your application may also be made available to the public on the Council's website, www.fndc.govt.nz. These details are collected to inform the general public and community groups about all consents which have been issued through the Far North District Council.

17. Declaration			
The information I have sup	oplied with this applic	ation is true and complete to the l	est of my knowledge.
Name (please write in full)	Adrian Tonks	Adrian Tonks	
Signature			Date 05-Dec-2025
		lication is made by electronic me	ans

Checklist
Please tick if information is provided
Payment (cheques payable to Far North District Council)
A current Certificate of Title (Search Copy not more than 6 months old)
Oetails of your consultation with lwi and hapū
Ocopies of any listed encumbrances, easements and/or consent notices relevant to the application
Applicant / Agent / Property Owner / Bill Payer details provided
Cocation of property and description of proposal
Assessment of Environmental Effects
Written Approvals / correspondence from consulted parties
Reports from technical experts (if required)
Copies of other relevant consents associated with this application
O Location and Site plans (land use) AND/OR
O Location and Scheme Plan (subdivision)
C Elevations / Floor plans
O Topographical / contour plans
Please refer to Chapter 4 of the District Plan for details of the information that must be provided with an application. Please also refer to the RC Checklist available on the Council's website. This contains more helpful hints as to what information needs to be shown on plans.



#### **SANSON & ASSOCIATES LTD**

Planners & Resource Consent Specialists



## **Assessment of Environmental Effects**

#### **Application for Resource Consent:**

A Combined Multi-Unit Development and Subdivision of Lot 92, 98 Deeds Plan W46, Kawakawa

Prepared for: Far North Housing Limited

By: Steven Sanson | Consultant Planner
Reviewed: Andrew McPhee | Consultant Planner

Date: December 2025

## 1.0 APPLICANT & PROPERTY DETAILS

Applicant	Far North Housing Limited	
Address for Service	Sanson & Associates Limited	
	PO Box 318	
	PAIHIA 0247	
	C/O - Steven Sanson	
	steve@sansons.co.nz	
	021-160-6035	
Legal Description	Lot 92, 98 Deeds Plan W 46	
Record Of Title	NA523/225	
Physical Address	84 Gillies Street, Kawakawa	
Site Area	7,588m² [Topo Confirmed]	
Owner of the Site	Far North Holdings Limited	
District Plan Zone	Commercial / Rural Production in the operative Far	
	North District Plan [ODP]	
	Mixed Use Zone in the Proposed Far North District Plan [PDP]	
District Plan Features	Pedestrian Frontage ; Historic Site 61 – Star Hotel	
Archaeology	Nil	
NRC RPS Overlays	River Flooding	
Soils	Class 4 / Town	
Protected Natural Area	Nil	
HAIL	Grassland / Built Up Area	
Wetlands	Nil (According to NRC Biodiversity Wetlands Maps)	

## 2.0 SUMMARY OF PROPOSAL

Proposal	The proposal is for a Resource Consent to construct a medium-density, multi-residential development at Old Whangae Road, including 30 residential units [18 x 1-bed and 12 x 2-bed] designed as six, two-storey blocks, with 35 car parks and open space.  The proposal also includes an associated subdivision.	
Reason for Application	Consent is required for the following activities in the OD and PDP.  8.6.5.1.1 Residential Intensity 8.6.5.1.2 Sunlight 8.6.5.1.3 Stormwater Management 8.6.5.1.4 Setback from Boundaries 8.6.5.1.5 Transportation 8.6.5.1.10 Building Coverage 12.3.6.1.1 Excavation / Filling in the Rural Production Zone 12.7.6.1.1 Setback from Rivers 13.7.2.1 Minimum Lot Sizes 14.6.1 Esplanade Areas 15.1.6A.2.1 Traffic Intensity 15.1.6B.1.1 Car Parking Spaces SUB-R14 Subdivision [PDP]	
Appendices	Appendix A – Record of Title & Instruments Appendix B – Architectural Drawings Appendix C – Scheme Plan Appendix D – Engineering Reports and Plans [Geotech, Three Waters, Civil Plans]. Appendix E – Consultation Appendix F – NRC Application [Provided on Request]	
Consultation	Refer Appendix E.	

#### 3.0 INTRODUCTION & PROPOSAL

#### 3.1 Report Requirements

This report has been prepared for Far North Housing Limited in support of a land use and subdivision consent application at Old Whangae Road, Kawakawa.

Section 88 of the Resource Management Act 1991 [RMA] requires that every resource consent application shall be made in the prescribed form and manner and includes the information relating to the activity, including an assessment of the activity's effects on the environment, as required by Schedule 4.

Schedule 4 of the RMA outlines the matters which must be included within an application for resource consent, including:

- a) a description of the activity:
- b) a description of the site at which the activity is to occur:
- c) the full name and address of each owner or occupier of the site:
- d) a description of any other activities that are part of the proposal to which the application relates:
- e) a description of any other resource consents required for the proposal to which the application relates:
- f) an assessment of the activity against the matters set out in Part 2:
- g) an assessment of the activity against any relevant provisions of a document referred to in section 104(1)(b).

Schedule 4 also defines additional matters to be included in an application for subdivision consent and the matters to be considered when preparing an assessment of effects on the environment.

These statutory requirements are addressed in the application.

#### 3.2 Description of Proposal

The proposal is for 30 residential units [ $18 \times 1$ -bed and  $12 \times 2$ -bed] designed as six, two-storey blocks, with 35 car parks and open space.

Footpaths and internal access are provided to Old Whangae Road, with the footpath extending across adjoining sites connecting to the wider surrounds.

Part of the site adjoins State Highway 1 where the Star Hotel is located across this frontage.

Part of the Twin Coast Cycle Trail connects through the site Old Whangae Road.

As announced by FNDC in November 2022, Kawakawa has been allocated \$25.6 million specifically for road extensions and significant water infrastructure upgrades to enable approximately 300 new homes. This proposal serves as a key component of that planned growth, utilizing the capacity enabled by this confirmed government funding.

#### **Unit Configuration**

The unit breakdown for the development is as follows:

- Total Units 30
  - o One-Bedroom Units: 18 units [Block A, Block B, and Block E]
    - These are contained within three separate, two storey blocks containing six units each. Three units are located on the ground floor, and three units are located on the first floor per Block.
    - The units on the ground floor [Type A1] are proposed to be 57.5m² in size.
    - The first-floor units [Type A2] are proposed to be 60.5m².
  - o Two-Bedroom Units: 12 units [Block C, Block D, and Block F]

- These are contained within three separate, two storey blocks containing three, four and five units each. These units take up both the ground and first floor.
- The Type B2 units are proposed to be 43.5m² on the ground flood and 46.11m² on the first floor.



Figure 1 – Proposal Site Plan [Source: Eclipse Architecture]

The proposal also includes a stage subdivision of the sites involved as follows:

#### Stage 1:

Lot 1: 0.6055ha

Lot 3: 0.1655ha [0.1503ha Net].

#### Stage 2:

Lot 1: 0.3593ha [0.3104ha Net]

Lot 2: 0.2462ha

The subdivision rationale allows for the allotment containing the Star Hotel to be separated from the allotment where development is proposed via Stage 1.

Stage 2 further separates the development site into two lots to allow for the development to be owned by different entities. Easements are provided to facilitate this.

With respect to the subdivision of the sites this results in:

- Block A, Block B and Block C being located in Lot 1 of Stage 2. This includes 19 carparks, three of which are accessible and 8 x bike parks.
- Block D, Block E and Block F being located in Lot 2 of Stage 2. This includes 16 car parks, three of which are accessible, and 8 x bike parks. The rubbish collection area is located in this allotment.

It is understood that the general cadence of the development would be to undertake Stage 1 on the assumption that minimal physical works are required. The crossings for Lot 3 are proposed to be undertaken with the development in Stage 2.

Following completion of Stage 1, the land use development would take place across Lot 1 of Stage 1, and on completion of the land use development, the site would be subdivided in accordance with the Stage 2 scheme plan.



Figure 2 – Proposal Scheme Plan [Source: Survey Worx]

#### Site Earthworks & Retaining

The project requires earthworks over an area of 4,790m<sup>2</sup>. The planned earthworks volumes are:

• Cut: 0m<sup>3</sup>

Fill: 8.965m<sup>3</sup>

The volume of earthworks requires both FNDC and NRC consents. Various retaining walls are required with heights of 1.1m, 1.2m, 1.9m and 2m. An earth wall that is 2.5m in height is promoted around the boundary of the site.

To address the underlying alluvial soils and flood plain location, the proposal involves specific engineering methodologies:

- Foundation Construction of a geogrid-reinforced engineered gravel raft to mitigate differential settlement risks.
- Stormwater Installation of a 525mm diameter negative-grade pipe beneath the building platform to replicate pre-development overflow paths.
- Levels Raising the finished ground level to RL 6.75m to achieve freeboard above the 1% AEP flood level with 7.0m finished floor levels [FFL].

#### Access & Carparking

A new commercial double vehicle crossing will be constructed on Old Whangae Road to provide access to the development site. This will be provided in accordance with Council Engineering Standards.

Similarly, two new commercial double crossings are proposed to Lot 3 that contains the Star Hotel.

For the 30 units, 35 car parks are proposed to be provided, six of which are proposed to be accessible. 16 bike parks are provided across two separate areas.

A 1.8m footpath and kerbing is proposed from the development along Old Whangae Road to Gillies Street.

Various road marking is proposed to tie into the road arrangements along Whangae Road / Gillies Street.

#### **Impervious Surfaces**

The development site [i.e exclusive of Lot 3] has existing pavement areas of 1,100m<sup>2</sup>. The existing pervious area is 4,811m<sup>2</sup>.

This is proposed to be changed by having a roof area of 1,187m<sup>2</sup>, access of 1,172m<sup>2</sup>, path area of 510m<sup>2</sup> and pervious areas of 3,042m<sup>2</sup>. This results in 49% coverage of the site.

#### **Landscaping and Outdoor Amenity Areas**

The development incorporates both private and outdoor communal amenity areas, with significant landscaping proposed throughout the site.

- Each Type A1 dwelling has at least 20m² of private outdoor areas. Type A2 dwellings have a balcony and deck which is ~5.92m² in size.
- The Type B2 dwellings have dual outdoor areas with  $\sim$ 27m<sup>2</sup> provided outdoors on the ground floor.
- As above, the development contains up to 3,552m<sup>2</sup> of open space / landscaping overall. This includes considerable communal open space and internal footpaths which connect to the surrounds.

#### Infrastructure

In terms of water supply , the proposal involves extending the existing 50 mm diameter rider main along the eastern side of Old Whangae Road. Blocks A & B will connect to the new extended 50 mm rider main. Blocks C, D, E & F will connect to the existing 50 mm rider main on the western boundary.

Reports confirm the network has sufficient pressure to handle the development's peak hourly demand and meet firefighting requirements [to FW2] without compromising minimum service levels.

In terms of wastewater, a new private 150 mm PVC gravity network will be constructed within the site to service all residential blocks [A–F]. This internal network will discharge directly into the existing 300 mm concrete gravity main that runs through the southern portion of the site.

While there are no constraints at the connection point, known downstream capacity issues are currently being addressed by a separate Council upgrade project funded by the Infrastructure Acceleration Fund.

In terms of stormwater, a new stormwater network will collect runoff from all blocks and discharge it to the northern side of the existing diversion bank. A new 525mm diameter pipe will be installed beneath the building platform at a negative grade.

The pipe only takes stormwater in moderate to extreme flood events, i.e. rarely ever has any flow in it. It would work as an inverted syphon (i.e. two MH with a connection pipe between them) so that pipe fully drains between events. It also means the inlet is fully submerged before it starts flowing reducing the risk of blockages.

This is designed to replicate the pre-development overflow path, conveying floodwaters from the eastern unlined channel to a scruffy dome outlet west of Old Whangae Road. No onsite detention [attenuation] is required because the site is located at the bottom of the catchment.

#### **Supporting Documents**

The proposal is supported by numerous plans and reports.

**Appendix A** contains the Record of Title and Instruments for each site subject to development.

**Appendix B** contains the development plans for the proposal. This includes a site location plan, visuals, 3D overview, site plan, floor plans, elevations and sections.

**Appendix C** contains the proposed stage subdivision associated with the proposal including easements.

**Appendix D** includes a Geotechnical Report, a Three Waters Report which considers the flooding implications of the development and engineering plans.

**Appendix E** contains consultation with FNDC via CDM notes, Top Energy, Chorus and NZTA.

**Appendix F** can be provided on request which is an application to the Northland Regional Council for authorisations associated with earthworks and structures within the Wajomio Stream.

Activity Status: The proposal is a Non-Complying Activity.

#### 4.0 SITE & SURROUNDING ENVIRONMENT

#### 4.1 Zoning & Resource Features

The site is located Old Whangae Road, Kawakawa. The site is 7,588m<sup>2</sup> and is legally described as Lot 92, 98 Deeds Plan W 46. The site is limited to parcels, however a topo survey has been undertaken and confirms the site size and boundaries.

The property has a mixed zoning under the ODP, being Commercial and Rural Production. Under the PDP, the site is in the Mixed Use Zone.

The site is subject to a pedestrian frontage overlay and the Star Hotel located along the State Highway 1 frontage is considered to be a Historic Building [#61]. These features also apply under the PDP.



Figure 3 – Site Location [Source: Prover]



Figure 4 - FNDC Zone Map [Source: Far North Maps]

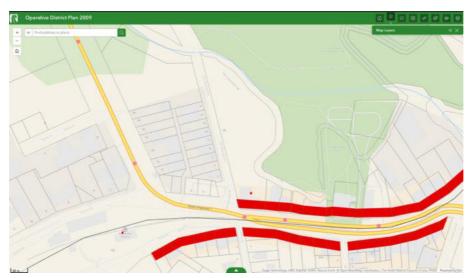


Figure 5 - FNDC ODP Features Map [Source: Far North Maps]



Figure 6 - FNDC PDP Zone & Features Map [Source: Far North Maps]

#### 4.2 Record of Title & Instruments

The Record of Title and relevant instruments are provided in <u>Appendix A</u>. These are not considered to be of concern to the proposed development.

#### 4.4 Topography & Natural Features

The site is reasonably flat and is located next to a stream and existing flowpaths. The site is subject to flooding as outlined by Far North District Council maps.

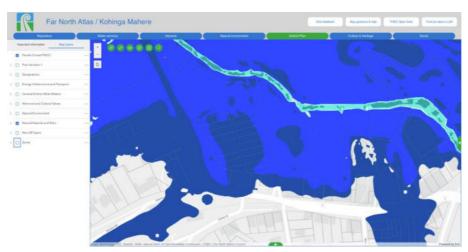


Figure 7 - Flooding [Source: Far North Maps]

#### 4.5 Built Form & Access

The area where developed is proposed has been recently cleared and subject to works associated with the Waiomio Stream. The site also contains the Star Hotel and associated car parking. The site has access from State Highway 1 and Old Whangae Road. The site has access to services as outlined below.

The land cover of the site has been pasture and built up settlement as per Figure 9.

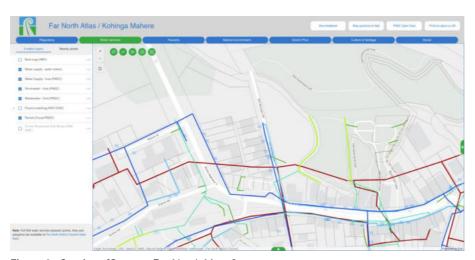


Figure 8 - Services [Source: Far North Maps]

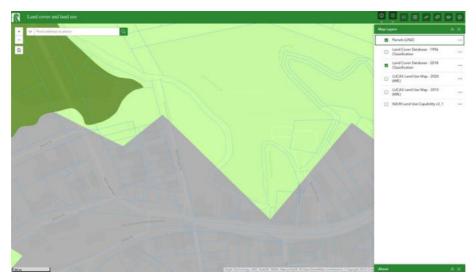


Figure 9 - Landcover [Source: Far North Maps]

#### 4.6 Surrounding Environment

The site is located in an area with a variety of uses that are established along the State Highway and along Old Whangae Road. Along the State Highway, this includes usual activities such as a liquor store, laundromats, grocers, NZ Post, food shops, gas stations and Te Hononga – Kawakawa Library. Along Old Whangae Road, this includes areas for parking, and light industrial activities such as panel beaters, engineering firms, and funeral services.

The variety of uses are commensurate with the Mixed Use zone proposed for the area and wider surrounds.

## 5.0 ASSESSMENT OF RELEVANT RULES

#### 5.1 Assessment

An assessment of the relevant rules of the ODP Plan is provided in the Tables below.

Note: An assessment of the Commercial Zone rules has not been undertaken as all development is located in the Rural Production Zone.

Table 1 - Rural Production Zone Rule Assessment

Rule	Assessment	Status
8.6.5.1.1 Residential Intensity	30 dwellings are well outside the permitted number of dwellings	Non-Complying
	allowed.	
8.6.5.1.2 Sunlight	It is likely that there are sunlight breaches along Old Whangae Road.	Restricted Discretionary
8.6.5.1.3 Stormwater Management	The proposal includes an additional 2,869m <sup>2</sup> of impervious surfaces. This results in 49% coverage.	Discretionary
8.6.5.1.4 Setback	Buildings are within 10m setbacks.	Restricted Discretionary
8.6.5.1.5 Transportation	Traffic Intensity breach for 30 dwellings [300 movements] which is above the 60 permitted.  Parking breach as current plan requires 2 per dwellings.  Access breaches as 30 dwellings requires a vested road standard.	Discretionary
8.6.5.1.6 Keeping of Animals	Not relevant	Complies
8.6.5.1.7 Noise	Residential type noise anticipated	Complies
8.6.5.1.8 Building Height	All buildings are less than 12m in height	Complies
8.6.5.1.9 Helicopter Landing Area	Not relevant	Complies
8.6.5.1.10 Building Coverage	The proposal contains 1,187m² of buildings. This results in 20.08% coverage.	Discretionary
8.6.5.1.11 Scale of Activities	Not relevant as residential use proposed.	Complies

8.6.5.1.12 Temporary	Not relevant	Complies
Events		

#### Table 2 - District Wide Matters

Rule	Assessment	Status
12.1 Landscapes & Natural Features	Not relevant.	Complies
12.2 Indigenous Flora & Fauna	Not relevant.	Complies
12.3 Soils & Minerals	The proposal includes more than 5,000m³ of works and retaining walls above 1.5m in height.	Discretionary.
12.4 Natural Hazards	Not relevant.	Complies
12.5 Heritage	The proposal does not seek to alter, undertake maintenance, remove or destroy the existing heritage building.	Complies
12.7 Lakes, Rivers and Wetlands	Development is within 30m of the Waiomio Stream	Discretionary
12.8 Hazardous Substances	Not relevant.	
12.9 Renewable Energy & Energy Efficiency	Not relevant.	Complies
13 Subdivision	The Commercial Zone subdivision of Lot 3 is Controlled. The Rural Production Zone	Non-Complying

	subdivision is Non- Complying.	
14 Financial Contributions	At this stage the proposal does not provide an esplanade reserve along the Waiomio Stream	Discretionary
15 Transportation	The proposal generates 300 traffic movements in the Rural Production Zone [Rule 15.1.6A.2.1].  35 car parks are provided whereas 60 car parks are required [Rule 15.1.6B.1.1].  The proposal should be accessed from a vested road due to servicing more than 8 household equivalents [Rule 15.1.6C.1.1].	Discretionary
16 Signs and Lighting	Not relevant	Complies
17 Designation	Not relevant.	Complies
18 Special Areas	Not relevant.	Complies
19 GMO's	Not relevant.	Complies

Overall, the proposal is a **Non Complying Activity**.

In terms of Regional Council matters, various consents are required, and resource consent is being sought concurrently. A copy of this application is available upon request.

Table 3 – PDP Rules with Legal Effect

Rule	Assessment
Hazardous Substances	Not relevant as no such substances proposed.
	Complies
Heritage Area Overlays	Not indicated on PDP.
	Complies
Historic Heritage	Rules HH-R1 to HH-R10 are not relevant as no
	works are proposed to the existing Star Hotel.
	Complies
Notable Trees	Not indicated on PDP.
	Committee
Sites and Areas of Significance	Complies  There are no activities prepased within the
Sites and Areas of Significance to Māori	There are no activities proposed within the SASM.
to Maori	SASIM.
	Complies
Ecosystems and Indigenous	Not relevant as no clearance proposed.
Biodiversity	Not rotovant as no otearanos proposea.
Activities on the Surface of	Not indicated on PDP.
Water	
	Complies
Earthworks	Proposed earthworks will be undertaken in
	accordance with the relevant standards
	including GD-05 and will have an ADP applied.
	Complies
Signs	Not indicated on PDP.
	Complies
Orongo Bay Zone	Not indicated on PDP.
	Complies
Subdivision	A Restricted Discretionary consent is required
	under the PDP in terms of SUB-R14 –

heritage resource.  Restricted Discretionary
Subdivision of a site that contains a scheduled

Resource consent is also required under the PDP.

This report provides a considered assessment of relevant NPS's and NES's and in summary, no further consents are required under these higher order documents.

### 6.0 NOTIFICATION ASSESSMENT

#### 6.1 Public Notification

The table below outlines the steps associated with public notification insofar as it relates to s95 of the RMA.

Table 4 - s95 Adverse Effects Assessment

Step 1	Mandatory public notification in certain circumstances		
S95A(3)(a)	Has the applicant requested that the application be publicly notified?	No	
S95A(3)(b)	Is public notification required under section 95C?(after a request for further information)	TBC	
S95A(3)(c)	Has the application been made jointly with an application to exchange recreation reserve land under section 15AA of the Reserves Act 1977.		
Step 2	if not required by step 1, public notification precluded in cercircumstances	rtain	
S95A(5)(a)	Is the application for a resource consent for 1 or more activities and each activity is subject to a rule or national environmental standard that precludes public notification?	No	
S95A(5)(b)	Is the application for a resource consent for 1 or more of the following, but no other, activities;  (i) a controlled activity;  (i) a restricted discretionary, discretionary, or non-complying activity, but only if the activity is a boundary activity;	No	

#### 7.0 EFFECTS ON THE ENVIRONMENT

Effects on persons who are owners and occupiers of the land in, on, or over which the application relates, or of adjacent land must be disregarded when considering effects on the environment (s 95D(a)). Adjacent persons are shown and listed in Figure 5 and 6 below.

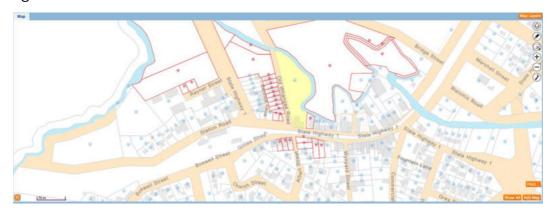


Figure 10 - Site & Surrounds [Source: Prover]

Address	Capital Value	Last Sale Date	Last Sale Price	Land Area	Floor Area	Cat
3 Old Whangae Road Kawakawa Far North	64000			287 m²		IVP Industrial Vacant
4 State Highway 1 Kawakawa Far North						null Undefined
5 Old Whangae Road Kawakawa Far North	80000	11 Jul 2002	50000	343 m²		IVP Industrial Vacant
7 Old Whangae Road Kawakawa Far North	79000	23 Mar 2023	170000	336 m²	140 m²	ILP Industrial Light manufacturing
9 Old Whangae Road Kawakawa Far North	150000	01 Jan 1900	81000	329 m²	210 m <sup>2</sup>	ISP Industrial Service
11 Old Whangae Road Kawakawa Far North	106000			329 m²	170 m²	ISP Industrial Service
13 Old Whangae Road Kawakawa Far North	117000	31 Jul 2017	120000	329 m²	200 m²	ISP Industrial Service
80 Gillies Street Kawakawa Far North	195000	04 Jun 2014	200000	559 m²	454 m²	CRPB Commercial Retail
15 Old Whangae Road Kawakawa Far North	78000	27 Jun 2004	9857	336 m²		IVP Industrial Vacant
17 Old Whangae Road Kawakawa Far North	300000	27 Jun 2004	220143	658 m²	480 m²	ILP Industrial Light manufacturing
53 Gillies Street Kawakawa Far North	650000	01 Mar 2016	650000	1,872 m²	596 m²	CXP Commercial Multiple/unknown
71 Gillies Street Kawakawa Far North	550000	23 Dec 1996	245000	1,067 m²	1,100 m²	CXP Commercial Multiple/unknown
0 Bridge Street Kawakawa Far North	560000	01 Jan 1900	25000	3.3656 ha		OP Other Passive
0 State Highway 1 Kawakawa Far North	165000	06 Jun 2008	36000	6,081 m²		IVP Industrial Vacant
8 Rayner Street Kawakawa Far North	1860000			5.6664 ha	458 m²	CKP Commercial Education

Figure 11 – Adjacent / Adjoining Persons [Source: Prover]

#### 7.1 Effects that May be Disregarded

The permitted baseline may be taken into account should the Council deem it relevant. In relation to the proposal, the permitted baseline is not considered overly relevant as only a small amount of legitimate permitted development could take place on this split zoned site.

#### 7.2 Effects Assessment

The following assessment has been prepared in accordance with Section 88 and Schedule 4 of the RMA which specifies that the assessment of effects provided

should correspond with the scale and significance of the proposal. The effects of the proposal are considered in <u>Table 5</u> below.

<u>Table 5 – Effects Assessment</u>

Item	Assessment Criteria	Assessment
Positive Effects	Nil	Cultural Wellbeing
Linoto		Expression of Kaitiakitanga and Identity     The architectural plans explicitly incorporate a     Pou Whenua within the central communal     courtyard. This physical marker serves as a     cultural anchor, reinforcing the connection to the     land and the identity of Ngāti Hine within the     development.
		Housing for Mana Whenua     In partnership with the Ngāti Hine Health Trust,     the development provides secure housing within     the rohe, allowing whānau to remain connected     to their ancestral lands and community support     networks rather than being displaced due to a     lack of housing stock.
		Social Wellbeing
		Addressing Housing Need     The proposal delivers 30 new residential units [18 one-bedroom and 12 two-bedroom units]. This medium-density approach significantly increases the local housing stock, directly addressing housing deprivation in the area.
		Accessibility and Universal Design     The architectural drawings confirm compliance with Universal Design Standards. Features include level entry thresholds, wider doors [810mm+], and ground-floor bathrooms. This ensures the housing caters to kaumātua and

whānau with mobility issues, promoting social inclusion and aging in place.

Walkability and Connectivity
 The site is highly connected, located within walking distance of essential social infrastructure:

o Local Town Centre: 1-10 minutes.

Primary School: 8 minutes.

o High School: 20 minutes.

#### Community Design

The Master Plan emphasizes social interaction through the inclusion of shared courtyards, a pergola, and pedestrian-friendly pathways connecting the blocks internally and externally.

#### **Economic Wellbeing**

- Construction Employment
   The project involves significant civil works, including 8,965m³ of fill for earthworks, construction of retaining walls, and 30 residential units. This will generate immediate employment and economic activity for local contractors and tradespeople.
- Support for Local Economy By placing 30 households within 500m of the Kawakawa town center, the development increases foot traffic and customer base for local businesses and services, contributing to the town's economic vitality.
- Efficient Land Use

The proposal converts underutilized land into high-value medium-density housing, maximizing the economic utility of the land resource within the existing urban limit.

#### **Environmental Wellbeing**

		Flood Resilience and Climate Adaptation     A major environmental benefit is the remediation of flood hazards. The proposal raises the FFL of the units to 7.0m, placing building platforms 500mm above the 1% AEP flood level [including climate change allowance].
		Improved Drainage Infrastructure     The project includes the installation of a new     525mm diameter negative-grade stormwater pipe     beneath the site. This infrastructure replicates     pre-development overflow paths, conveying     floodwaters from the unlined channel to a     discharge point, ensuring no adverse flooding     effects on upstream or downstream properties.
		Land Remediation     The geotechnical strategy involves stabilizing weak alluvium soils through preloading and the construction of engineered gravel rafts. This improves the stability and safety of the land, making it suitable for long-term habitation.
		Landscape and Permeability     Despite the density, the site plan maintains 50%     landscape area across the development, which assists with onsite amenity and permeable surface area for surface water management.
Residential	Chapter 11	Residential Intensity [Chapter 11.1]
Intensity, Setbacks and Sunlight	and Chapter 12	Scale and Character     The design breaks the massing into six distinct blocks [A–F] separated by courtyards and parking to reduce visual dominance. It is acknowledged that the design of the proposal does not address Old Whangae Road and proposes to instead front the Waiomio Stream. This is largely due to the nature of Old Whangae Road being a no exit road with minimal pedestrian interaction. However, some units do address Old Whangae Road with their outdoor living space. The design is

considered to meet the right balance of being appropriately separated from the Stream, take advantage of its amenity, and contextualising the built development against the nature and purpose of Old Whangae Road.

#### Heights

The scale of the buildings are within the height limits for the zone.

#### • Visual Dominance

The use of varied cladding materials [fibre cement, profiled metal] and articulated rooflines breaks up the building bulk, reducing visual domination.

#### Setback and Sunlight

The development has numerous interfaces where it is not setback at least 10m from site boundaries. At the Old Whangae Road interface, the effects here are limited to pedestrians and road users which is currently limited due to it be a no – exit road. The placement of the buildings close to this boundary is unlikely to impact any future roading decisions. Setback and sunlight at the other interface is limited by the existence of stormwater infrastructure which provides additional separation to other activities and in effect acting as an addition boundary / setback buffer for the development. The internal setback and sunlight breaches are appropriate as the main access road has been positioned here to ensure access to sunlight is maximised and that impact to privacy are minimised.

#### Lakes, Rivers, Wetlands [Chapter 12.7.7]

Cultural Values [Criterion a]
 The development notes the importance of the Waiomio Stream and has sought to position buildings to allow for its amenity to be a positive effect for the development. Development

impacts from earthworks and ongoing servicing are considered to be appropriately mitigated. The site is not considered as a site of significance. There are no known archaeological sites present.

- Natural Hazards [Criterion c]
   The proposal actively mitigates flood hazards by raising the FFL of units to 7.0m, which is 500mm above the 1% AEP flood level. The Geotech report also recommends a Reinforced Earth Wall to withstand erosion forces from flood waters.
- Amenity and Natural Character [Criterion d & e]
   Having at least a 50% landscape area helps
   soften the built environment's impact on the
   stream margin. The setback is well below what is
   envisaged, however ensures the buildings do not
   visually crowd the stream edge. The site is
   developed in terms of stream protection works
   and the existing connecting footpath through the
   site.
- Water Quality [Criterion f, g, & h]
   The design includes a new stormwater outlet with a concrete headwall and riprap protection down to the water level to prevent scour and erosion, thereby protecting water quality. The development connects to reticulated sewerage, avoiding on-site disposal risks to the stream. The stormwater features are compatible with fish passage and appropriately mitigate effects to fauna and flora.
- Functional Need [Criterion k]
   The site is adjacent to the water body and is proposed to be rezoned to Mixed Use through the PDP. The proposed activity is consistent with that future use proposed by Council.
- Public Access [Criterion k]
   The Civil Plans identify an existing Foot Bridge and Existing Path near the stream margin, which

		are integrated into the site layout, maintaining connectivity.
Stormwater & Building	Chapter 11	Stormwater Management [Chapter 11.3]
Coverage		The Three Waters Report confirms that stormwater neutrality is not required because the site is located at the bottom of the catchment. Runoff discharges directly to the northern side of the diversion bank, meaning peak flows do not compound upstream flood peaks.
		To manage the alteration in natural drainage, the proposal includes a specific engineering solution, being a new 525 mm diameter negative-grade pipe. This infrastructure is designed to replicate the predevelopment overflow behaviour of the existing unlined channel, ensuring that the raising of the land does not dam or divert overland flows onto neighbouring properties.
		The proposal actively provides for climate change by setting FFL at RL 7.00m [500mm freeboard above the 1% AEP + CC level]. This demonstrates a robust response to future climate risks.
		The Three Waters report details a scruffy dome intake and a new outlet with a concrete headwall and riprap protection. These engineering solutions prevent scour and erosion at the discharge point. The hydraulic modelling confirms that these measures result in a negligible difference in flood depths between the pre- and post-development scenarios, satisfying the requirement to mitigate adverse effects.
		Building Coverage [Chapter 11.24]
		The development site remains with 50% open space following completion of the development. This is

considered appropriate in context of the site and the stormwater environment it is located.

The buildings are proposed to be modern dwellings and are not in keeping with the surrounding buildings but are not out of place in this environment. Private open space is appropriately provided for, as is communal open space on the site for residents.

The scale and bulk of buildings are addressed above. The design approach has been to develop the site into a series of blocks as opposed to a monolithic structure. Heights are in keeping with the permitted standard. The closeness of the buildings to public places has been considered to result in minimal effects along Old Whangae Road, with stormwater infrastructure providing an additional buffer to those adjacent properties.

The building coverage of ~20% is not considered to result in adverse effects that are more than minor.

## Traffic, Parking and Access

## Chapter 11 & Chapter 15

From a traffic perspective, no adverse effects are considered to arise from the increase in traffic movements from the residential development. Old Whangae road has sufficient capacity for the development and the intersection with Gillies Street provides ample sight distances. Minor road marking changes are proposed in this respect.

In terms of parking, whilst there is a parking breach, the proposal includes largely one bedroom dwellings and it is typical to allocate 1 car park for these units. On the whole, the proposal provides for 1 car park per unit, and 5 additional car parks for visitors. This is considered appropriate in an urban environment which is close to local amenities, goods and services.

In terms of access effects, the proposal accords with engineering standards in terms of providing appropriate vehicle crossings and the layout and

		design of the internal access although not of a road to vest standards, is appropriate for the development. No major upgrades are proposed along Old Whangae Road.
Development Servicing	Chapter 13 / Engineering Standards	As outlined in the engineering reports provided in Appendix D, the site can be appropriately serviced and conditions of consent can ensure that the proposal meets relevant standards.
Natural Hazards	Chapter 12	The Three Waters Report appropriately considers the potential flooding effect of the proposal and considers that this results in a less than 5mm impact. This is a marginal effect and considered to be less than minor. There are no other hazards known to impact the development.
Subdivision	Chapter 13	The sites created can be appropriately serviced by infrastructure, have appropriate easements, and will be developed with a land use activity that is anticipated by the PDP. There are no effects resulting from the subdivision that are not assessed via the substantive land use proposal.
		The effects of the subdivision with respect to the PDP breach of the Star Hotel is not considered to result in any effects. This is a simple subdivision to ensure that the Star Hotel has its own title that is separate from the housing development.
		Only the building is considered to have heritage value, not the site. This is confirmed by the ODP and PDP mapping and description of the heritage resource.
Earthworks & Geotech	Chapter 12	The proposal includes appropriate erosion and sediment controls, and this aspect will also be considered by the Northland Regional Council. Subject to appropriate conditions being imposed in terms of this matter, effects will be no more than minor.

		The Geotech Report confirms that subject to recommendations being adhered to, development can proceed accordingly.
Reserve Matters	Chapter 14	At this stage, the scheme plan does not show a reserve to vest or any provision for the existing footpath. This is not to suggest that this is not negotiable through the consent process.
Concluding Statement:		Having considered the above, the effects of the proposal are considered to be no more than minor.

## 8.0 EFFECTS TO PEOPLE

The table below outlines the steps associated with limited notification insofar as it relates to s95 of the RMA.

Table 6 - s95 Affected Persons Assessment

Step 1	certain affected groups and affected persons must be notif	<u>ied</u>
S95B(2)(a)	Are there any affected protected customary rights groups?	No
S95B(2)(b)	Are there any affected customary marine title groups (in the case of an application for a resource consent for an accommodated activity)?	No
S95B(3)(a)	Is the proposed activity on or adjacent to, or may affect, land that is the subject of a statutory acknowledgement made in accordance with an Act specified in Schedule 11?	No
S95B(3)(b)	Is the person to whom the statutory acknowledgement is made is an affected person under section 95E?	No
Step 2	if not required by step 1, limited notification precluded in circumstances	ertain
S95B(6)(a)	the application is for a resource consent for 1 or more activities, and each activity is subject to a rule or national environmental standard that precludes limited notification:	No
S95B(6)(b)	the application is for a controlled activity (but no other activities) that requires a resource consent under a district plan (other than a subdivision of land)	No

## 8.1 Affected Person Determination

As the proposed activity does not trigger mandatory limited notification, nor is it precluded, an assessment of potentially affected persons must be undertaken.

The consent authority has discretion to determine whether a person is an affected person. A person is affected if an activity's adverse effects are minor or more than minor to them. The effects of the proposal on adjacent landowners have been undertaken in section 8.3 below.

## 8.2 Written Approvals Received & Consultation

No written approvals have been sought or provided. However, consultation has been undertaken with Top Energy, Chorus and NZTA. A CDM has been undertaken with FNDC. A response to the matters raised in the CDM is as follows:

Table 7 - CDM Response

CDM Item	Council Query / Comment	Design Response & Reference
Planning	Residential vs. Commercial:	Response: The site is located
[Zoning]	Council requested justification	on a cul-de-sac [Old Whangae
	for a purely residential	Rd] physically separated from
	development in the PDP "Mixed	the main commercial strip.
	Use Zone" which prioritizes	Commercial frontage is not
	commercial activity.	viable here. Residential
		intensity supports the nearby
		town center vitality without
		competing with it.
Urban Design	Active Frontage & Retaining:	Response: The retaining wall is
	Concern that the 2m retaining	a functional necessity for flood
	wall creates a barrier and fails to	mitigation [raising FFL to 7.0m].
	provide "active street frontage"	
	or connectivity to the cycle trail.	This earth wall is only 2.5m in
		height and different from that
		shown on the CDM plans.

		I
		Its visual dominance is
		softened by landscaping and
		architectural fencing, details of
		which can be provided as a
		condition of consent.
		Connectivity is direct to the
		cycle trail footpath internally to
		the site. Other users can go via
		Old Whangae Road.
Urban Design	Safety (CPTED): Council	Response: The layout
Orban Booign	queried lighting for car parks	promotes passive surveillance
	and pedestrian	over the central courtyard and
	safety/surveillance.	carparking areas. Lighting will
	Safety/Surveillarice.	
		be provided for, details of which
		can form part of the overall
		developed design package.
Engineering	Emergency Access: Can	<b>Response:</b> FFL are raised to RL
[Flooding]	fire/ambulance vehicles access	7.0m [500mm freeboard]. The
	the site during a 100-year flood?	Three Waters Report confirms
	Are carparks underwater?	the driveway and parking areas
		are designed to manage
		floodwaters, and the site is
		located at the bottom of the
		catchment, requiring no
		attenuation.
Engineering	Site Stability: Council noted the	Response: The Geotech Report
[Geotech]	site is "potentially medium	identifies a "weak alluvium
[coodson]	hazard" and requested cut/fill	layer". The proposal utilizes an
	balance and retaining design.	Engineered Gravel Raft
	batarios ana rotanning acoign.	foundation with geogrid
		reinforcement and preloading
Enginessing	Consitu Consituación accessor	to mitigate settlement risks.
Engineering	Capacity: Capacity assessment	Response: A new private
[Services]	required for water and	150mm wastewater network
	wastewater.	will discharge to the existing
		300mm main. Water supply
		utilizes an extended 50mm
		rider main. Engineering reports
		confirm sufficient capacity.

Engineering	Discharge Strategy: How is	Response: A new 525mm
[Stormwater]	stormwater managed to prevent	negative-grade pipe is
	downstream risk?	proposed to replicate the pre-
		development overflow path.
		This conveys floodwaters from
		the eastern channel to the
		outlet without worsening
		downstream effects.
Reserves	Esplanade: An esplanade	Response: The development is
	waiver or reserve may be	set back from the stream. No
	required along the stream.	formal esplanade reserve to
		vest is proposed, but public
		access is maintained via the
		existing footpath network.

## 8.3 Localised Effects Assessment [Effects to Persons]

<u>Section 7</u> of this report provides a graphic and table of the relevant adjacent persons that this assessment relates.

Based on the separation distances and the nature of the proposed activity, the neighbours at Old Whangae Road are unlikely to be adversely affected by the development.

The physical buffer provided by the road width itself, combined with the natural boundary of the Waiomio Stream and the adjacent Council-owned land, ensures significant spatial separation between the new residential units and the existing uses.

The proposed residential activity is inherently compatible with the surrounding environment as it generates lower levels of noise, dust, and vibration than the existing activities, thereby avoiding nuisance effects.

Furthermore, potential infrastructure impacts have been engineered out. Specifically, the installation of the new 525mm negative-grade stormwater pipe ensures that the raising of the site levels will not displace floodwaters onto neighbouring properties, and the upgraded commercial vehicle crossing is designed to safely accommodate the increased traffic without disrupting the flow of traffic on Old Whangae Road.

## 8.4 Effect to Persons Conclusion

No persons are considered potentially affected by the proposal.

## 9.0 STATUTORY CONTEXT

## 9.1 Far North District Plan – Operative [ODP]

An assessment of the relevant objectives and policies associated with the ODP has been undertaken and is found in tables below.

While the site is zoned Rural Production under the ODP, it is physically severed from any functional rural unit, being located within the urban limit and surrounded by commercial/industrial uses.

The assessment below demonstrates that strictly applying Rural Production objectives would effectively sterilize the land.

The proposal aligns more closely with the PDP's Mixed Use Zone, which Council notified the site to be and recognizes the site's suitability for urban intensification.

Table 8 - Rural Environment Assessment

Objective / Policy	Assessment
Objectives	
8.3.1 To promote the sustainable management of natural and physical resources of the rural environment while enabling activities to establish in the rural environment.	The proposal enables the sustainable management of physical resources by utilizing an isolated, underutilized land parcel for essential housing, rather than encroaching on productive rural land elsewhere.
8.3.2 To ensure that the life supporting capacity of soils is not compromised by inappropriate subdivision, use or development.	The site's soils are already compromised by historic fill and urban proximity. The Geotech report confirms the land requires significant remediation [gravel raft] to be stable, indicating it has low utility for rural production.
8.3.3 To avoid, remedy or mitigate adverse effects of activities on the rural environment.	Effects on the rural environment are negligible as the site is functionally part of the urban environment, disconnected from the wider rural hinterland.

Objective / Policy	Assessment	
8.3.4 To protect areas of significant indigenous vegetation and significant habitats of indigenous fauna.	No significant indigenous vegetation or habitats are present on the site; the site is pasture and built-up area.	
8.3.5 To protect outstanding natural features and landscapes.	The site does not contain outstanding natural features or landscapes.	
8.3.6 To avoid actual and potential conflicts between land use activities in the rural environment.	The site is separated from rural activities. Reverse sensitivity regarding the adjacent industrial zone is mitigated by the physical separation of the road and Steam and the nature of the proposed residential use.	
8.3.7 To promote the amenity values of the rural environment.	The proposal enhances amenity by replacing a vacant, flood-prone lot with a high-quality, architecturally designed housing development with appropriate open space [50% coverage].	
8.3.8 To facilitate the sustainable management of natural and physical resources in an integrated way to achieve superior outcomes to more traditional forms of subdivision, use and development through management plans and integrated development.	The proposal utilizes a comprehensive master plan approach, integrating engineering, flood management, and architectural design to achieve a superior outcome to ad-hoc development.	
Policies		
8.4.1 That activities which will contribute to the sustainable management of the natural and physical resources of the rural environment are enabled to locate in that environment.	Housing is a critical resource. Locating high-density housing near existing infrastructure contributes to sustainable urban growth management.	

Objective / Policy	Assessment	
8.4.2 That activities be allowed to establish within the rural environment to the extent that any adverse effects of these activities are able to be avoided, remedied or mitigated and as a result the life supporting capacity of soils and ecosystems is safeguarded.	Adverse effects [flooding, stability] are technically resolved via engineering solutions [gravel raft, stormwater outlet], safeguarding the surrounding ecosystem.	
8.4.3 That any new infrastructure for development in rural areas be designed and operated in a way that safeguards the life supporting capacity of air, water, soil and ecosystems while protecting areas of significant indigenous vegetation and significant habitats of indigenous fauna, outstanding natural features and landscapes.	New infrastructure [wastewater / stormwater] connects to reticulated networks where possible or is designed to mitigate effects [e.g. scour protection in the Stream].	
8.4.4 That development which will maintain or enhance the amenity value of the rural environment and outstanding natural features and outstanding landscapes be enabled to locate in the rural environment.	The development introduces a structured, landscaped urban form that improves the visual amenity of a currently underutilized site.	
8.4.5 That plan provisions encourage the avoidance of adverse effects from incompatible land uses, particularly new developments adversely affecting existing land-uses (including by constraining the existing land-uses on account of sensitivity by the new use to adverse effects from the existing use – i.e., reverse sensitivity).	The proposed residential use acts as a transition buffer between the town centre and the Stream / cycle trail, compatible with the mixed-use trajectory of the area.	

Objective / Policy	Assessment
8.4.6 That areas of significant indigenous vegetation and significant habitats of indigenous fauna habitat be protected as an integral part of managing the use, development and protection of the natural and physical resources of the rural environment.	Not applicable; no significant vegetation exists on the site.
8.4.7 That Plan provisions encourage the efficient use and development of natural and physical resources.	This is a highly efficient use of land, delivering 30 units in close proximity to town services, maximizing the utility of the physical resource.
8.4.8 That, when considering subdivision, use and development in the rural environment, the Council will have particular regard to ensuring that its intensity, scale and type is controlled to ensure that adverse effects on habitats (including freshwater habitats), outstanding natural features and landscapes, on the amenity value of the rural environment, and where appropriate on natural character of the coastal environment, are avoided, remedied or mitigated.	While the intensity is higher than the rural zone anticipates, it is appropriate for the site's physical context and the PDP's urban zoning direction.

Table 9 – Rural Production Zone Assessment

Objective Or Policy	Performance Of Proposal
Objectives	
8.6.3.1 To promote the sustainable management of natural and physical resources in the Rural Production Zone.	The proposal manages the land resource sustainably by repurposing non-productive land for high-demand housing.

Objective Or Policy	Performance Of Proposal
8.6.3.2 To enable the efficient use and development of the Rural Production Zone in a way that enables people and communities to provide for their social, economic, and cultural well-being and for their health and safety.	The proposal provides for social and economic well-being by delivering 30 units to the community.
8.6.3.3 To promote the maintenance and enhancement of the amenity values of the Rural Production Zone.	The design includes significant landscaping and architectural articulation to enhance the visual amenity of the site and surrounds.
8.6.3.4 To promote the protection of significant natural values of the Rural Production Zone.	The Waiomio Stream margin is respected through setback and rip-rap protection works, ensuring natural values are not degraded.
8.6.3.5 To protect and enhance the special amenity values of the frontage to Kerikeri Road between its intersection with SH10 and the urban edge of Kerikeri	Not relevant to this location.
8.6.3.6 To avoid, remedy or mitigate the actual and potential conflicts between new land use activities and existing lawfully established activities (reverse sensitivity) within the Rural Production Zone and on land use activities in neighbouring zones.	The residential use is compatible with the surrounding mixed-use environment. The adjacent uses are mixed in nature and compatible with an urban fringe setting.
8.6.3.7 To avoided, remedy or mitigate the adverse effects of incompatible use or development on natural or physical resources.	The proposal is compatible with the urban-edge context and the future Mixed Use zoning promoted by Council.

Objective Or Policy	Performance Of Proposal	
8.6.3.8 To enable the efficient establishment and operation of activities and services that have a functional need to be located in the rural environments.	While not a rural activity, the development has a functional need to locate here to utilize the specific land holding of the applicant for housing needs.	
8.6.3.9 To enable rural production activities to be undertaken in the zone	The site is too small and isolated for viable rural production; its conversion does not undermine the district's overall rural productivity.	
Policies		
8.6.4.1 That a wide range of activities be allowed in the Rural Production Zone, subject to the need to ensure that any adverse effects, including any reverse sensitivity effects, on the environment resulting from these activities are avoided, remedied or mitigated.	The policy allows a range of activities. Residential is appropriate given the specific site constraints preventing rural production.	
8.6.4.2 That standards be imposed to ensure that the off-site effects of activities in the Rural Production Zone are avoided, remedied or mitigated.	Engineering reports confirm off-site effects [stormwater, traffic] are mitigated to acceptable standards.	
8.6.4.3 That land management practices that avoid, remedy or mitigate adverse effects on natural and physical resources be encouraged.	Sediment and erosion control plans [Appendix D] ensure land management best practices are followed during earthworks.	
8.6.4.4 That the intensity of development allowed shall have regard to the maintenance and enhancement of the amenity values of the Rural Production Zone.	The density is high but designed with internal courtyards and landscaping to ensure high on-site amenity for residents.	

Objective Or Policy	Performance Of Proposal		
8.6.4.5 That the efficient use and development of physical and natural resources be taken into account in the implementation of the Plan.	Developing 30 units on this site is a more efficient use of the land resource than leaving it as a remnant, unproductive rural lot.		
8.6.4.6 That the built form of development allowed on sites with frontage to Kerikeri Road between its intersection with SH10 and Cannon Drive be maintained as small in scale, set back from the road, relatively inconspicuous and in harmony with landscape plantings and shelter belts			
8.6.4.7 That although a wide range of activities that promote rural productivity are appropriate in the Rural Production Zone, an underlying goal is to avoid the actual and potential adverse effects of conflicting land use activities.	See 8.6.3.6 above. Conflicts are minimized through design and separation.		
8.6.4.8 That activities whose adverse effects, including reverse sensitivity effects, cannot be avoided remedied or mitigated are given separation from other activities.	road by retaining and landscaping, and from the Stream by the bund/esplanade		
8.6.4.9 That activities be discouraged from locating where they are sensitive to the effects of or may compromise the continued operation of lawfully established existing activities in the Rural Production zone and in neighbouring zones.	surrounding environment is transitioning to mixed-use, making this activity less sensitive than it would be in a purely working rural environment.		

Table 10 - Subdivision Chapter Assessment

Objective Or Policy	Performance Of Proposal		
Objectives			
13.3.1 To provide for the subdivision of land in such a way as will be consistent with the purpose of the various zones in the Plan and will promote the sustainable management of the natural and physical resources of the District, including airports and the social, economic and cultural wellbeing of people and communities.	The subdivision facilitates a land use [housing] that directly promotes wellbeing while managing adverse effects.		
13.3.2 To ensure that subdivision of land is appropriate and is carried out in a manner that does not compromise the life-supporting capacity of air, water, soil or ecosystems, and that any actual or potential adverse effects on the environment which result directly or indirectly from subdivision, including reverse sensitivity effects, are avoided, remedied or mitigated.	The subdivision layout is designed specifically to accommodate the multi-unit development, ensuring all lots are serviced and accessible.		
13.3.3 To ensure that the subdivision of land does not jeopardise the protection of outstanding landscapes or natural features in the coastal environment.	Not applicable.		
13.3.4 To ensure that subdivision does not adversely affect scheduled heritage resources through alienation of the resource from its immediate setting/context.	The subdivision separates the Historic Star Hotel onto its own title [Lot 3], ensuring its protection and distinct management from the new residential lots.		

Objective Or Policy	Performance Of Proposal		
13.3.5 To ensure that all new subdivisions provide a reticulated water supply and/or on-site water storage sufficient to meet the needs of the activities that will establish all year round.	reticulated council water supply via a extended rider main.		
13.3.6 To encourage innovative development and integrated management of effects between subdivision and land use which results in superior outcomes to more traditional forms of subdivision, use and development, for example the protection, enhancement and restoration of areas and features which have particular value or may have been compromised by past land management practices.	The simple subdivision structure supports an innovative medium-density housing model that is new to this locality.		
13.3.7 To ensure the relationship between Maori and their ancestral lands, water, sites, wahi tapu and other taonga is recognised and provided for.	ds, partnership to provide housing for Mana		
Policies			

Objective Or Policy	Performance Of Proposal		
13.4.1 That the sizes, dimensions and distribution of allotments created through the subdivision process be determined with regard to the potential effects including cumulative effects, of the use of those allotments on:  (a) natural character, particularly of the coastal environment;  (b) ecological values;  (c) landscape values;  (d) amenity values;  (e) cultural values;  (f) heritage values; and  (g) existing land uses.	The allotment sizes are dictated by the comprehensive land use proposal, ensuring they are sized for the intended housing typology.		
13.4.2 That standards be imposed upon the subdivision of land to require safe and effective vehicular and pedestrian access to new properties.	vehicle crossings designed to Council		
13.4.3 That natural and other hazards be taken into account in the design and location of any subdivision.	, , , , , , , , , , , , , , , , , , , ,		
13.4.4 That in any subdivision where provision is made for connection to utility services, the potential adverse visual impacts of these services are avoided.	Services are underground, avoiding visual clutter.		

Objective Or Policy	Performance Of Proposal
13.4.5 That access to, and servicing of, the new allotments be provided for in such a way as will avoid, remedy or mitigate any adverse effects on neighbouring property, public roads, and the natural and physical resources of the site caused by silt runoff, traffic, excavation and filling and removal of vegetation.	A comprehensive Erosion and Sediment Control Plan [RC210] is provided to manage earthworks effects.
13.4.6 That any subdivision proposal provides for the protection, restoration and enhancement of heritage resources, areas of significant indigenous vegetation and significant habitats of indigenous fauna, threatened species, the natural character of the coastal environment and riparian margins, and outstanding landscapes and natural features where appropriate.	The subdivision boundary respects the curtilage of the Star Hotel.
13.4.7 That the need for a financial contribution be considered only where the subdivision would:  (a) result in increased demands on car parking associated with non-residential activities; or  (b) result in increased demand for esplanade areas; or  (c) involve adverse effects on riparian areas; or  (d) depend on the assimilative capacity of the environment external to the site.	The applicant acknowledges financial contributions will be assessed in accordance with the Plan.
13.4.8 That the provision of water storage be taken into account in the design of any subdivision.	Reticulated supply is available; onsite storage is not required.

Objective Or Policy	Performance Of Proposal
13.4.9 That bonus development donor and recipient areas be provided for so as to minimise the adverse effects of subdivision on Outstanding Landscapes and areas of significant indigenous flora and significant habitats of fauna.	Not applicable.
13.4.10 The Council will recognise that subdivision within the Conservation Zone that results in a net conservation gain is generally appropriate.	Not applicable.
13.4.11 That subdivision recognises and provides for the relationship of Maori and their culture and traditions, with their ancestral lands, water, sites, waahi tapu and other taonga and shall take into account the principles of the Treaty of Waitangi.	See 13.3.7. The development creates housing on land for local whānau.
13.4.12 That more intensive, innovative development and subdivision which recognises specific site characteristics is provided for through the management plan rule where this will result in superior environmental outcomes.	The subdivision enables a higher density than standard rural/residential, resulting in superior social outcomes for the district.
13.4.13 Subdivision, use and development shall preserve and where possible enhance, restore and rehabilitate the character of the applicable zone in regard to s6 matters, and shall avoid adverse effects as far as practicable by using techniques including:  (a) clustering or grouping development within areas where there is the least	The subdivision creates a structured, landscaped urban edge that improves upon the current vacant/scrub appearance.

Objective Or Policy	Performance Of Proposal
impact on natural character and its	
elements such as indigenous vegetation,	
landforms, rivers, streams and	
wetlands, and coherent natural patterns;	
(b) minimising the visual impact of	
buildings, development, and associated	
vegetation clearance and earthworks,	
particularly as seen from public land and	
the coastal marine area;	
(c) providing for, through siting of	
buildings and development and design of	
subdivisions, legal public right of access	
to and use of the foreshore and any	
esplanade areas;	
(d) through siting of buildings and	
development, design of subdivisions,	
and provision of access that recognise	
and provide for the relationship of Maori	
with their culture, traditions and taonga	
including concepts of mauri, tapu,	
mana, wehi and karakia and the	
important contribution Maori culture	
makes to the character of the District	
(refer <b>Chapter 2</b> and in particular	
Section 2.5 and Council's "Tangata	
Whenua Values and Perspectives"	
(2004);	
(e) providing planting of indigenous	
vegetation in a way that links existing	
habitats of indigenous fauna and	
provides the opportunity for the	
extension, enhancement or creation of	
habitats for indigenous fauna, including	
mechanisms to exclude pests;	

Objective Or Policy	Performance Of Proposal
(f) protecting historic heritage through the siting of buildings and development and design of subdivisions.	
13.4.14 That the objectives and policies of the applicable environment and zone and relevant parts of <b>Part 3</b> of the Plan will be taken into account when considering the intensity, design and layout of any subdivision.	The design considers the Mixed Use zone objectives of the PDP, aligning the subdivision with the future character of the area promoted by Council upon its notification.

Table 11 - Mixed Use Zone PDP Assessment

Objectives	Assessment			
MUZ-O1 The Mixed Use zone is the focal point for the district's commercial, community and civic activities, and provides for residential development where it complements and is not incompatible with these activities.	critical mass necessary to support the commercial and civic activities of the nearby Kawakawa centre.			
MUZ-O2 Development in the Mixed Use zone is of a form, scale, density and design quality that contributes positively to the vibrancy, safety and amenity of the zone.	are consistent with the urban form			
MUZ-O3 Enable land use and subdivision in the Light Industrial zone where there is adequacy and capacity of available or programmed development infrastructure to support it.	Infrastructure reports confirm the development can be serviced, supporting the enabling of this land use.			
MUZ-O4 The adverse environmental effects generated by activities within the zone are managed, in particular at zone boundaries.	Effects at boundaries are managed through setbacks, landscaping, and acoustic privacy considerations.			

MUZ-O5 Residential activity in the Mixed Use zone is located above commercial activities to ensure active street frontages, except where the interface is with the Open Space zone.

While not above commercial, the residential use is appropriate given the site's location on a secondary road where commercial frontage is not viable and would detract from the Kawakawa main street.

#### **Policies**

## MUZ-P1 Enable a range of commercial, community, civic and residential activities in the Mixed Use zone where:

- a. it supports the function, role, sense of place and amenity of the existing environment; and
- b. there is:
  - existing infrastructure to support development and intensification, or
  - ii. additional infrastructure capacity can be provided to service the development and intensification.

#### **Assessment**

The proposal supports the 'sense of place' by providing housing near the town centre. Existing infrastructure is being utilized and extended to support this intensification.

MUZ-P2 Require all subdivision in the Mixed Use zone to provide the following reticulated services to the boundary of each lot:

- a. telecommunications:
  - i. fibre where it is available;
  - ii. copper where fibre is not available;
  - iii. copper where the area is identified for future fibre deployment.
- b. local electricity distribution network; and

The development connects to reticulated water, wastewater, and power/telecommunications as required.

c. wastewater, potable water supply and stormwater where they are available.

MUZ-P3Require development in the Mixed Use zone to contribute positively to:

- a. high quality streetscapes;
- b. pedestrian amenity;
- c. safe movement of people of all ages and abilities;
- d. community well-being, health and safety; and
- e. traffic, parking and access needs.

The development contributes to community well-being [housing], safe movement [new footpaths], and pedestrian amenity [connection to cycle trail].

MUZ-P4 Require development in the Mixed Use zone that is adjacent to Residential and Open Space zones to maintain the amenity values of those areas, having specific regard to:

- a. visual dominance;
- b. privacy;
- c. shadowing;
- d. ambient noise; and
- e. light spill.

The site adjoins open space [Stream and council owned land] and roading. Visual dominance is managed through building articulation and material selection.

MUZ-P5 Restrict activities that are likely to have an adverse effect on the function, role, sense of place and amenity of the Mixed Use zone, including:

- a. residential activity, retirement facilities and visitor accommodation on the ground floor of buildings, except where a site adjoins an Open Space zone;
- b. light or heavy industrial activity;
- c. storage and warehousing;

Residential on the ground floor is restricted in this zone generally to protect commercial streets. However, Old Whangae Road is not a primary commercial street and if used in this capacity would likely detract from the Kawakawa main street.

- d. large format retail activity over 400 m<sup>2</sup>; and
- e. waste management activity.

MUZ-P6 Promote energy efficient design and the use of renewable electricity generation in the construction of mixed use development. The units are designed to modern building code standards for energy efficiency.

MUZ-P7 Consider the following effects when assessing applications to establish residential, early childhood, retirement and education facilities:

Privacy and shadowing have been assessed. The layout maximizes internal amenity while minimizing effects on the streetscape.

- a. the level of ambient noise;
- b. reduced privacy;
- c. shadowing and visual domination; and
- d. light spill.

MUZ-P8 Manage land use and subdivision to address the effects of the activity requiring resource consent, including (but not limited to) consideration of the following matters where relevant to the application:

- a. consistency with the scale, density, design, amenity and character of the mixed use environment;
- the location, scale and design of buildings or structures, outdoor storage areas, parking and internal roading;
- c. at zone interfaces:
  - i. any setbacks, fencing, screening or landscaping required to address potential conflicts;

The proposal is consistent with the scale of the mixed-use environment. Natural hazards [flooding] are managed via engineering design [raised floor levels].

- ii. any adverse effects on the character and amenity of adjacent zones;
- d. the adequacy and capacity of available or programmed development infrastructure to accommodate the proposed activity; including:
  - i. opportunities for low impact design principles;
  - ii. management of three waters infrastructure and trade waste;
- e. managing natural hazards;
- f. the adequacy of roading infrastructure to service the proposed activity;
- g. any adverse effects on historic heritage and cultural values, natural features and landscapes or indigenous biodiversity, and
- h. any historical, spiritual, or cultural association held by tangata whenua, with regard to the matters set out in Policy TW-P6.

## 9.2 Regional Policy Statement for Northland [RPS]

An assessment of the relevant objectives and policies associated with the RPS for Northland has been undertaken and is also found in tables below. The RPS sets region wide objectives and policies for the environment.

#### Table 12 - RPS Assessment

Objective / Policy	Assessment
--------------------	------------

Integrated Catchment Management	Not relevant		
Region Wide Water Quality	Not relevant		
Ecological Flows and Water Quality	Not relevant		
Indigenous Ecosystems & Biodiversity	There are no SNA's on the site.		
Enabling Economic Wellbeing	There is economic benefit and job growth through the construction aspects of the project.		
Economic Activities – Reverse Sensitivity And Sterilization	The proposal does not result in any more than minor reverse sensitivity or sterilization effects.		
Regionally Significant Infrastructure	The proposal does not impact any regionally significant infrastructure and contains consultation with NZTA.		
Efficient and Effective Infrastructure	The proposal seeks to use existing infrastructure within the urban context.		
Security of Energy Supply	Power is already provided to the site to and will service the proposed dwellings.		
Use and Allocation of Common Resources	Not relevant.		
Regional Form	The proposal does not result in any more than minor reverse sensitivity effects, or a change in character or sense of place.		
Tangata Whenua Role in Decision Making	Council may send this application to relevant hapū or iwi if considered appropriate to do so to fulfil their obligations.		
Natural Hazard Risk	All natural hazard risks have been considered and appropriately mitigated.		
Natural Character, Outstanding Natural Features, Outstanding Natural Landscapes And Historic Heritage	Not relevant.		

Having considered the relevant components of the RPS, it is concluded that the proposal is not inconsistent with the relevant objectives and policies.

## 9.4 National Policy Statements and Environmental Standards

With respect to the National Environmental Standard – Soil Contamination, this is not considered relevant as no such uses have been associated with the site that is on the HAIL.

In terms of the National Environmental Standard for Freshwater, there are no known natural wetland areas on the site or the surrounds that are subject to assessment under it.

The site is not subject to the National Policy Statement for Highly Productive Land due to its existing soil class.

The Far North District is classified as Tier 3 under the National Policy Statement on Urban Development. It is considered that this development is an efficient use of land proposed to be zoned Mixed Use under the PDP, contributing towards a well-functioning urban environment.

There are no other relevant National Policy Statements or Environmental Standards.

#### 9.5 Conclusion

The above assessment finds that the proposal is not inconsistent with relevant statutory and higher order objectives and policies.

## 10.0 S104D ASSESSMENT

As a Non-Complying Activity, the application must pass at least one of the 'gateway tests' set out in Section 104D of the RMA before Council can consider granting consent. The two tests are:

- The adverse effects of the activity on the environment will be minor (or less than minor); or
- The application is for an activity that will not be contrary to the objectives and policies of the relevant plan.

#### **Adverse Effects Assessment**

The assessment of effects in Section 7.0 of this report demonstrates that the adverse effects of the proposal will be no more than minor. The receiving environment is an urban-fringe location characterized by light industrial and commercial activities, physically severed from the wider rural hinterland by the Waiomio Stream and roading infrastructure.

Detailed modelling confirms the proposal achieves hydraulic neutrality. The use of a 525mm negative-grade pipe and raised floor levels (RL 7.00m) ensures that flood risk is mitigated for residents and not transferred to third parties.

The addition of 30 residential units is supported by available infrastructure capacity. Traffic generation is compatible with the capacity of Old Whangae Road, and the site has access to reticulated services which will be upgraded as part of the works.

The design utilises a layout with significant landscaping (50% coverage) to soften visual dominance, ensuring the built form is compatible with the mixed-use character of the immediate area.

The adverse effects are effectively mitigated by the engineering design and site layout.

### **Objectives and Policies Assessment**

Case law has established that for an activity to be 'contrary' to objectives and policies, it must be 'repugnant to' or 'directly opposed to' the policy framework, rather than simply non-complying.

The site is split zoned, and the area of the proposed development is technically Rural Production in the ODP. The literal application of the zone's objectives must be balanced against the physical reality of the site. Council promotion of the site through the PDP signals a clear shift in the planning direction for this specific site, rezoning it to Mixed Use. Hearings are now complete and the site has not been subject to a rezoning request, establishing that its promoted rezoning is not challenged.

The PDP explicitly identifies this zone as a focal point for activity. The proposal directly supports these objectives by providing the residential density necessary to support the vitality of the nearby Kawakawa town center.

Given the advanced stage of the PDP and the clear anomaly of the current ODP zoning, more weight should be placed on the PDP direction. The proposal is entirely consistent with the Mixed Use objectives.

The proposal is not repugnant to the relevant objectives and policies. It aligns with the future direction Council promotes through the PDP and does not offend the underlying intent of the ODP's rural protection provisions given the site's specific non-productive characteristics.

It is considered that the proposal passes both the adverse effects test (s104D(1)(a)) and the objectives and policies test (s104D(1)(b)). Accordingly, the Council has the jurisdiction to consider and grant the application under Section 104B of the RMA.

## 11.0 PART 2 ASSESSMENT

### 11.1 Section 5 - Purpose of the RMA

Section 5 in Part 2 of the RMA identifies the purpose as being the sustainable management of natural and physical resources. This means managing the use of natural and physical resources in a way that enables people and communities to provide for their social, cultural and economic well-being which sustain those resources for future generations, protecting the life supporting capacity of ecosystems, and avoiding remedying or mitigating adverse effects on the environment.

It is considered that proposal represents Part 2, Section 5 of the RMA.

## 11.2 Section 6 - Matters of National Importance

In achieving the purpose of the RMA, a range of matters are required to be recognised and provided for. This includes:

- a) the preservation of the natural character of the coastal environment (including the coastal marine area), wetlands, and lakes and rivers and their margins, and the protection of them from inappropriate subdivision, use, and development:
- b) the protection of outstanding natural features and landscapes from inappropriate subdivision, use, and development:
- c) the protection of areas of significant indigenous vegetation and significant habitats of indigenous fauna:
- d) the maintenance and enhancement of public access to and along the coastal marine area, lakes, and rivers:

- e) the relationship of Maori and their culture and traditions with their ancestral lands, water, sites, waahi tapu, and other taonga:
- f) the protection of historic heritage from inappropriate subdivision, use, and development:
- g) the protection of protected customary rights:
- h) the management of significant risks from natural hazards.

In context, the relevant items to the proposal have been recognised and provided for.

#### 11.3 Section 7 - Other Matters

In achieving the purpose of the RMA, a range of matters are to be given particular regard. This includes:

- (a) kaitiakitanga:
- (aa) the ethic of stewardship:
- (b) the efficient use and development of natural and physical resources:
- (ba) the efficiency of the end use of energy:
- (c) the maintenance and enhancement of amenity values:
- (d) intrinsic values of ecosystems:
- (e) [Repealed]
- (f) maintenance and enhancement of the quality of the environment:
- (g) any finite characteristics of natural and physical resources:
- (h) the protection of the habitat of trout and salmon:
- (i) the effects of climate change:
- (j) the benefits to be derived from the use and development of renewable energy.

These matters have been given particular regard through the design of the proposal.

## 11.4 Section 8 - Treaty of Waitangi

The Far North District Council is required to take into account the principles of the Treaty of Waitangi when processing this consent. This consent application may be sent to local lwi and hapū who may have an interest in this application.

#### 11.5 Part 2 Conclusion

Given the above, it is considered that the proposal meets the purpose of the RMA.

## 12.0 CONCLUSION

A Non Complying resource consent is sought from the Far North District Council to carry out a multi unit development including subdivision in the Rural Production Zone of the ODP and Mixed Use Zone of the PDP.

The proposal is considered to result in less than minor effects on the environment and through assessment, there are no more than minor effects to persons.

The proposal is not considered contrary to the objectives and policies of both District Plans, and clearly aligns with Councils intent and promotion of this site as Mixed Use zone through the PDP.

The proposal is consistent with the Regional Policy Statement for Northland and achieves the purpose of the RMA.

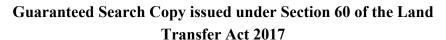
Relevant NPS' and NES' have been considered with the proposal finding consistency with their general aims and intent.

Regards,		
Steven Sanson		
Consultant Planner		



# RECORD OF TITLE UNDER LAND TRANSFER ACT 2017 FREEHOLD









**Part-Cancelled** 

Identifier NA523/225

Land Registration District North Auckland

**Date Issued** 12 June 1930

**Prior References** 

DI 1E 505 DI 1E 516 NA417/224

**Estate** Fee Simple

Area 7537 square metres more or less Legal Description Lot 92, 98 Deeds Plan W 46

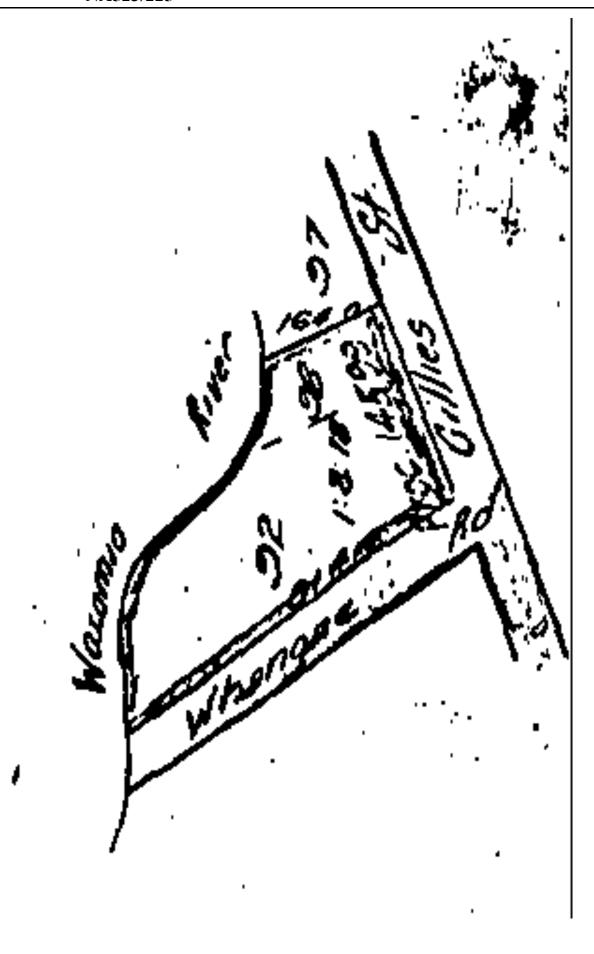
**Registered Owners** 

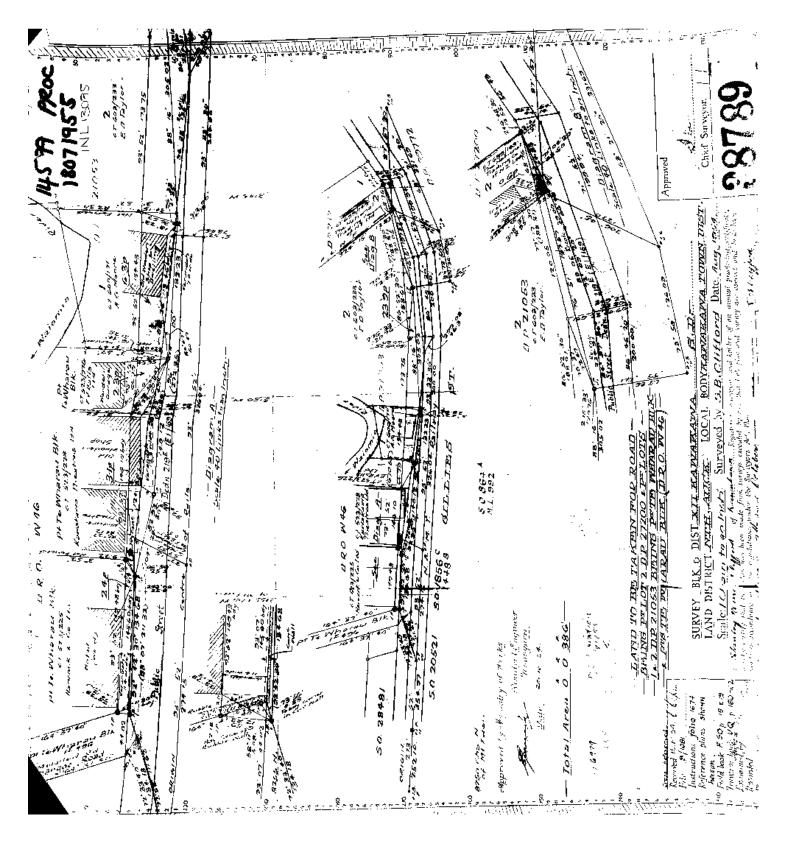
Far North Holdings Limited

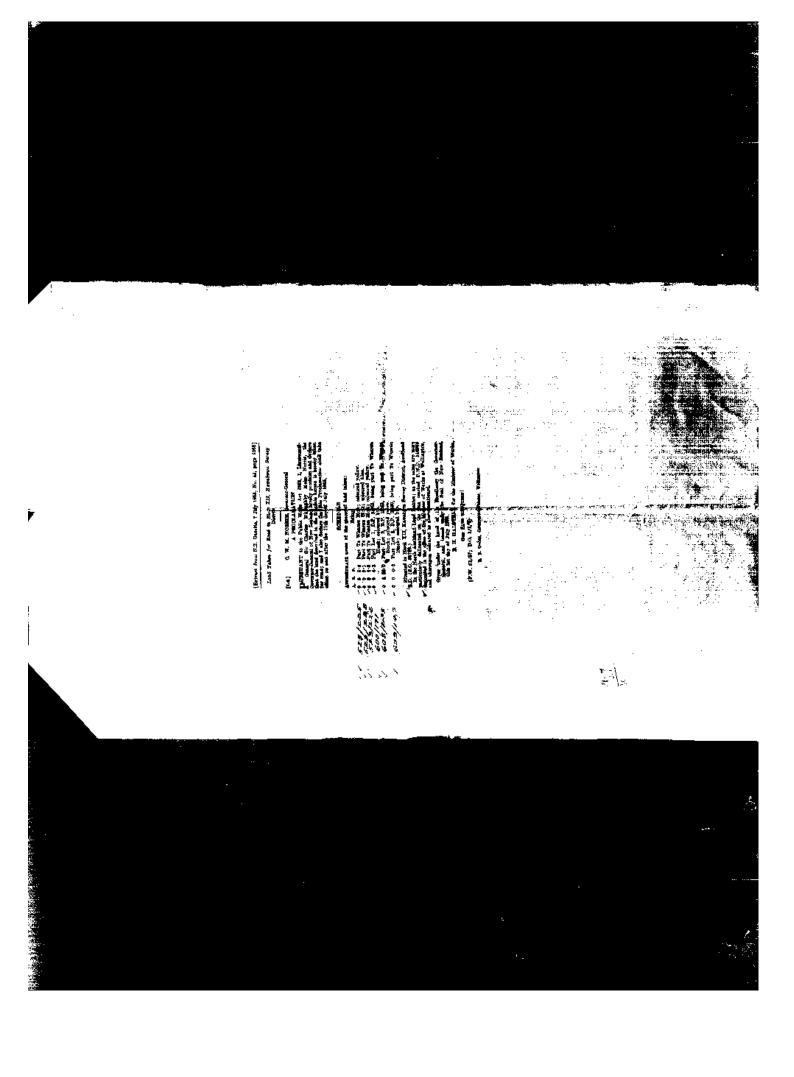
#### **Interests**

14599 Proclamation taking part for road - 18.7.1955 at 2.00 pm

Subject to a drainage right (in gross) over part in favour of Kawakawa Town District Council created by Transfer A290841 - 31.5.1968 at 10.00 am







0.70 m = 0.780 = 0.01.03

(Approved by the District Land Registrar, Auckland, No. 3360)

(Nem Zealand)

(C)

Under the Land Transfer Act, 1962

## Memorandum of Transfer

subject however to such encumbrances, liens and interests as are notified by memoranda underwritten or endorsed hereon in that piece of land situated in the Land District of North Auckland containing CHE ACRE THREE ROODS EIGHTEEN PERCHES (1s. 5r. 18p.)

more or less being Not 92 and 98 on Deeds Plan V.46 being part Te Marau Block and described in Certificate of Title Volume 523 Polio 225 (North Auckland Registry)

AND CHARAS the grantor in consideration of the Corporation hereinafter mentioned improving the disposal of stormwater in the vicinity of the grentor's land has agreed to transfer and grant to the Body Corporate called THE CHAIRLIN COUNCIALORS AND DIFFERED of THE TOWN DISPRICE OF MANAGEMYA (hereinafter with its successors and assigns referred to to so and included in the term "the Corporation") an easement in and over that portion of the land above described coloured yellow on the plan annexed hereto and thereon marked \*\*\*\*\*\* assement 8 ft. wide" (hereinafter called "the said land") for the conveyance of water whether rain tempest spring scakage or scepage water for the disposal thereof in such manner as the Corporation shall determine FOW THIS LEMCRANDUM CF TRANSMED WIAMESSMIH that in pursuance of the said agreement and for the consideration aforesaid the Grantor DOTH HERDBY TRANSFER AND GRANT unto the Corporation as an easement in gross full, free and uninterrupted right, . Liberty and privilege-for all times beneafter to take convey lead drain, and discharge water whether rain tempest spring scakage or scepage water in any quantities through in and under the said land and for such purposes and from time to time to construct lay place extend maintain alter repair and renew a drain or drains with a line or lines of pipes and conduits with or without manholes of such internal and external dirensions and with such valves surface boxec and descrits as the Corporation shall think fit through or under the said land at such a depth as the Corporation shall think fit with power and authority for the Corporation its surveyors engineers employees contractors workmen agents servands and all persons authorised by it with or without horses carts and other vehicles and machinery implements tools pipes and materials of any kind from time to time and at all times to enter and remain upon the said land for the purposes aforesaid (including opening up the soil for inspection or cleaning the said drains pipes and cesspits and

generally to do and perform such acts and things in and upon the said land as may be necessary or proper for or in relation to any of the purposes aforesaid AND the grantor and the Corporation <u>HEREBY COVENANT AND AGREE</u> the one with the other of them as follows:-

- 1. That all works authorised to be carried out hereunder shall be carried out as expeditiously as possible and with as little disturbance to the surface of the said land as possible and immediately upon the completion of any such work the surface of the land shall be restored as nearly as possible to its original condition.
- 2. THAT the Corporation will from time to time repair and make good all damage to fences gates drains paths or driveways upon the said land caused by the carrying out by the Corporation of any of the works hereinbefore mentioned.
- 3. That the granter will not place any buildings erections or fences on the said land or any part thereof and will not at any time hereafter do or permit or suffer any act whereby the rights powers licences and privileges hereby granted to the Corporation may be interfered with or affected or whereby the passage of water through the said pipes and conduits as aforesaid may be in any way interrupted or restricted <u>FROVIDED ALMANS</u> this provision shall not affect any boundary fence between the land of the Grantor and any adjoining land.
- 4. THAT nothing herein contained or implied shall be deemed to compel the Corporation to conduct water through the said open drains pipes or conduits and the Corporation may discontinue such drainage and recommence such drainage at will.
- 5. THAT nothing herein contained shall be deemed to abrogate limit restrict or spridge any of the rights powers and remedies vested in the Corporation by any statute and in particular by "The Lunicipal Corporations Act 1954" and "The Public Works Act 1928" or any of them or any amendment thereof, or any act or acts passed in substitution therefor.
- 6. THAT the Corporation in addition to the right privileges and liberties herein contained shall also have the rights created by the Seventh Schedule to the Land Transfer act 1952.

IN WITHESS WHEREOF these presents have been executed this & day of day

of dtal 198
THE COLLOW SEAL OF HANCOCK

& CC. LI.IFED Vas hereunto

affixed in the partier

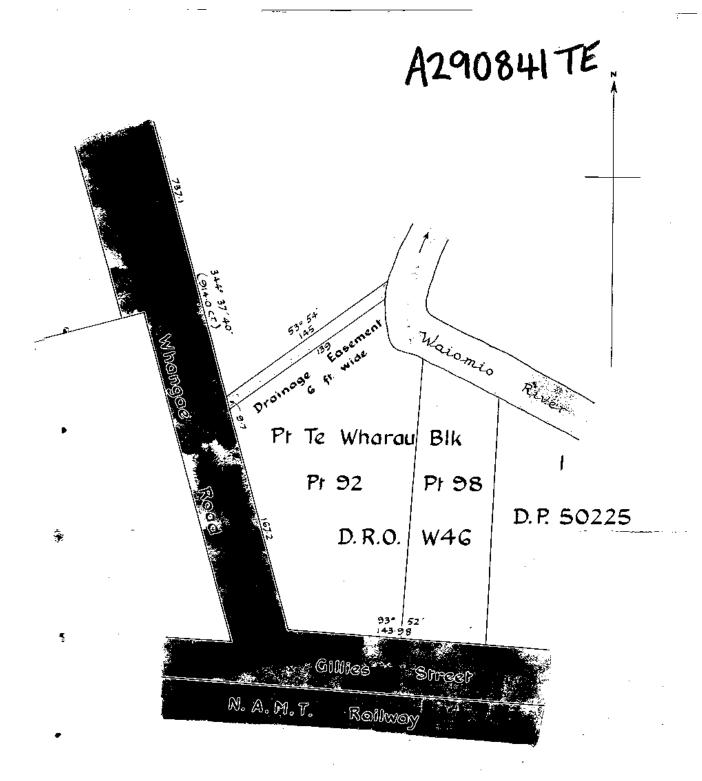
THE COLLON SHAP OF THE SCRY CORFORATE
called MAE CHAIRMAN COUNCILLORS AND
CITIZENS OF THE TOW. DISTRICT OF
HAWANA JA was pursuent to a resolution
of the Nawakawa Town Council passed
on the 8 day of 1958

hereunto affixed in the presence of :-

The Journ of Constraint of Con

\_CHATREAU

FOWN CLERK



Drainage Easement over Pt Te Wharau Blk
Blk XII Kawakawa S.D.
Kawakawa Town Dist.

Scale: 50 links to an inch

De la constantina della consta

In Consideration of

(the receipt of which sum is hereby acknowledged)

Do hereby Transfer to the said

 $\alpha$ ll

estate and interest in the

said piece of land above described

In witness whereof

have hereunto subscribed

name this

day of

Signed by the above named

in the presence of

No.

TRANSFER OF

GRAND OF HASELEND

Grantor

Correct for the purposes of the Land Transfer Act.

Solicitor for the Transferee.

TAWAKAMA POME COUNCIL

ALMOCOK & CC. INVITED

Grantee *Transferee* 

X Transferor

Particulars entered in the Register-Book Vol.

Folio

30 MAY 19

19

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Assistant Land Registrar

of the District of Auckland

Neturos
Firms Lockerya Ct
3 J MAY 1968
Times: /A
Foe: /A 1

RISETOT Abstract No. 3/09.
SCHUTTERS,
THANG. TEI.

Solicitors for the Transferee

THE LAW SOCIETY OF THE DISTRICT OF AUCKLAND
P.P.Co.lud.(5)—5883

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CT 523/225 prod

**(** 



LOCALITY MAP - LARGE SCALE

NTS@A1 HALF-SCALE@A3

DESTINATION	DISTANCE	TIME BY WALK
LOCAL TOWN CENTER	100M-500M	1-10 MIN
CULTURAL CENTER	300M	5 MIN
SPORTS / RECREATION	650M	10 MIN
CHURCH	400M	7 MIN
PRIMARY SCHOOL	450M	8 MIN
HIGH SCHOOL	1.4KM	20 MIN





SITE LOCATION

NTS@A1 HALF-SCALE@A3













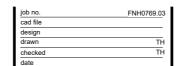












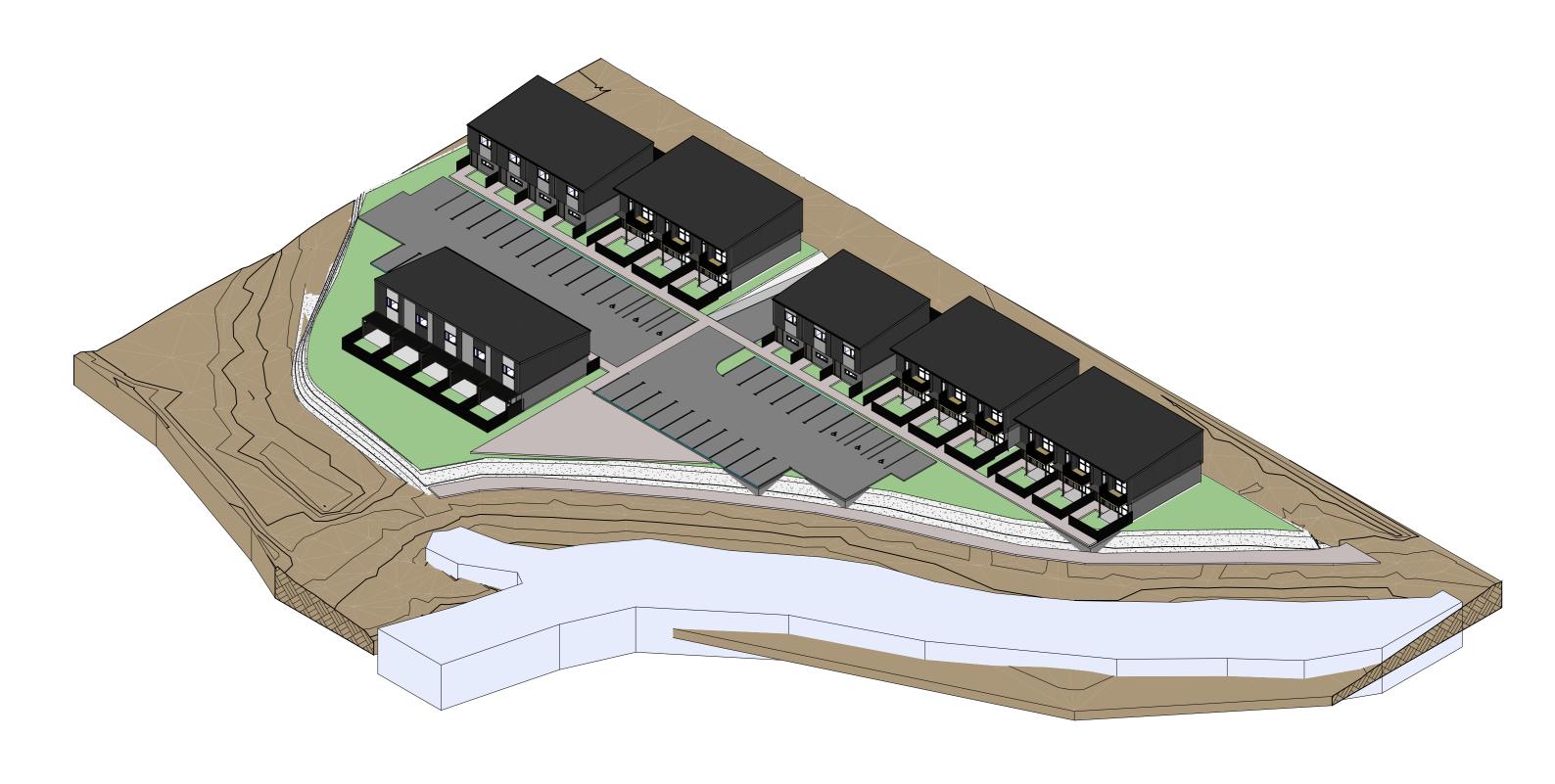
MEDIUM DENSITY HOUSING OLD WHANGAE RD, KAWAKAWA dwg title
VISUALS

RESOURCE CONSENT
scale

AS SHOWN@A1

COURCE CONSENT

AS SHOWN@A1
HALF-SCALE@A3









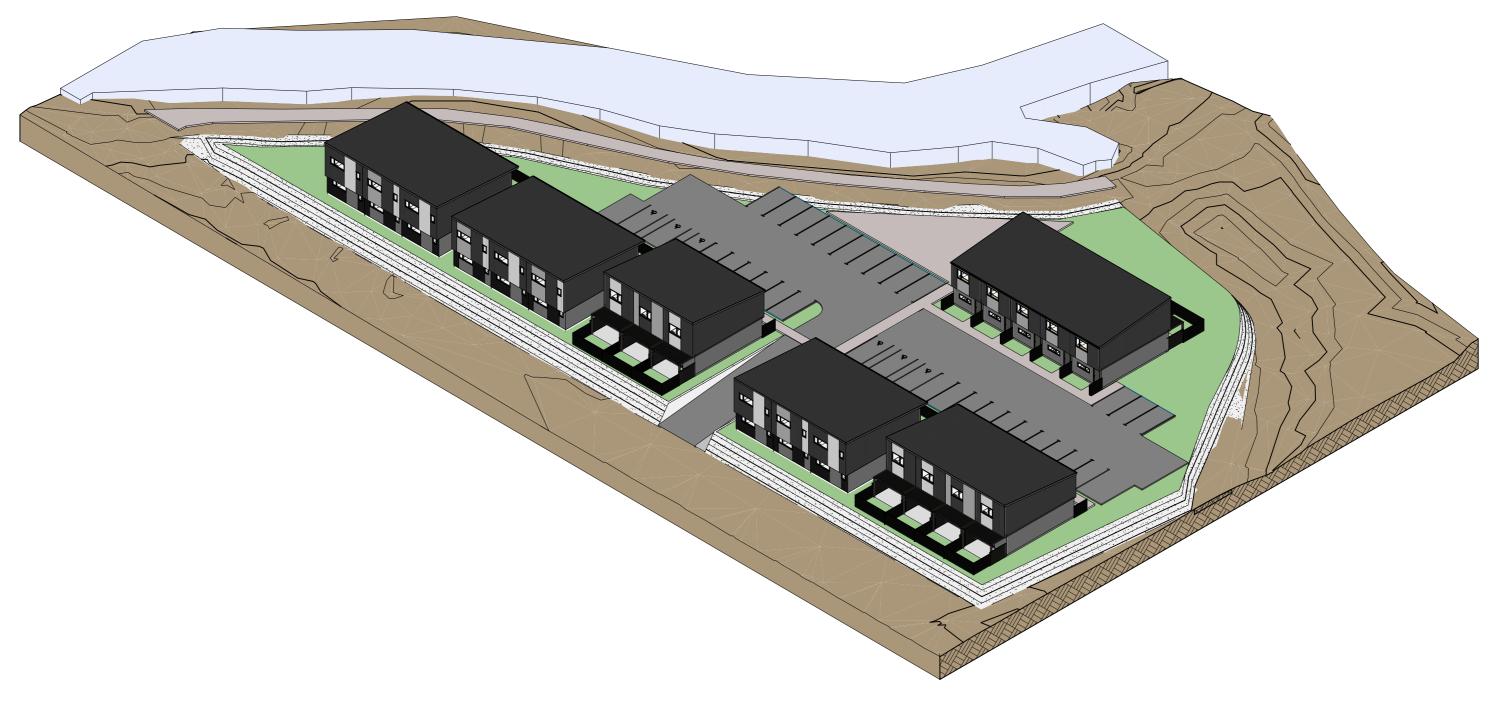










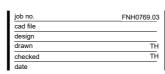












MEDIUM DENSITY HOUSING OLD WHANGAE RD, KAWAKAWA 3D OVERVIEW -MASTER PLAN status

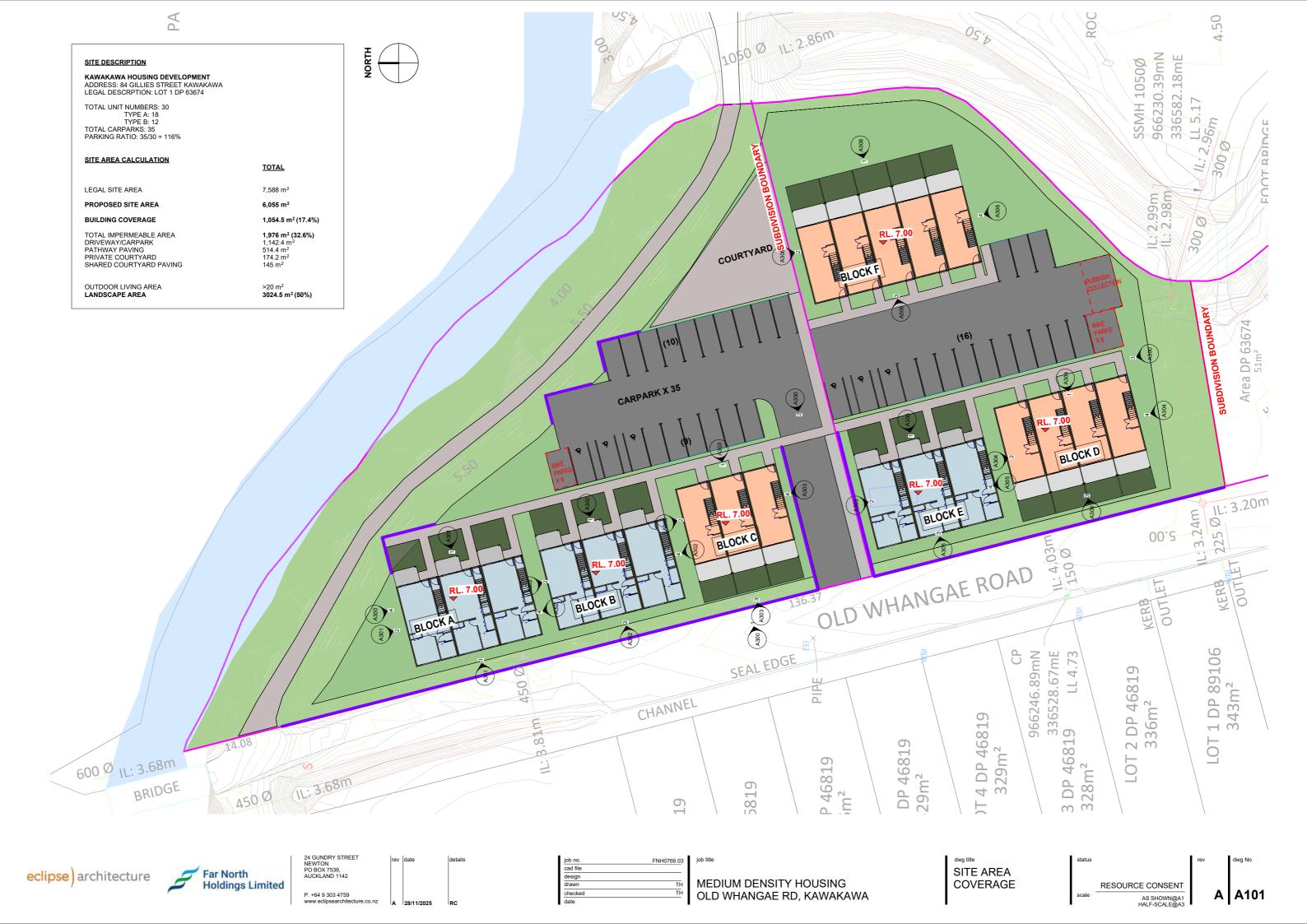
RESOURCE CONSENT

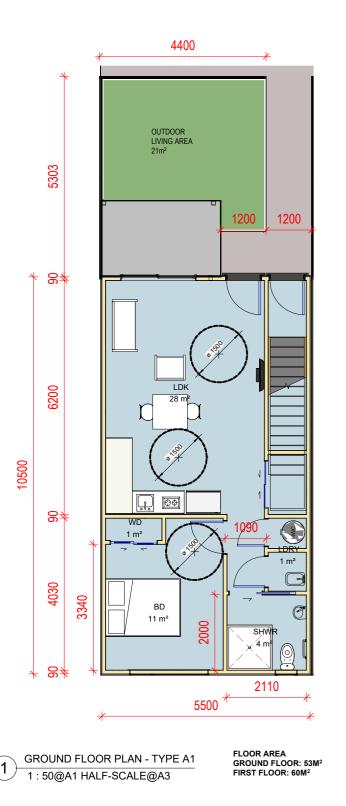
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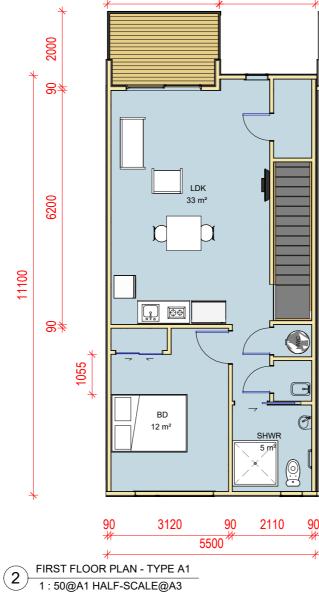
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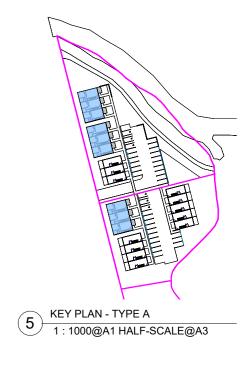








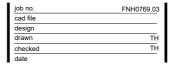




Parking	One carpark is provided per dwelling	YES
raikiliy	One carpaix is provided per dwelling	IES
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES
	Apartment complexes and multi-unit developments: Drop-off zone for customers 'use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	YES
	One path is at least 600mm wide between the dwelling and the clothesline	YE
	Where Timber landings and decks are provided, they are level entry.	YE
	All exterior doors have a clear opening width of at least 810mm.	YE
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YE
	There is step-free access from the main-entry to the main living-area.	YE
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YE
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YE
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YE
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YE
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YE
Fixtures and Fittings	To be compliant during BC Stage	YE
Finishes	To be compliant during BC Stage	YE

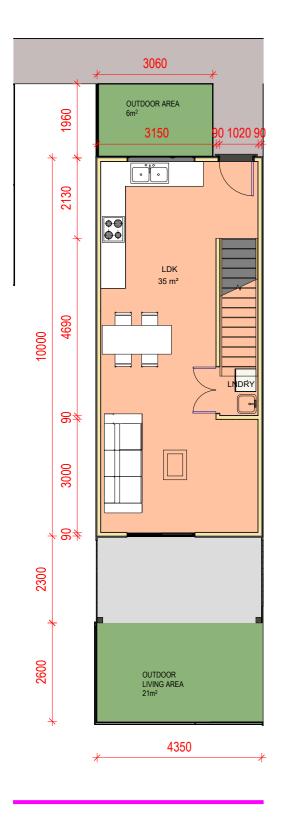


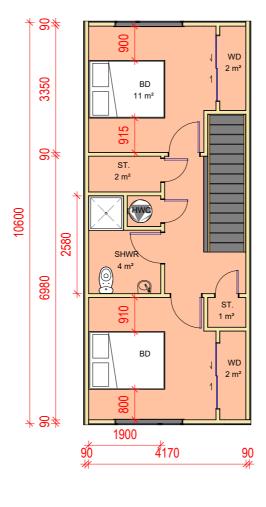












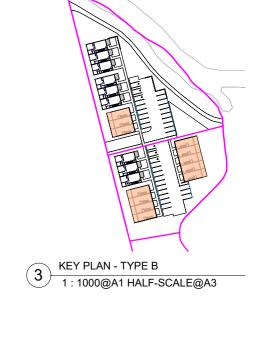
FLOOR AREA GROUND FLOOR:42M<sup>2</sup> FIRST FLOOR: 46M<sup>2</sup> TOTAL: 88M<sup>2</sup>

GROUND FLOOR PLAN - TYPE B

1:50@A1 HALF-SCALE@A3

PIRST FLOOR PLAN - TYPE B

1:50@A1 HALF-SCALE@A3



STANDARD UNIVERSAL DES	SIGN COMPLAINCE	
Parking	One carpark is provided per dwelling	YES
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES
	Apartment complexes and multi-unit developments: Drop-off zone for customers 'use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	YES
	One path is at least 600mm wide between the dwelling and the clothesline	YES
	Where Timber landings and decks are provided, they are level entry.	YES
	All exterior doors have a clear opening width of at least 810mm.	YES
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YES
	There is step-free access from the main-entry to the main living-area.	YES
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YES
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YES
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YES
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YES
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YES
Fixtures and Fittings	To be compliant during BC Stage	YES
Finishes	To be compliant during BC Stage	YES

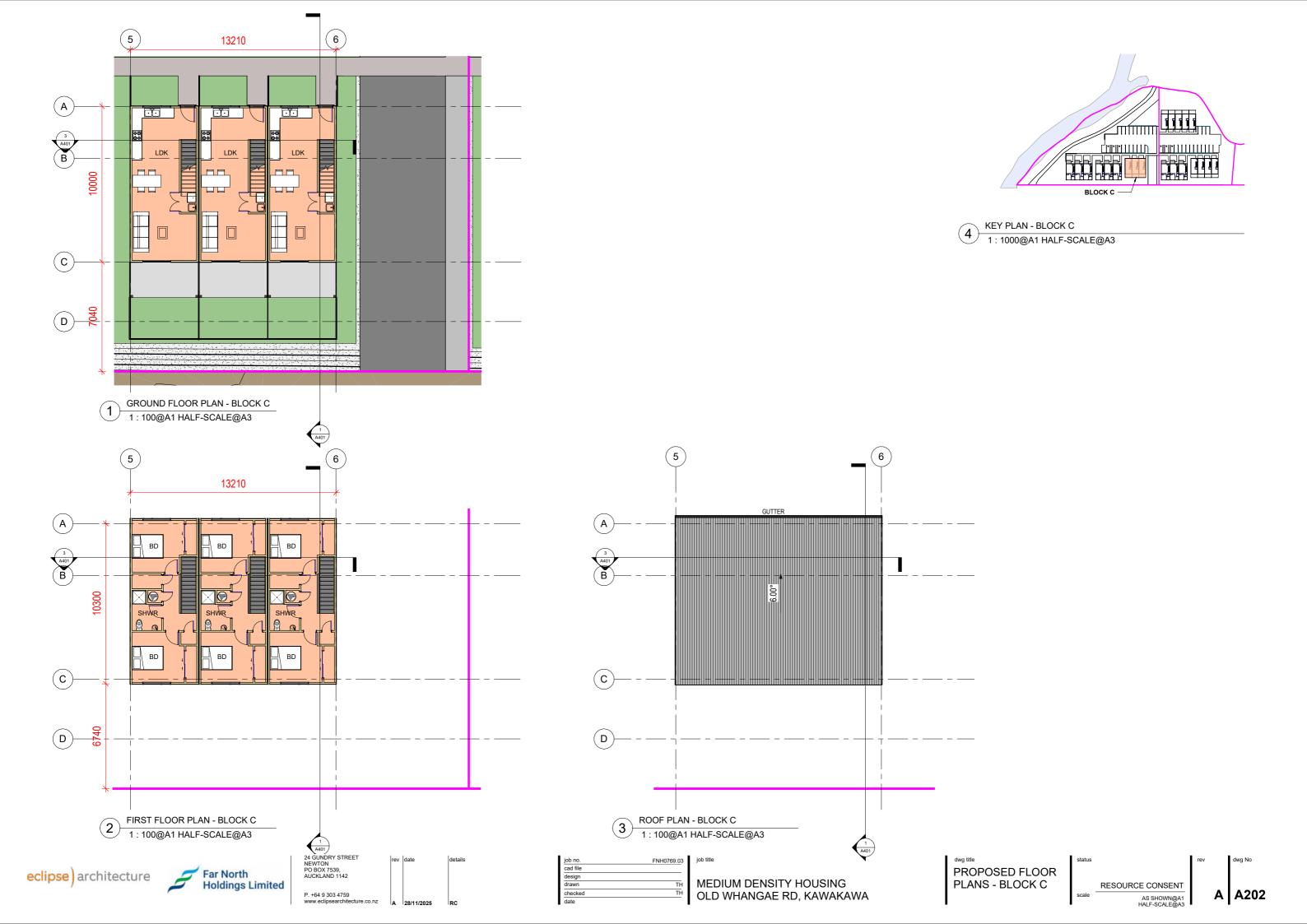


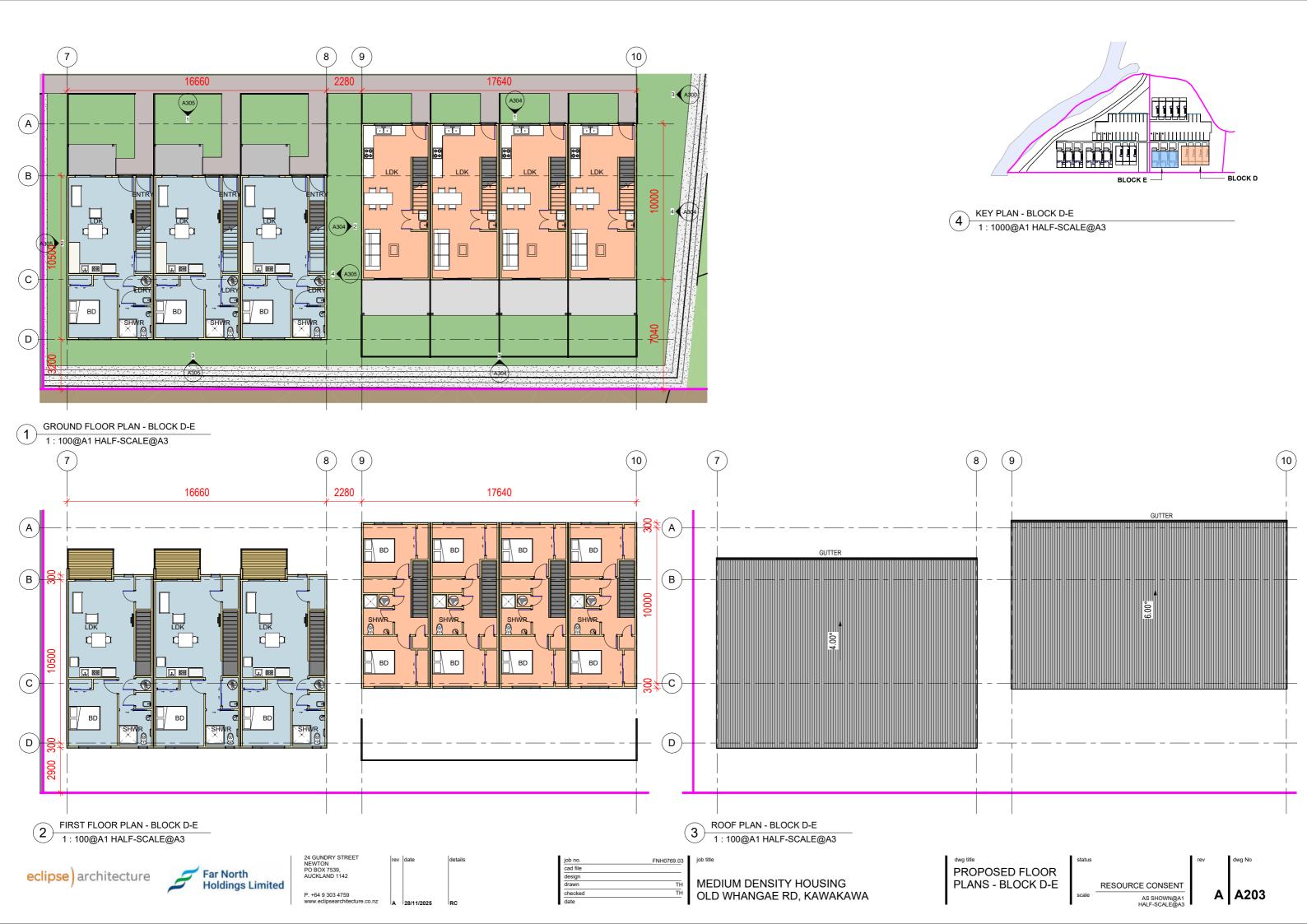


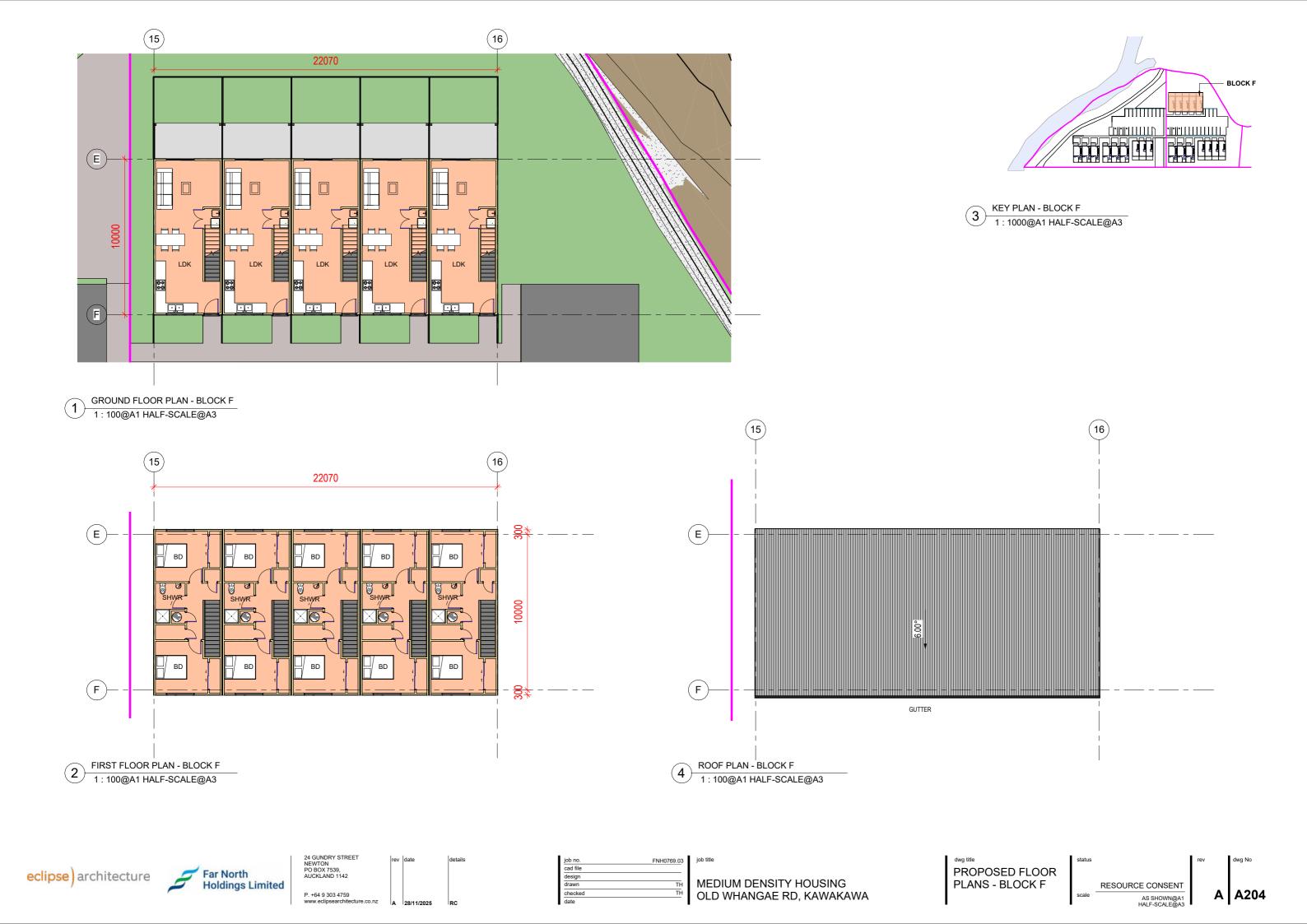


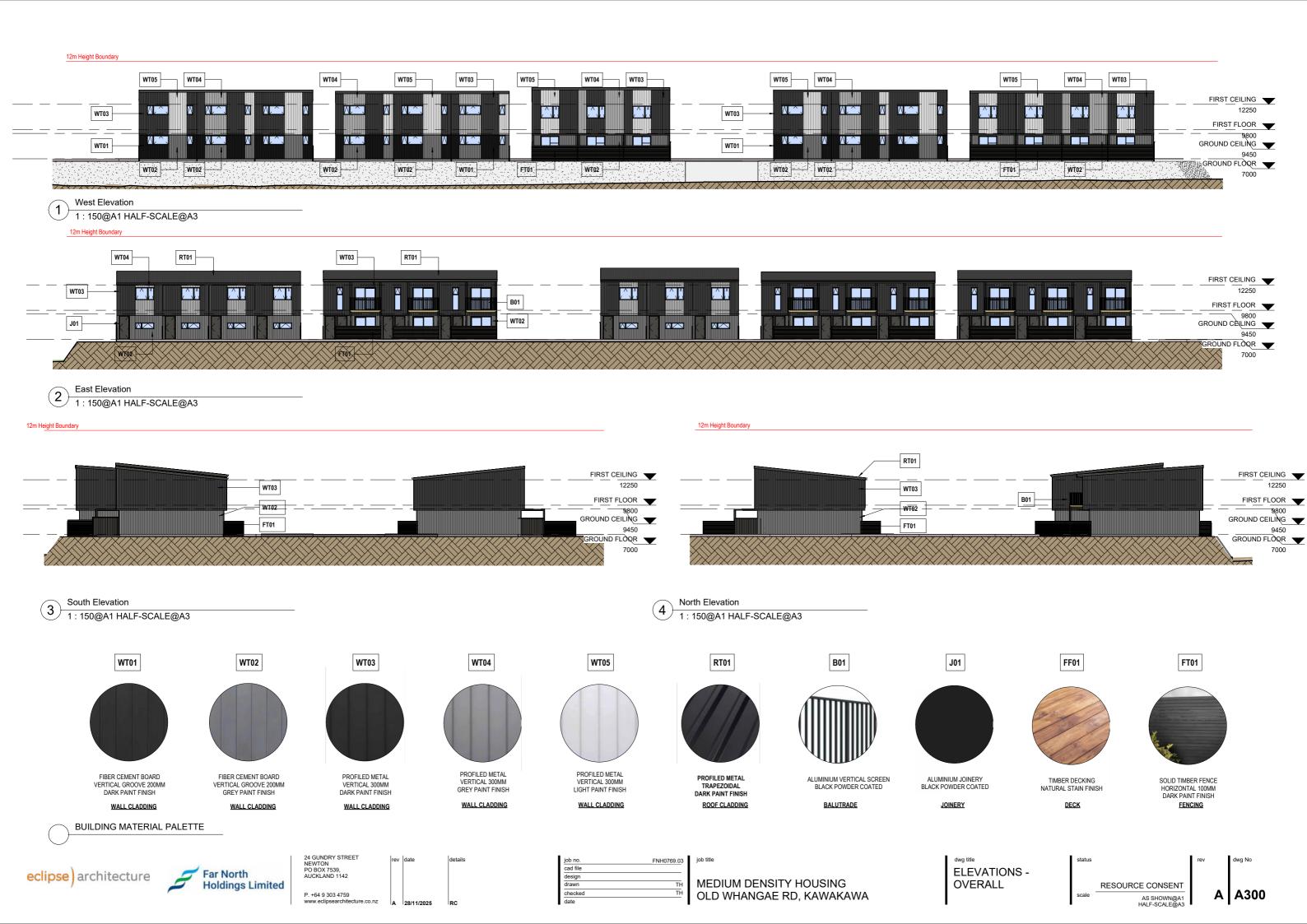


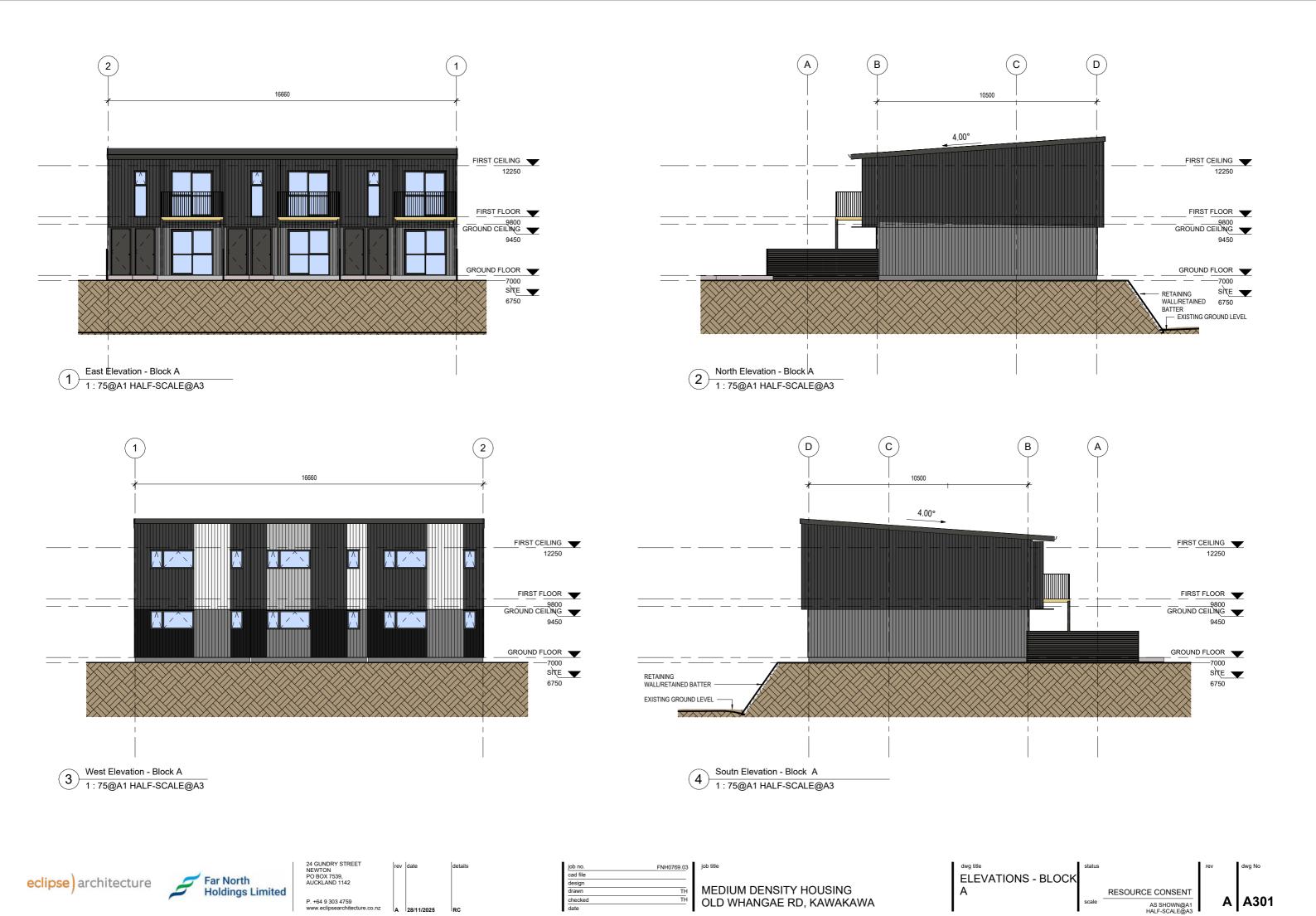


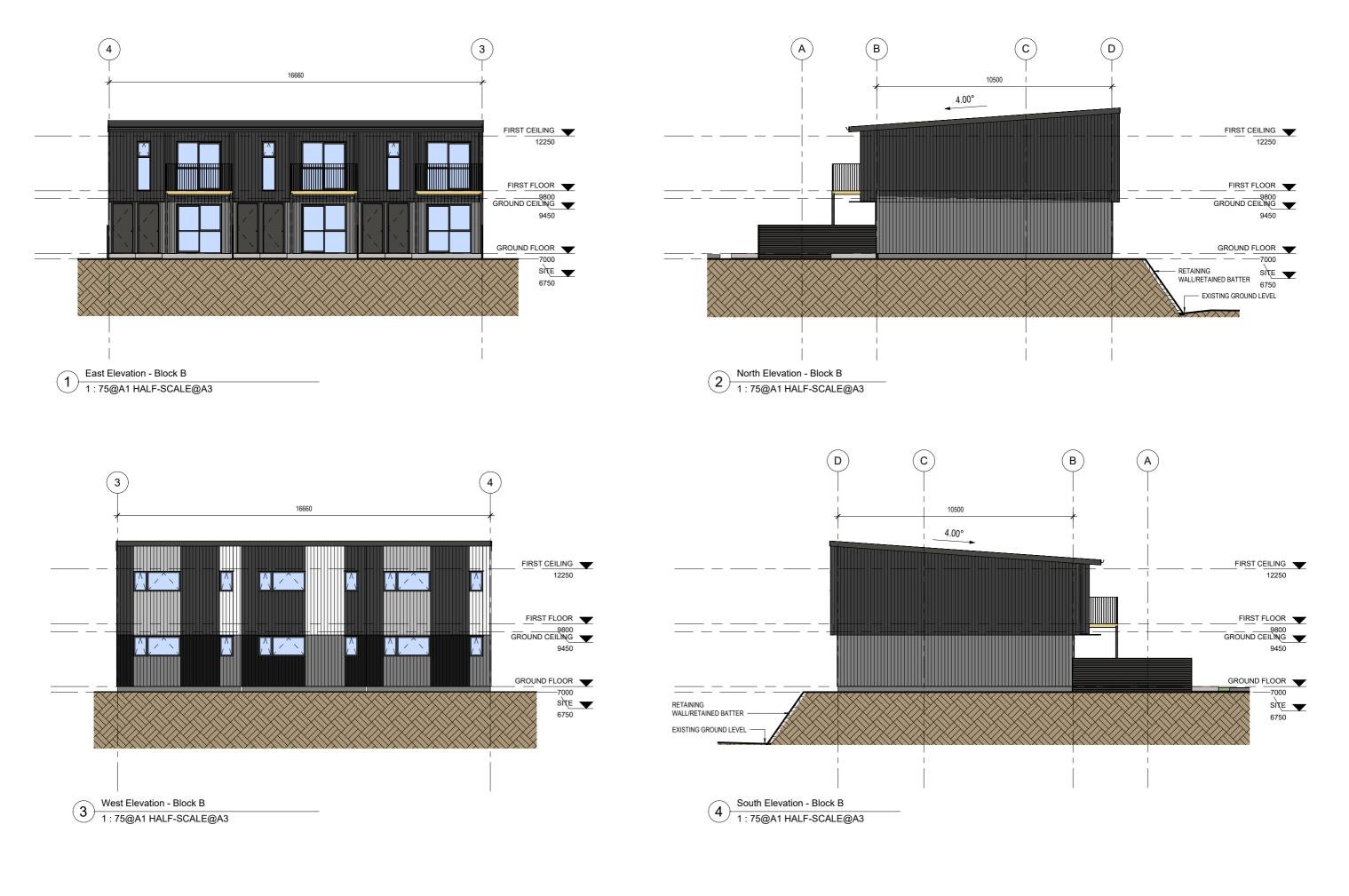










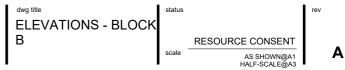


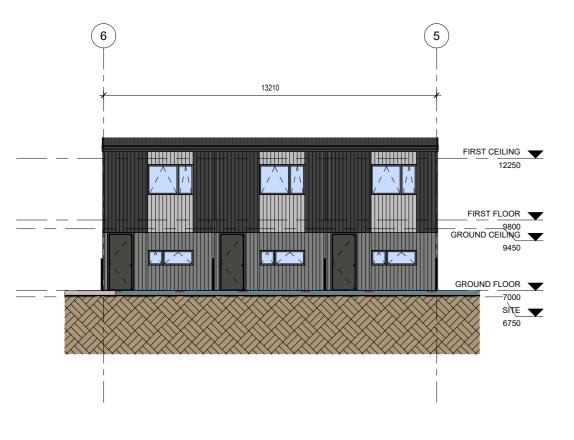




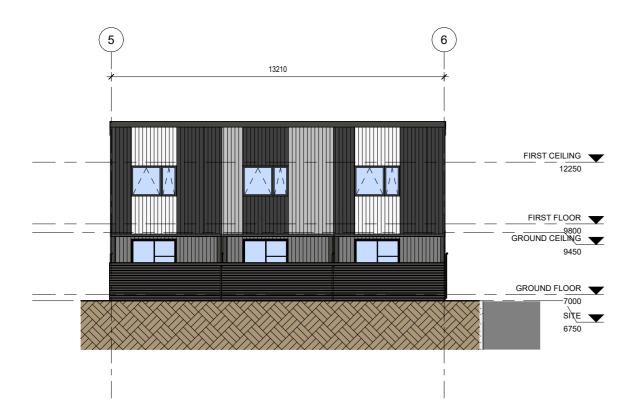








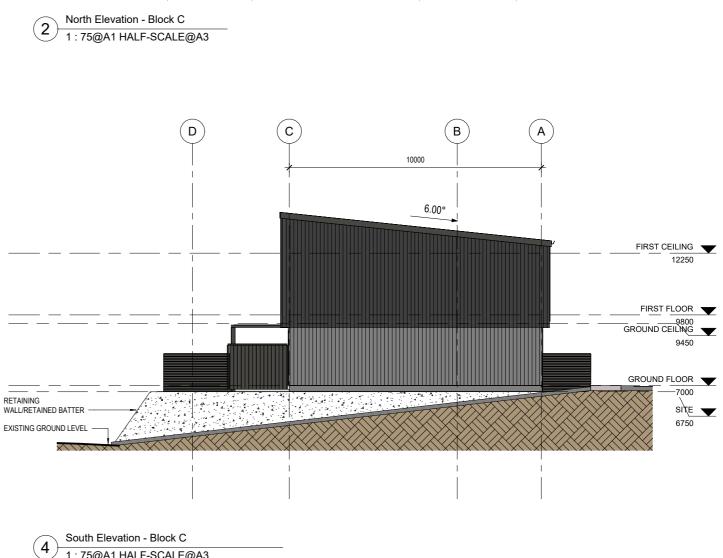
East Elevation - Block C 1 : 75@A1 HALF-SCALE@A3



West Elevation - Block C 3 1 : 75@A1 HALF-SCALE@A3



ELEVATIONS - BLOCK C RESOURCE CONSENT AS SHOWN@A1 HALF-SCALE@A3



(c)

(D)

FIRST CEILING 12250

FIRST FLOOR

GROUND CEILING

GROUND FLOOR

WALL/RETAINED BATTER 6750 - EXISTING GROUND LEVEL

RETAINING

SITE \_

(B)

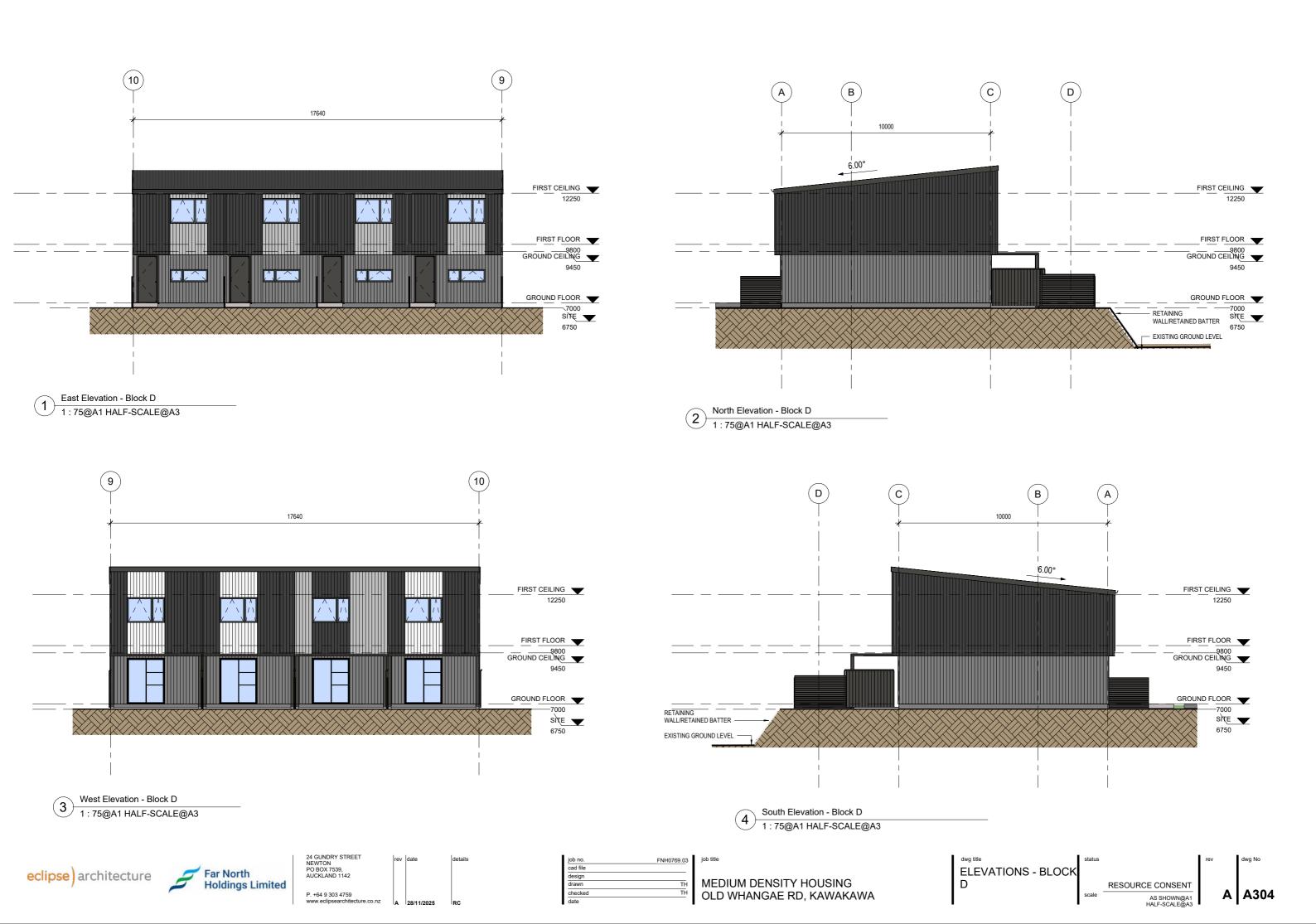
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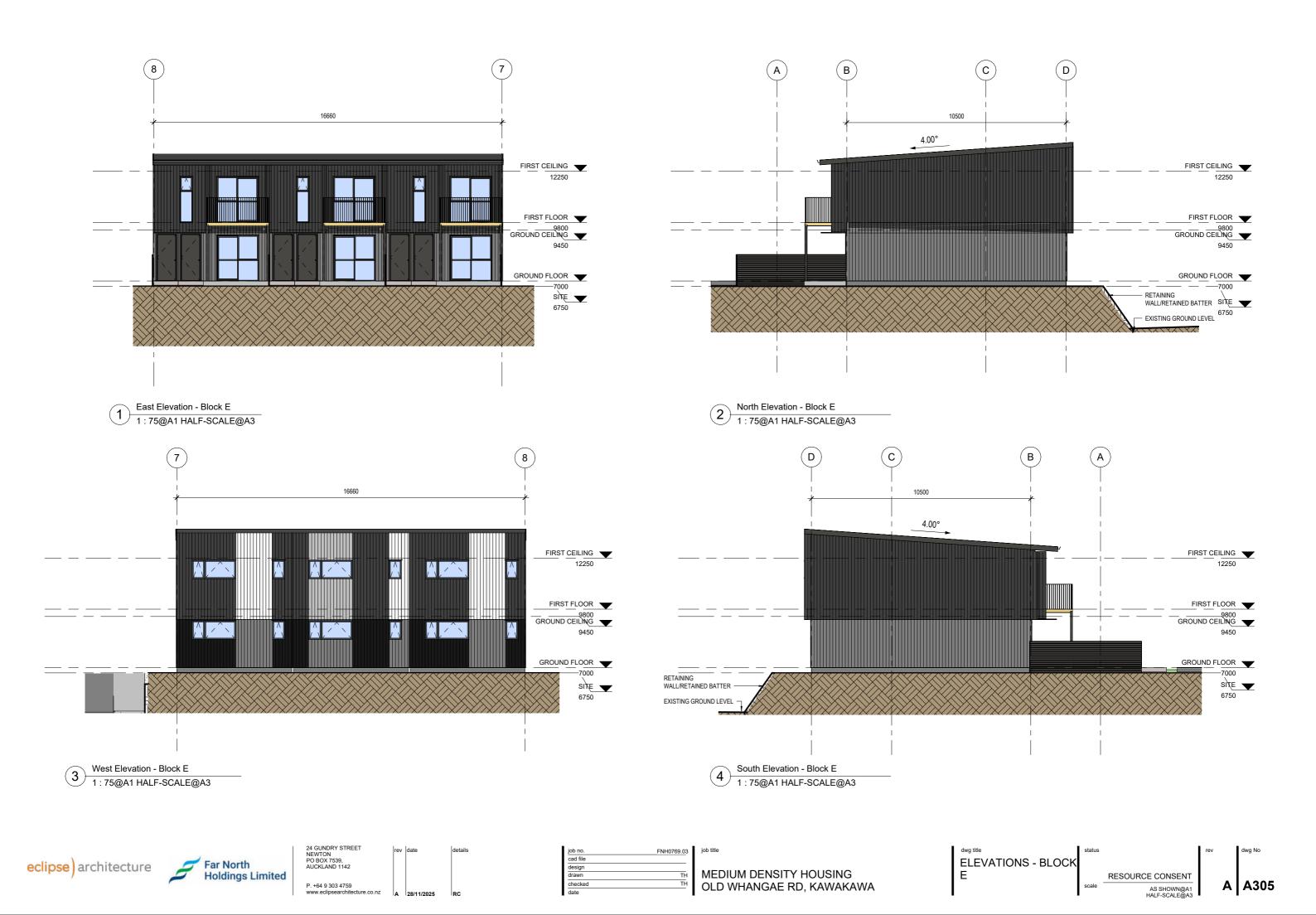
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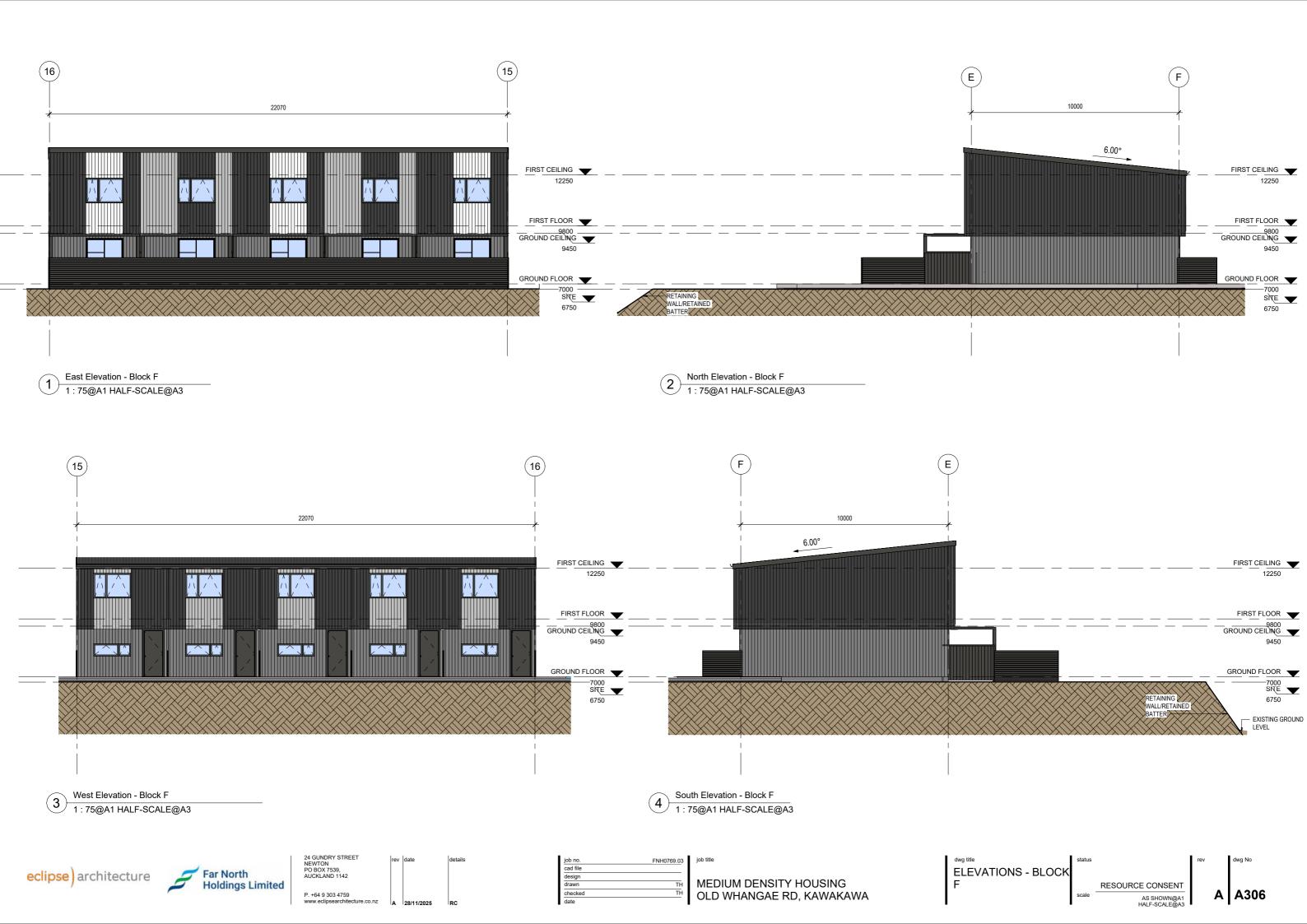


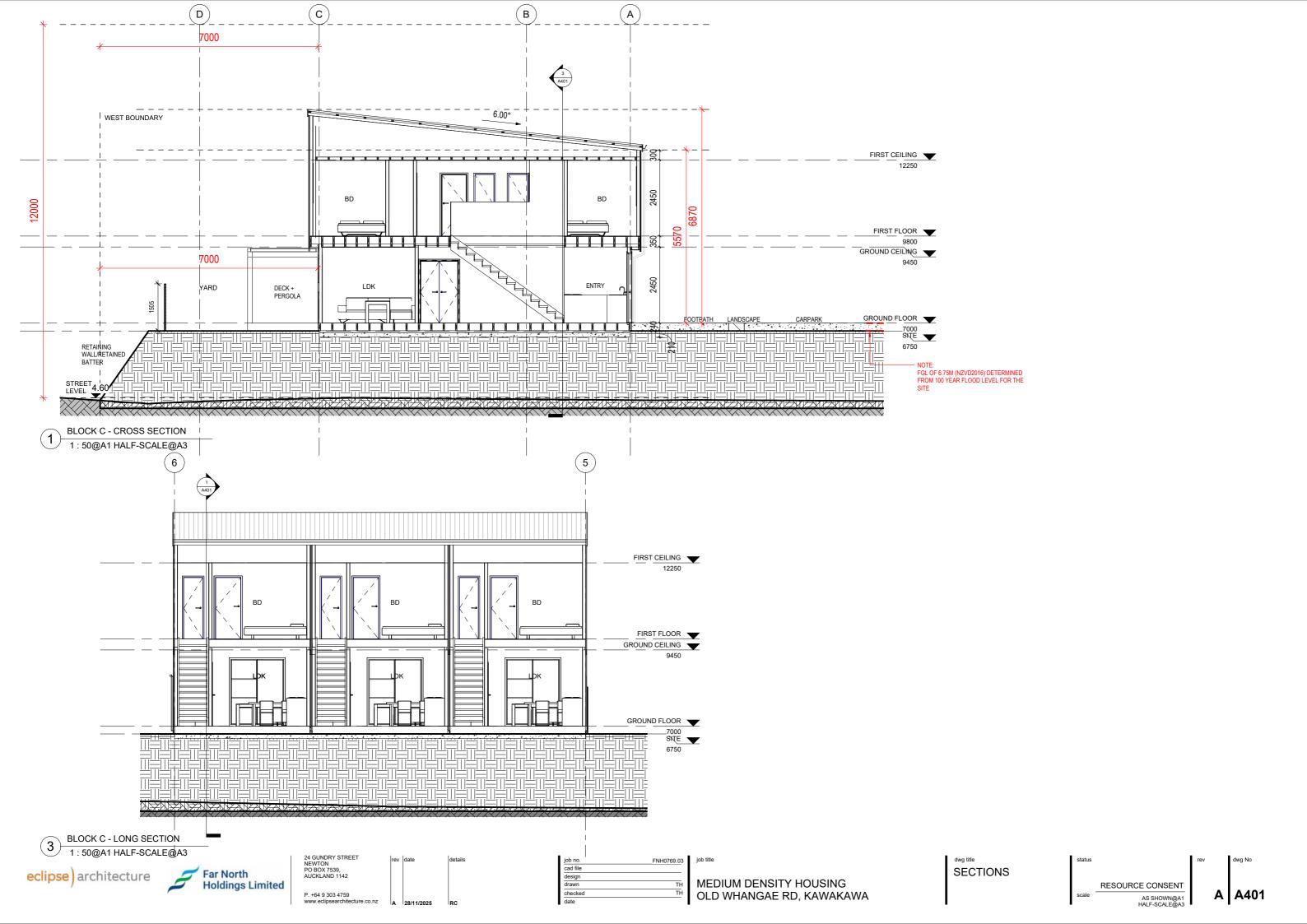


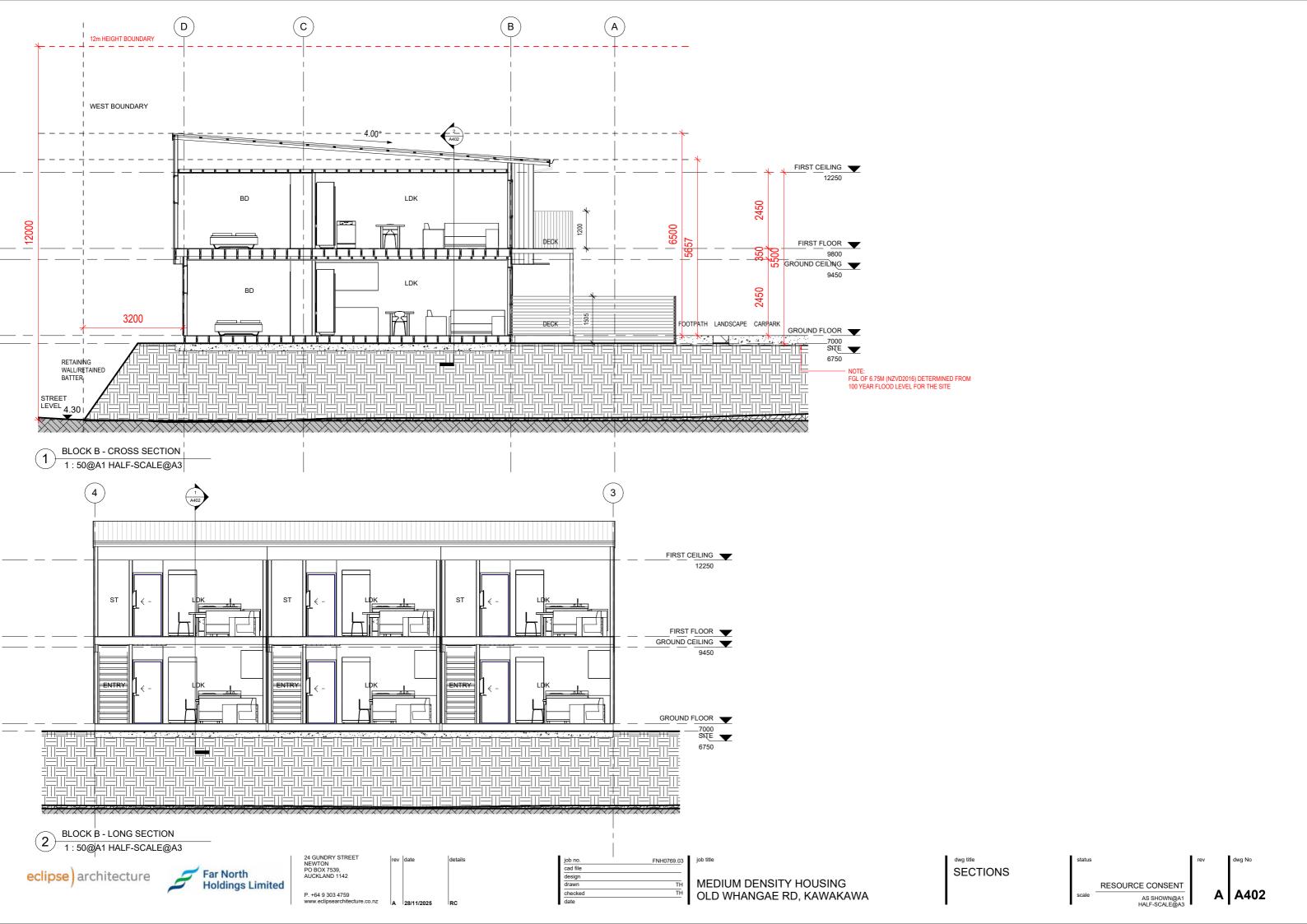
24 GUNDRY STREET NEWTON PO BOX 7539, AUCKLAND 1142 P. +64 9 303 4759 www.eclipsearchited

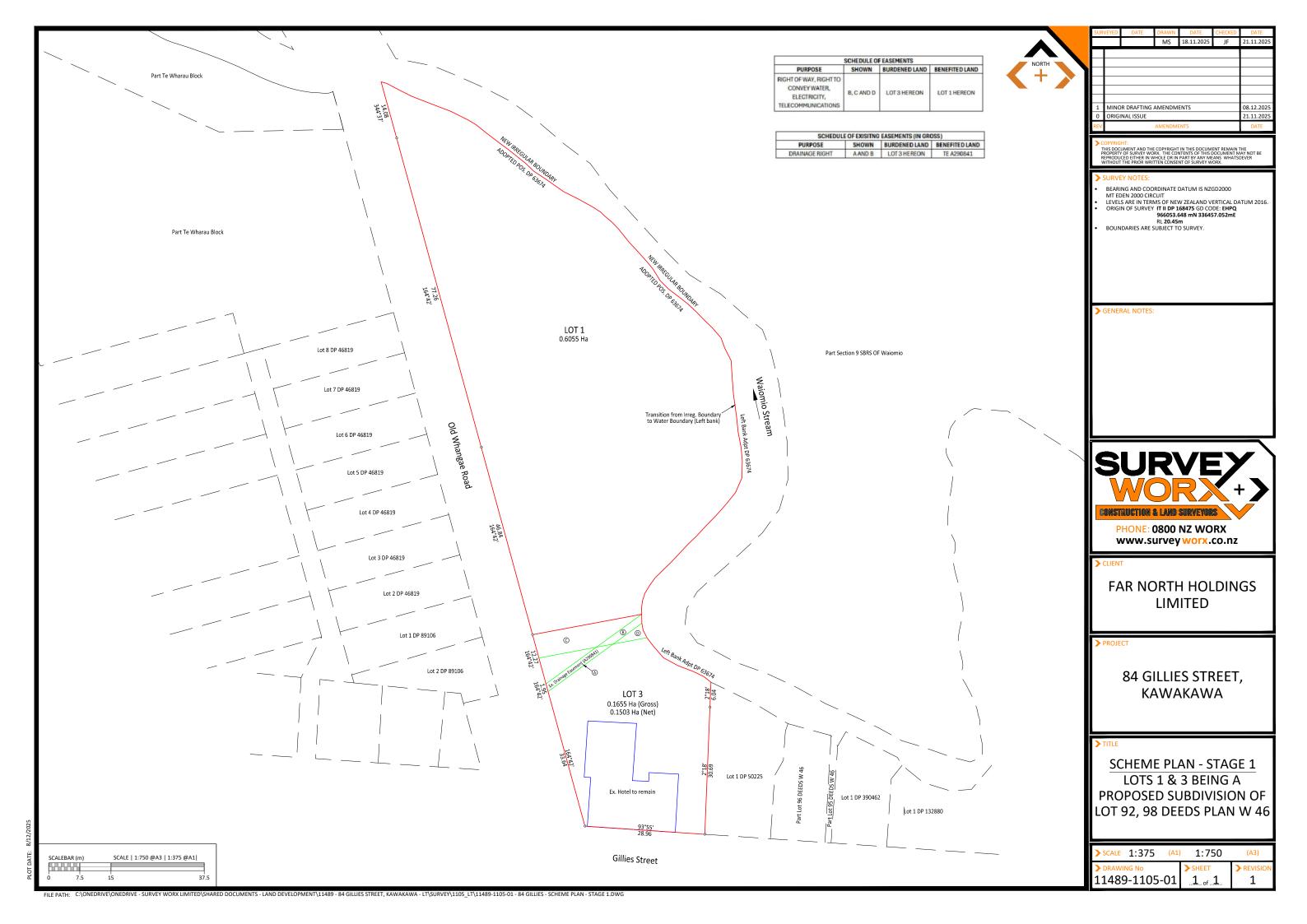


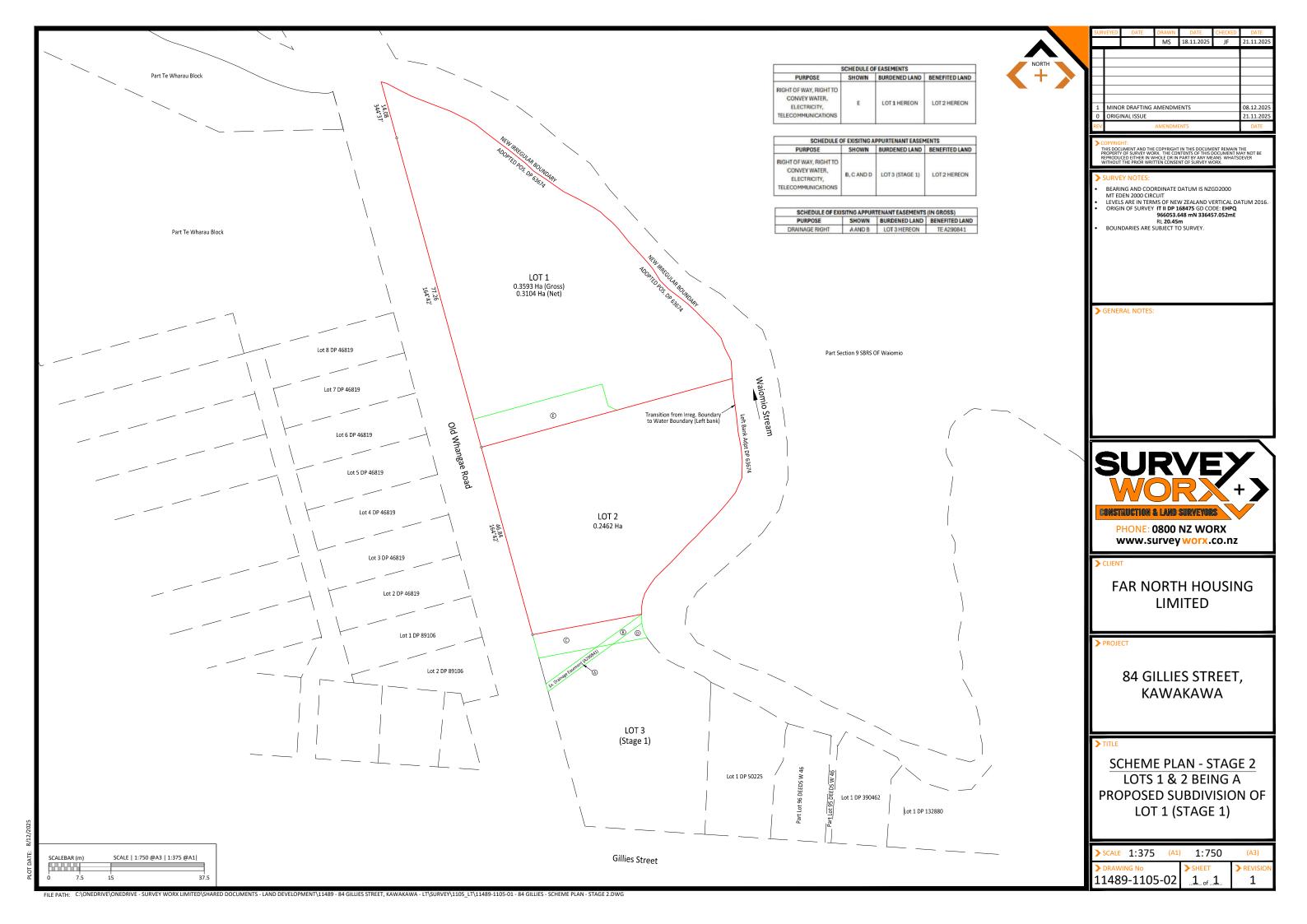














# **GEOTECHNICAL REPORT**

FOR
PROPOSED DEVELOPMENT
AT
LOT 1 DP 64674
OLD WHANGAE RD
FOR
FAR NORTH HOUSING LTD



Job No:	25-058
Date: Rev0	9/12/2025



Dec. 2025

Revision	Date of issue	Description
Rev 0	9/12/2025	ISSUED FOR CONSENT

Prepared By: <b>Jonty White</b>	Reviewed and Authorized By: Pradeep Kumar
aline	Runz
Engineering Geologist (BSc, Geology)	B.E hons, NZCE, MIPENZ, IntPE, CPEng. (Structural, Geotechnical)



### Geotechnical Report For Proposed Development At Old Whangae Rd, Kawakawa For Far North Housing Ltd

### Dec. 2025

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**APPENDIX B - Lab results, slope stability models** 

<u>APPENDIX C - Reference material and conceptual plans.</u>





### 1. EXECUTIVE SUMMARY

This report was requested by Far North Housing Ltd and has been prepared to assess the geotechnical aspects of LOT 1 DP 63674, Old Whangae Rd, Kawakawa for the proposed development.

This report assesses the site regarding, land stability, foundation requirements, earthworks, drainage and serviceability, and can be used to support resource and building consent applications to the local territorial authority. It has been prepared for the sole use of our client. It shall not be used, reproduced or copied in any manner or form without the permission of PK Engineering Ltd.

The subsoils on the site have been determined at discrete locations. It should be understood that soils away from those locations may vary from this report. We have construction monitoring and ground bearing capacity checks at the base of foundations to ensure the soil conditions are as per our geotechnical report.

It should be noted that if there is a change in the location of any of the buildings we should be given the chance to determine if further testing is required to prove the ground conditions and better recommend foundation design parameters.

We should be engaged during building consent stage to ensure that the foundations and stormwater/wastewater services for the developed designs are consistent with this report. Should there be any variation in the plans from what was stated in this report then would need to be engaged accordingly.

From our site investigations the subsoils on the site can be described as a stiff upper crust 1.5-3.0 metres deep with undrained shear strengths averaging 70kPa, overlying a 5.60-18.0-metre-thick layer of poorly consolidated saturated silty CLAY, with varying Peat quantities and undrained shear strengths generally less than 50kPa and often lower than 30kPa. At the base of the weak layer is solid rock formation of the Waipapa group. This above mentioned is typical of such landforms within this locality.

The client has provided us with conceptual plans which indicate the development of the relatively flat portion of the site adjacent to the local river, and within the flood plain. The concept plans are part of a stage of conceptual information co-ordinated over the past few years in order to develop the site sustainably with respect to the geotechnical hazards that are present. The plans indicate the client wishes to provide moderate density 2-storey apartment style buildings with carparking for residential housing, to meet the needs of the local residents.

The client has requested that we provide geotechnical recommendations to help them develop the site, which given the complexity of the geotechnical hazards present is crucial to obtaining a sustainable long-term design that is fit for purpose.







Figure 1: Site overview concept design by Far North Holdings Ltd.

A summary of the site classifications from our investigations and knowledge of the geotechnical requirements of the site have been provided in Table 1 below and described in more detail within this report.

Table 1: Executive Summary

<u> </u>		
Natural hazards maps	Flood Hazards identified	
Geological mapping	Tauranga Group and Waipapa Group	
	(Greywacke/argillite)	
Seismic subsoil class	Class C – NZS 1170.5 (2004)	
Earthquakes and tsunamis	Earthquake low risk & Tsunami no risk	
Liquefaction	Low Risk	
Settlement	High Risk (Not good Ground NZS3604:2011)	
Expansivity	Moderately Expansive (upper crust)	
Slope Stability	F.O.S within tolerable limits.	
Foundation type	Rib raft is recommended	
Engineered Fill	Requires specific design to account for differential settlements	
Retaining walls	Required to be designed by suitably chartered professional engineer.	
Drainage measures	Required for short term and long term	
Stormwater design	Flood modelling is critical to the finished levels.	





### 2. INTRODUCTION

This report was requested by Far North Housing Ltd and has been prepared to assess the geotechnical aspects of LOT 1 DP 63674, Old Whangae Rd, Kawakawa for the proposed development.

This report assesses the site regarding, land stability, foundation requirements, earthworks, drainage and serviceability, and can be used to support resource and building consent applications to the local territorial authority. It has been prepared for the sole use of our client. It shall not be used, reproduced or copied in any manner or form without the permission of PK Engineering Ltd.

### 3. DESKTOP STUDY

### 3.1 GENERAL SITE DESCRIPTION

The lot encompasses a land area of approximately 0.7588 hectares and is located in the low-lying portion of Kawakawa river reserve accessed via Old Whangae rd. The lot is irregular in shape, with the southern third consisting of an existing commercial building adjacent to Gillies Street, and paved carpark areas at the north end. The remainder of the site is covered in grass and is relatively flat, apart from a 20m strip which straddles the river and consists of bunded slopes that form man-made flood protection. The proposed development plans to locate two storey lightweight buildings and carparks within two thirds of the lot along the central portion of flat land, grassed and paved. Reference should be made to the topographical plans and concept plans shown in figures 2 & 3 and

Site topographic survey has been conducted by a registered surveyor and the locations and dimensions of all features as shown on the accompanying plans and discussed in this report are from the survey.

The subsurface conditions discussed in this report have been determined at very specific locations and will not identify any variations in ground strength or composition at other locations on this site. During construction should ground conditions be found to vary significantly from those described in this report PK Engineering Ltd. is to be notified immediately.





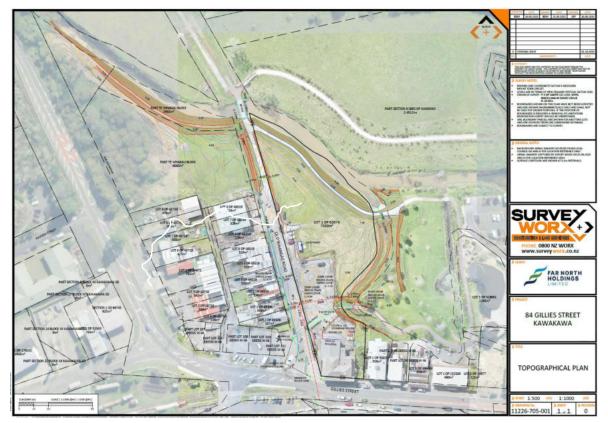


Figure 2. Site Topo by Survey Worx



Figure 3. Concept Plans





# 3.2 COUNCIL NATURAL HAZARDS

The flood hazard extents as modelled by Northland reginal council are depicted in figure 4 below and pose a hazard to the development if not managed properly. The flood modelling is not covered in detail in this report. Reference should be made to flood controls in a special report prepared by Hoskin Civil – "Old Whangae Road, Development, Kawakawa Three Waters Report" - 078-3wr-01-RevP1.

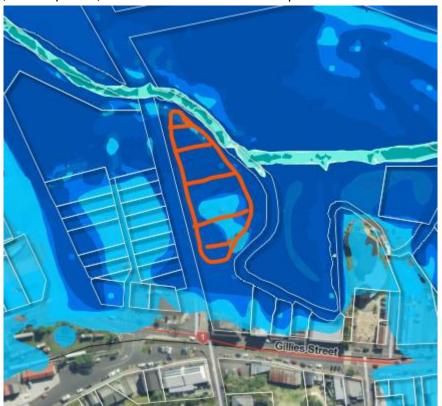


Figure 4. NRC Coastal and River flood hazard maps.

# 3.3 GEOLOGICAL MAPPING

The site geology according to GNS sciences (figure 1 below) is mapped as the Tauranga group Holocene deposits, of unconsolidated-poorly consolidated mud, sand, gravel and peat of alluvial, colluvial and lacustrine origins. This description is consistent with what we encountered in our intrusive investigation. The mapped geology also indicates the contact between Tauranga group and Waipapa group geology, is consistent with the rock mass found in our deep boreholes, underlying the Tauranga group between 8.60 metres to 21.0 metres deep, the rock has a slope of approximately 16 degrees towards the north.





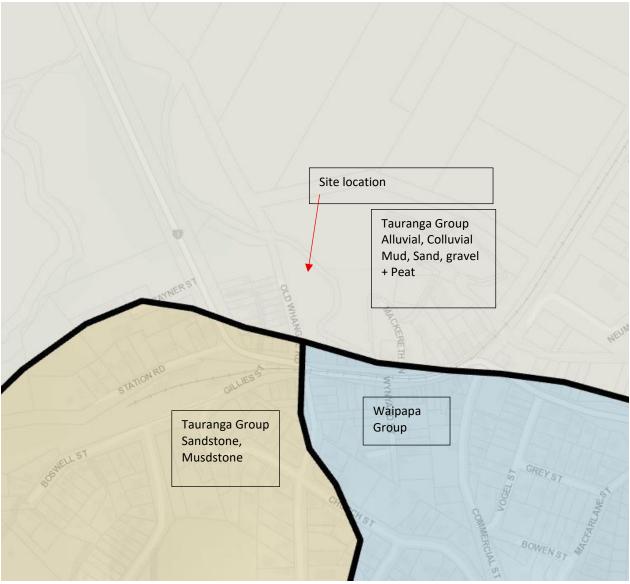


Figure 5: Extract from GNS WEB MAPS

# 3.4 PREVIOUS REPORTING

No previous reporting has been identified for this site.

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# 4. SITE INVESTIGATIONS AND SOIL CLASSIFICATION

# **4.1 VISUAL INVESTIGATION**

A thorough walkover of the site was undertaken, and geotechnical features related to site stability and drainage will be required.

# **4.2 SUBSURFACE INVESTIGATIONS.**

# 4.2.1 HAND AUGERHOLE TESTING.

Six subsurface exploratory auger holes have been drilled on the site shown on the attached site plan as AH1-AH6. In situ undrained shear strength readings were taken at 300mm intervals in each hole. These holes were drilled with a 50mm hand auger to different depths based on subsurface requirements or until was in practicable. Scala penetrometer tests were carried out in the base of some of the auger holes and readings were taken as blows per/50mm increment until enough information was gathered.

A summary table of the subsurface data has been provided below (Table 2)

Table 2: Subsurface data

Item	Depth (m)	Rock Intercept (m)	Scala Depth (m)	GWL (m)
AH1/PT1	3.0	-	6.4	<b>1.35</b> (6/10/2025)
AH2/PT2	4.5	-	7.45	<b>0.9</b> (6/10/2025)
AH3/PT3	3.9	-	5.9	<b>1.36</b> (6/10/2025)
AH4	3.3	-	-	<b>3.0</b> (4/11/2025)
AH5	4.0	-	-	<b>2.4</b> (4/11/2025)
AH6	3.0	-	-	<b>2.6</b> (4/11/2025)
MB01	24.0	21.0	-	-
MB02	10.25	8.60	-	-

<sup>\*</sup>AH = (AUGERHOLE), PT= (SCALA PENETROMTER) & MB=MACHINE BOREHOLE)





Auger holes AH1 – AH6 all intercepted stiff to very stiff silty clays with undrained shear strengths generally exceeding 75kPa, before intercepting a weaker layer of fine-grained silty Clay, with undrained shear strengths less than 50kPa, and with saturation beyond the plastic limit of the soil, making it prone to creep. Scala penetrometer tests were undertaken at the base of AH1-AH3 into the soft layers, with a generally increasing readings with depth, which may be due to a combination of skin friction and greater compaction. PT1, encountered anomalous stronger readings around 5.7-6.40 metres below ground level.

The auger hole inferred subsoil profiles have been illustrated on cross sections A-A and B-B. Reference should be made to sheets SG2 and SG3 in Appendix A and the auger hole logs and scala penetrometer sheets in appendix A.



Figure 1: Hand auger samples taken form AH3 down to 3.90m bgl







Figure 2: Hand auger samples taken from AH4 down to 3.30m bgl

### 4.2.3 MACHINE BOREHOLE TESTING

Two subsurface exploratory machine boreholes were undertaken by Brown Bros Ltd with observation by us. The machine boreholes have been located as shown on sheet SG1 (appendix A) and summary of the results have been shown in Table 2 above.

The machine boreholes were carried out with a fully hydraulic percussion drilling machine, taking mostly intact samples for the entire depth, with SPT readings at regular intervals and sample push tubes at specified locations.

A summary of the results has been provided in appendix A,

MB01 encountered the stiff clayey silt crust to approximately 3.0 meters below ground level, before encountering weakly consolidated alluvium down to a depth of 21.0 meters before encountering intact rock mass (greywacke). MB02 encountered a similar profile of clayey silt crust, however the weak alluvium layer was 8.60metres deep before intact rock mass (greywacke) was encountered.

A table 3 below indicates the summary of subsurface layers.



# Table 3: Subsurface data summary

Unit description	Depth to layer (m)	Thickness (m)	Shear value (kpa)	Scala (blow per 50mm)
Topsoil/Fill	0	200-250	-	-
Stiff – very stiff alluvium crust	0.20 (av)	1.6-3.6m	57-170	-
Very soft to Stiff alluvium (plastic, cohesive)	1.6-3.6	5.6 – 18m	27-50 (as tested)	-
Highly- Moderately weathered bedrock of the Waipapa Group	8.6-21.0	2m +	-	-



Photo 3: MB02 SAMPLE BOX.







Photo 4: MB02 Sample Box.

# **4.3 GROUND WATER AND MOISTURE CONDITIONS**

At the time of the investigation the winter weather had produced significant amounts of rainfall in the locality. The soils we encountered were predominantly moist, for the upper couple of metres, before a sharp transition to a wet saturated state under the groundwater table. The ground water table ranged from 0.9m deep to 3.0 metres deep below existing ground level. The ground water table was found to vary based on the depth of the overlying moderately compacted crustal layer of stiff to very stiff clayey SILTS< (brownish orange in colour). Generally, the ground water table was found just above the base of this layer. The reason for the variability of groundwater based on the soil conditions is likely due to the overburden pressure of the upper crust on the weaker saturated alluvium below creating a hydrostatic pressure variation.



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# 4.4 LABORATORY TESTING

Laboratory testing was conducted on soils collected in push tubes at variable depths within the upper stiffer crustal layer and the weaker alluvium soils underlying this layer in order to obtain soil parameters for calculating the short term and long-term behaviour of the soils under static loads imposed by the proposed development, as well as dynamic load conditions. These have been described in further detail in the sections below.

A summary of the lab test for each push tubes are shown below, and the results are provided in appendix C.

Table 4: Lab sample summary

Item	(Layer)	Depth bgl (m)	Lab Test types
MB01 (Push tube)	Upper crust (silty	2.2-2.95	NZS4402 & AS 1289.7.1.1 Tests
	Clay)		-Water content
MB01 (Push tube)	Weaker Silty Clay	4-20-4.95	- Atterberg Limits
	Alluvium		(liquid/plastic/plasticity index)
	(Saturated)		- Linear shrinkage
MB02 (Push Tube)	Upper crust (silty	2.2-2.95	-Shrinkage index
	Clay)		-Solid density
MB02 (Push Tube)	Weaker Silty Clay	5.20-5.95	- Consolidation (various load cycles)
	Alluvium		
	(Saturated)		

# 4.5 SEISMIC SUBSOIL CLASS

This site is considered Subsoil Class C – Shallow soil site as defined by NZS 1170.5 (2004) "Structural Design Actions) Part 5: Earthquake actions – New Zealand ". The soft soil was not deep enough to classify the site in the Class D category.





# 5. SITE STABILITY

# **5.1 DEFINITION AND LEGISLATION**

This section provides information that relates to section 71 (3) of the Building Act (2004), which in purpose is set out to assess the geotechnical hazards and their limitations and restrictions on buildings on land subject to natural hazards. Those hazards are:

- Erosion (including coastal erosion, bank erosion, and sheet erosion)
- Falling debris (including soil, rock, snow and ice)
- Subsidence
- Inundation (including flooding, overland flow, storm surge, tidal effects, and ponding).
- Slippage.

The relevant hazards and their relationship to the site and buildings are outlined in the remainder of this section below.

### 5.2 EARTHQUAKE AND TSUNAMI HAZARDS

This site is located in the low-risk zone for earthquakes due to its distance from known active faults and the Hikurangi subduction zone. The design of the foundations of the buildings should be rigid enough not to fail under dynamic loading, such that the serviceability limit state of the buildings is compromised.

Likewise, the risk of inundation is negligible on this site due to its horizontal distance from the coastline and the shape of the landmass which effectively creates an obstruction to the direct impacts of a tsunami. However, in a large tsunami event there is likely to be some tidal/surge behaviour alongside the site, which is considered low in terms of overall risk to the development. The Northland regional council has mapped the site as the safe area during a tsunami warning.





# 5.3 LIQUEFACTION

The site investigation has allowed us to determine that the upper 1.6-3.0 metres in non-liquefiable in nature due to the high cohesion and low porewater content of the soils, being well above the water table.

However, the behaviour of the soils under this stiff crust from our investigations suggest the added porewater pressure from dynamic shaking under seismic conditions would effectively displace the water content and cause consolidation and liquefaction may form as a result of this behaviour. However, in general the soils were fine grained enough that the liquefaction risk is considered to be very low.

A description of the Liquefaction process is described Below:

**Normal state:** Soil grains are in contact with each other, and the soil can support structures because of the friction between grains. The water in the pores helps balance pressure but doesn't carry the load.

**During shaking or rapid loading:** The soil is shaken, and grains try to compact. However, since the soil is saturated and water cannot drain away quickly, **pore water pressure increases**.

**Result:** As pore water pressure rises, it reduces the **effective stress** (the actual contact force between soil grains). When effective stress drops to near zero, the soil behaves like a liquid rather than a solid.

# **Effects of liquefaction:**

- Ground loses its ability to support loads (buildings may tilt or sink).
- Lateral spreading (ground moves sideways, often towards rivers or slopes).
- Sand boils or ejecta (water and sand erupt to the surface).
- Instability of slopes, embankments, and retaining structures.

Vibration of the soil is often the main cause of liquefaction. The two most common modes of vibration are earthquakes and the use of heavy machinery on-site or neighbouring sites. This site is low risk for earthquakes as described in section 5.2 above.

Vibration from machinery is usually correspondent with commercial excavations and drilling or use of heavy machinery. Size and impact from such machinery should be carefully considered and monitored during any construction upon this site.

It is recommended that no dynamic construction methods such as driven piles, are utilized on this site due to the risk of lateral spreading and the building platform is stiff enough to resist differential settlement in the rare chance of a seismic event.

All foundations must be carefully designed to ensure long-term performance and based upon the soil's parameters depicted in this report.





# 5.4 GROUND DEFORMATION OR SETTLEMENT

The soils on this site generally exhibit low to moderate strength and moderate to high compressibility. The deeper alluvium soils have a low degree of consolidation and are prone to creep type behaviour. The loads imposed on these soils, from the development can lead to uneven settlements if the gravel raft and foundation are not designed properly. Special care and analysis should be done to verify this when designing the foundations of any structure.

# 5.5 SOIL EXPANSIVITY.

The soils on this site can be classified as "**moderately expansive**" based on tactile descriptions made on site and experience in the locality. It is recommended to limit the exposure of any cut surfaces to excessive wetting and drying over the seasons. This can lead to desiccation cracking and instability. Any cut faces should be vegetated with plants such as vetiver grass or any locally hard-wearing deep-rooted plant known to provide erosion control. A suitable geomesh such as CIRTEX BIOCOIR Coconut Matting (0800 247 839) may also be used to prevent excessive drying of exposed cut faces.

# 5.6 SLOPE STABILITY

We carried out a numerical stability analysis across a critical soil profile along the edge of the proposed building platform and riverbank to check for the factors of safety against slippage from the additional loads imposed by the proposed building platform and surcharge loads. Figures 6 & 7 below indicate the static and dynamic slope stability models.

The factors of safety for the static model are above 2.0 indicating the risk of circular type slip failure behaviour along the riverbank is low, and the development isn't adding significant risk to the failure of the riverbank soils.

The factors of safety for the dynamic model indicate a factor of safety approaching 1.5, which is suitable form an ultimate limit state perspective (1/500-year return period), also considering the low risk of earthquakes in the locality.

The Horizontal coefficient for ULS within the dynamic slope stability model was derived from the formulas within NZS 1170.5:2004. Based off a design working life of 50 years for importance level 2 structures according to NZS 1170.0-2002.





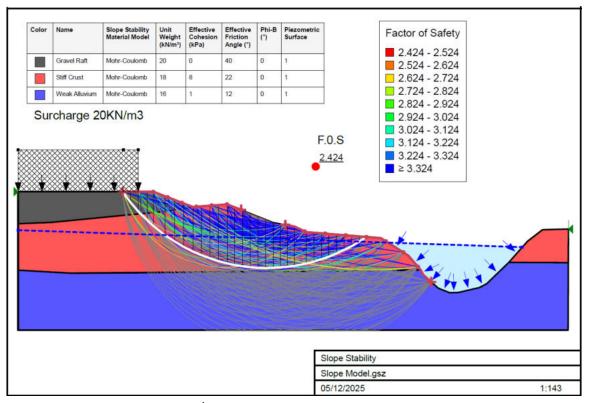


Figure 6: Geo-studio, slope/w static stability model.

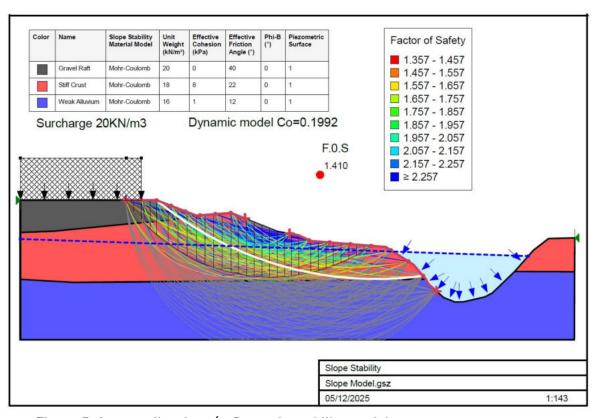


Figure 7: Geo-studio, slope/w Dynamic stability model.

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For Proposed Development
At Old Whangae Rd, Kawakawa
For Far North Housing Ltd

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# 6. ENGINEERING DISCUSSION

CHARTERED PROFESSIONAL ENGINEERS

The site has a complex underlying subsoil structure, which needs to be understood and to be able to develop the site in a sustainable manner. The site is underlain by a weak alluvium layer of varying thickness, between 5.30- 18.0m thick. The weak layer is considered to be moderately compressive and prone to differential settlements due to the variable thickness of the weak layer. Due to this fact, the site requires specific engineering design by a suitably experienced chartered professional engineer in order to develop the site sustainably.

The results of our lab testing have determined that this alluvium layer is at or beyond the liquid limit, in the depths tested below the crustal layer (4.20-5.95m). Therefore, the alluvium layer is behaving more like a viscous liquid than a soil. The weak alluvium within the machine boreholes was mostly homogenous, with a generally fine-grained texture, the major fraction of the soil being of clay particle size (<0.002mm diameter). Organic inclusions were found throughout the soils.

It is considered uneconomical to pile through the weak alluvium layer onto the rock strata. Therefore, the most feasible solution considering the site constraints from flooding and soil conditions is to float the buildings on an engineered raft, with enough rigidity built in to limit differential settlement.

PK engineering Ltd has designed the gravel raft and foundations for the Te Hononga Project (cultural centre) in Kawakawa on the neighbouring site, adjacent to this one under comparative conditions. It would be possible to adapt a similar technique to provide a sustainable solution to the proposed development on this site.

Most of the same engineering design principles apply to this development, and construction procedures such as preloading the site to accelerate short-term settlement before placement of the buildings, will help make this development a sustainable one. An outline of the engineering requirements and recommendations are outlined in the section 7 below.





# 7. ENGINEERING RECOMMENDATIONS

# 7.1 ENGINEERED RAFT (BUILDING PLATFORM)

The development of the site requires an engineered raft to lift the buildings out of the flood plain, as determined by specific flood modelling not included in this report. That flood modelling has established a finished ground level of RL 6.75, 1.5 metres above the average existing ground level is RL4.5. There are various engineering elements and recommendations described in the sections below in order to construct the engineered raft, which would be fit for purpose.

# 7.1.1 ENGINEERED FILL

The engineered fill needs to be constructed as a gravel raft acting like a large beam, which has enough tensile strength to limit differential settlement across the site. In order to create this beam effect, a layered compacted hardfill raft with geo mesh between the layers is required. The design of this engineered raft should be undertaken by a suitably experienced chartered professional engineer.

A conceptual cross section has been shown in appendix A of the principal design of the gravel raft.

# 7.1.2 RETAINING WALLS

The outer extents of the engineered raft require specific retaining wall design in order to ensure structural integrity of the raft from failure. The retaining walls need to be able to withstand the forces of nature, most notably erosion from flood waters, and vibrations from traffic along Old Whangae road. Due to the height of retaining it will be necessary to consider the pedestrian activity and surcharge loads from buildings and traffic when designing these walls. These retaining walls should be designed by a suitably experienced chartered professional engineer.

We have provided conceptual drawings in appendix A of a reinforced earth retaining wall option along the outside of the gravel raft, which is considered suitable for this site if done properly. Again, this should be designed by a suitably experienced chartered professional engineer.

# 7.1.2 SERVICES

It should be considered within the civil design of all pipe networks under the buildings, that services need to be protected from damage from the gravel raft undergoing differential settlement. This can be achieved by aligning the services within individual or shared trenches in parallel with each other, with flexible joins that allow the pipes to cope with some acceptable levels of differential settlements. When the gravel raft undergoes the initial phase of short-term settlement, it should mostly act like one big beam. However medium- and long-term consolidation may result in some differential settlement, and this must not compromise any of the services.

From information received by the client, it is proposed to place a Ø525 RCRRJ Class 4 Pipe under the building platform beneath the gravel raft. We recommend that specific design be carried out for the



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foundation of this pipe and flexible rubber ringed joins be utilized to allow the pipe to tolerate a reasonable amount of differential settlement along its length.

The design of the foundation for the concrete pipe would likely consist of a 1.8m wide x 0.5m deep gravel raft geotextile wrapped with tensile support from geogrids, to allow it to act more like a beam. Specific engineering design for this is required to be provided by a suitably chartered professional engineer.

It is envisaged that the support mechanism of this pipe will be coupled to the gravel raft to reduce the risk of differential settlements affecting its long-term performance.

# 7.2 BUILDING FOUNDATIONS

It is recommended that a rib-raft type foundation be utilised to support the 2-storey timber framed buildings. The rib-raft should be designed such that any point loads must be built into the rafts and not taken into the fill beneath. The rib-rafts need to be stiff enough to cope with any differential settlement that may occur over the long-term and should be designed by a suitably experienced chartered professional engineer.

The aspect ratios of these rafts must be limited to no more than 3. Control joints must be provided if the aspect ratio is exceeded.

For both rib-raft and slab on grade foundations the following consideration must be followed:

- Trees that grow in large sizes should not be planted in close proximity to any foundation.
- No stormwater discharge should be allowed to occur close to any foundation
- Proper control joins must be provided in the slab if the aspect ratio breaches 1 in 3 and the length of any slab exceeds 18 metres.
- A chartered professional engineer must be engaged to design any such rib raft or slab on grade
- PK Engineering Ltd must review and approve of the foundation design prior to any construction.



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# **7.3 FOUNDATION PARAMETERS**

The following parameters should be utilized for the design of the rib raft foundations and retaining walls:

# **COMPACTED HARDFILL:**

Bulk Density	$= 20kN/m^3$
Ultimate Bearing Capacity	= 950kPa
Allowable Bearing Capacity (F.O.S = 3)	= 300kPa
Dependable Bearing Capacity ( $\phi$ = 0.5)	= 475kPa
Internal angle of friction (φ)	= 40°

Subgrade Modulus = 18,000 KN/m<sup>3</sup>

# **STIFF CRUSTAL LAYER:**

Bulk Density	$= 17kN/m^3$
Ultimate Bearing Capacity	= 225kPa
Allowable Bearing Capacity (F.O.S = 3)	= 75kPa
Dependable Bearing Capacity ( $\phi$ = 0.5)	= 150kPa
Internal angle of friction (φ)	= 22°

# **POORLY CONSOLIDATED ALLUVIUM:**

Bulk Density	$= 16kN/m^3$
Ultimate Bearing Capacity	= 105kPa
Allowable Bearing Capacity (F.O.S = 3)	= 35kPa
Dependable Bearing Capacity ( $\phi$ = 0.5)	= 52.5kPa
Internal angle of friction (φ)	= 12°

# **MODERATELY WEATHERED ROCK:**

Bulk Density	= 24kN/m³
Ultimate Bearing Capacity	= 6mPa
Allowable Bearing Capacity (F.O.S = 3)	= 2mPa
Dependable Bearing Capacity (φ = 0.5)	= 3mPa





# 7.4 ACCESS AND PARKING

The development proposes to provide an 8.0m wide access ramp to the site for traffic and pedestrians. The sides of the ramp will require retaining walls to support the engineered fill (gravel raft), these should be designed by a suitably chartered professional engineer. The development concept plans also indicate the design of carpark and turning areas. This should be designed as a flexible pavement to allow for any differential settlement that may occur.

The engineering aspects required to provide a stable access ramp and parking area are listed below:

- The driveway should be formed such that there is minimum 2% crossfall to cesspits and adequate drainage facility built to direct water away from the gravel raft and into the stormwater reticulation.
- The engineered fill under the pavements be specifically designed and incorporated in the gravel raft design described in the sections above.
- Retaining walls along the edges of the ramp must be designed by a suitably experienced chartered
  professional engineer to support the engineered fill.
- No concentration of stormwater shall be discharged in an uncontrolled manner near the building platforms or around the edges and slopes of the gravel raft.

# 8. EARTHWORKS RECOMMENDATIONS

# 8.1 SITE PREPARATION AND EARTHWORKS

All topsoil or fill must be removed, and subgrade should be approved by a suitably qualified engineer prior to placement of any fill. These surfaces are also recommended to be proof rolled prior to placement of hardfill or clay fill.

It is the responsibility of the designer, project manager and contractor to read this report and ensure that the following recommendations are adhered to prior to any construction. Undertaking earthworks carefully and as per recommendations is critical to the short term and long-term stability of the site. Failure to comply with the following recommendations could undermine either of those aspects.

PK Engineering Ltd is of the view that any earthworks undertaken in winter months is not recommended. If the project manager requires a winter construction, they should submit a construction methodology for review prior to the start of any work. The person or persons in charge of this methodology should be familiar with documents such as GD05 - "Erosion and sediment control for land disturbing activities in the Auckland region"

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# 8.1.3 CUT BATTER SLOPES

No cut batter slopes are required as part of this development.

# 8.1.4 ENGINEERED FILL

The engineered fill Is required to be specifically engineered and constructed as per the specifications by the chartered professional engineers responsible for its design.

# 8.1.5 SITE DRAINAGE

Drainage measures should be in place so that no pooling or concentrated water is on or around the building platform, this includes short term and long-term drainage measures.

Due to the presence of the flood plane in close proximity to the edges of the proposed gravel raft, the exit points and gradients of all stormwater pipes must be carefully defined. Backwater infiltration into the drainage system should be avoided - especially around the structures.

Care must be taken to prevent excessive de-watering beneath the site as this may result in unintended settlements of the structure neighbouring the site being developed. Existing natural groundwater table and its historical fluctuation should be maintained as much as is possible and practicable.



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# 9. STORMWATER

Stormwater system designed must be done using correct best practice and it is desirable to keep the infrastructure within the gravel raft. This will eliminate some of the risk from breakage due to potential differential settlements. It is recommended that all such infrastructure have all flexi joins at regular intervals to mitigate effects of uneven settlements. An allowance of 10mm/10m of pipe lengths should be factored into these pipe design.

# 10. WASTEWATER

Not part of this report

# 11. RECOMMENDATIONS

After careful study of this site and the proposed development, I make the following recommendations:

- A geogrid reinforced gravel raft should be utilized to provide suitable stability to any foundation on this site.
- A rib-raft type of foundation should be considered to support any structure onto the abovementioned gravel raft.
- The aspect ratio for any rib-raft should be limited to 3.
- All infrastructure servicing the new structures should be placed within the depth of the gravel raft.
- All pipes embedded within the raft or under the raft must have flexible joins at regular centres.
- All foundation and gravel rafts must be designed by a suitably qualified and experienced chartered engineer.
- All foundation and gravel raft design must be checked and approved by PK Engineering Ltd.
- All foundation elements including gravel raft must be inspected and certified by a chartered professional engineer during construction.





# 12. CONCLUSION

After carrying out our geotechnical study, we conclude that this site can be developed in a sustainable manner without compromising the stability of the proposed structures. Carefully designed gravel raft and floating rib-raft type of foundation would ideally suit this site.

# 3. LIMITATIONS

This report should be read and produced in its entirety including the limitations to understand the context of the opinions and recommendations given.

This report has been prepared exclusively for Far North Housing Ltd in accordance with the brief given to us and the agreed scope and will be deemed exclusive to the owner. Information, opinions, and recommendations contained in this report can only be used for the purposes with which it was intended. PK Engineering Ltd accepts no liability or responsibility for any use or reliance on this report by any party other than the owner or parties working for or on behalf of the owner, such as local authorities. This report is not to be used for purposes beyond those for which it was intended for. This report was prepared in general accordance with current standards, codes and best practice at the time of this report. These may be subject to change.

The description of soils and analysis is based upon soil mapping in set locations on the site. It has been assumed that soil conditions are consistent with the discoveries in their location - there may be unforeseen variation in between. If any variation is found during the construction phase, then PK Engineering Ltd must be notified as soon as possible to advise on any changes to foundations that may be necessary.



# **APPENDIX A**



# **CONTENTS**

# **APPENDIX A**

A.1 AUGERHOLE LOGS

A.2 SCALA PENETROMETER LOGS

A.3 MACHINE BOREHOLE LOGS

A.4 PHOTOS OF SOIL SAMPLES

A.5 GEOTECHNICAL DRAWINGS

SITE PLAN CROSS SECTION AA CROSS SECTION BB

#### **BOREHOLE LOG NO -**AH1

Project: Old Whangae Road Client: Far North Housing Ltd.

Job No: 25-058



CHARTERED PROFESSIONAL ENGINEERS In situ shear vane #### ØØØ **±**±±± @@@ reading Graphic Remoulded shear vane Symbol reading **FILL** CLAY SILT SAND **HARDFIL** TOP Organic SOIL Scale Penetrometer Soil Soil Depth /Rock Soil/Roc **Undrained Shear** Scale Penetrometer **GWL Field Description** Strength (kPa) (blows/50mm) (mm) Graphic k type al Log 10 Silty TOPSOIL, gravel & bark inclusions, moist 100 150 22 300 @@@ SILT, brown, minor clay & gravel inclusions, stiff ( FILL) @@@ @@@ 600 600 000 SILT, light brown, some clay & fine sand, stiff, moist. #### 900 (NATURAL CRUST) Low - moderate plasticity #### 900 1200 #### #### 1200 1200 1500 **GWL @ 1.35** 500 #### 1800 1500 #### Silty CLAY, bluish grey, firm, saturated, low plasticity, 2100 74 beyond plastic limit 1800 53 2100 Tauranga group Holocene Alluvial Soils intercepted @1.35m 2700 2100 Poor recovery Low shear strength 2400 3000 2400 3300 2700 level 2700 **1**0 **Ground water** 3900 3000 EOH @ 3.0m 4200 3300 3600 3600 3900 5100 3900 1200 4200 1500 5700 4500 4800 4800 5100 5100 Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" Drill Methods 50 mm hand auger Test Location Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. The data Test Date 6/10/2025 will not identify any variations away from the location Inspector RD JW 2. UTP - Unable to penetrate. Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand Telephone: 09 407 3255 Fax: 09 407 3256 Email: TeamPK@pkengin.co.nz

#### **BOREHOLE LOG NO -**AH2 ENGINEERING Project: Old Whangae Road Client: Far North Housing Ltd. Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane #### ØØØ **±**±±± @@@ reading Graphic Remoulded shear vane Symbol reading **FILL** CLAY SILT SAND **HARDFIL** TOP Organic SOIL Scale Penetrometer Soil Soil Depth /Rock Soil/Roc **Undrained Shear** Scale Penetrometer **GWL Field Description** Strength (kPa) (blows/50mm) (mm) Graphic k type al Log 10 20 TOPSOIL and FILL 300 000 000 600 600 silty CLAY, light brown, moist to wet, firm, low plasticity 900 900 #### GWL @ 0.9m 58 1200 1200 1500 Silty CLAY, bluish grey, firm, saturated, low plasticity, beyond 1500 1500 plastic limit 2100 1800 1800 Tauranga Group Holocene Alluvial Soils intercepted @ 0.9m 2100 2700 2100 3000 27 Very soft, poor recovery 2400 2700 3300 Ground water level 2700 3600 3000 3000 3300 25 4200 3300 3600 3600 1200 3900 5100 3900 4200 4200 1500 5700 4500 EOH @ 4.5m 4800 4800 5100 5100 Drill Methods 50 mm hand auger Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" Test Location Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. The data

2. UTP - Unable to penetrate.

Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand

Test Date

Inspector

6/10/2025

RD JW

Telephone: 09 407 3255 Fax: 09 407 3256 Email: TeamPK@pkengin.co.nz

will not identify any variations away from the location

# BOREHOLE LOG NO - AH3

**Project:** Old Whangae Road **Client:** Far North Housing Ltd.



Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane #### ØØØ @@@ reading Graphic Remoulded shear vane Symbol reading **FILL** CLAY SILT SAND **HARDFIL** TOP Organic SOIL Soil Scale Penetrometer Soil Depth /Rock Soil/Roc **Undrained Shear** Scale Penetrometer **GWL Field Description** Strength (kPa) (blows/50mm) (mm) Graphic k type al Log TOPSOIL and FILL 100 150 300 300 000 62 @@@ 600 600 #### clayey SILT moderately stiff, moist, low plasticity #### #### 110 900 #### clayey SILT, crumbly, moist, minor moderately weathered rock #### inclusions <5mm 1200 110 1200 1500 **GWL @ 1.36m** #### 1500 1500 #### Clayey SILT, stiff, moist, moderate plasticity #### 2100 110 1800 1800 #### Tauranga Group Holocene Alluvial Soils intercepted @ 1.36m 2100 CLAY, soft, bluish grey, plastic, moist to wet. Saturated at 2. 2700 2100 3000 2400 3300 **Ground water level** 2700 3600 3000 3300 4200 3300 3600 3600 4800 3900 5100 3900 EOH @ 3.9m 4200 0 5700 4500 4800 4800 5100 5100 Drill Methods 50 mm hand auger Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" Test Location Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. The data Test Date 6/10/2025 will not identify any variations away from the location Inspector RD JW UTP - Unable to penetrate Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand Telephone: 09 407 3255 Fax: 09 407 3256 Email: TeamPK@pkengin.co.nz

# BOREHOLE LOG NO - AH4

Project: Old Whangae Road
Client: Far North Housing Ltd



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1200	#### :::::::::								1200	1500	
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#### BOREHOLE LOG NO -AH5

Project: Old Whangae Road



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000	#### :::::::								900 87	900
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2100	#### :::::::: ####	Alluvial	pted @	wet - soft , no org	anic inclu	sions			2400 68	3000
2400	::::::::	ene /	terce		Saturate	ed - GWL	@ 2.4m		2700 68	3300
2700	#### :::::::: ####	Holoc	evel in							3600
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st Date pector			4/11/20 JW	25		not identify - Unable t	any variations a	way trom the	ie location.	

# BOREHOLE LOG NO - AH6

Project: Old Whangae Road
Client: Far North Housing Ltd



Graphic Symbol		@@@ FILL			<del>/##</del> ILT	ØØØ SAND	HARDFIL	#### TOP	DDDDD Organic	In situ shear vane reading Remoulded shear vane reading
Depth	Soil /Rock	Soil/Roc	GWL			Field Descrip	tion	SOIL	Soil  Undrained Shear	Scale Penetrometer  Scale Penetrometer
(mm)	Graphic al Log	k type							Strength (kPa)	(blows/50mm)
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300	####			Clayey SILT, min					45	300
	:::::::: ####			moist, stiff to ve	ry stiff,	low- modera	te plasticity		600 120	600
600	::::::::: ####									
									900 123	900
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									1800 45 <sup>78</sup>	2100
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	#### :::::::::	oils	2.6m						2100 68	
2100	####	ial S	(9)	blue grey and br	own mo	ottled				2700
	#### #####	Alluv	pted						2400 60	3000
2400		ene	terce						2700 45	3300
	#### :::::::::	Tauranga group Holocene Alluvial Soils	Ground water level intercepted			ırated - GWL				
2700	:::::::::	4 dnc	ır lev	Silty CLAY, bluis	h grey, a	alluvium, sof	t to firm, satura	ited,	3000 48	3600
3000	:::::::::	la gr	wate	Beyond plastic li Low to no recove						3900
		ıranç	punc			E.O.h @ 3.0	m		3300 0	4200
3300		Таг	Gro						3600 0	4500
	::::::::									1350
3600	:::::::::								3900 0	4800
3900	:::::::::									5100
									4200	5400
4200	:::::::::								4500	
4500	::::::::									5700
4500	:::::::::								4800	6000
4800	::::::::									6300
	::::::::								5100	
5100									5400	6600
rill Metho	ada		50 mm	hand augar	Isi -	4a. All E:-!!	lo main a !	00 nc= N17/	5400	d Dook Field Descriptions"
est Loca	tion			hand auger site plan	1. 7	The subsurfac	e data described	above has l	been determined at a spe	d Rock Field Descriptions" ecific borehole location. The data
est Date spector	-		4/11/20 JW	25	V	vill not identify JTP - Unable	any variations a	way from the	ne location.	

#### P K ENGINEERING LIMITED PENETROMETER HOLE No. 90 KERIKERI RD Phone (09) 4073255 EMAIL pk.engin@pkengin.co.n; SHT. 1 of 1 Location: Old Whangae Rd Job No. 25-058 Driven by: JW/RD Date: 6/10/2 R.L at Ground Level: n/a PT1 PT2 PT3 PT4 Depth PT3 PT4 Depth PT1 PT2 PT3 PT4 Depth PT1 PT2 PT4 Depth PT1 PT2 PT3 hand à pushed down hand þ down paysnd

BOREHOLE LOG NO -BH01 (A) Location of Borehole Project: Old Whangae Road ENGINEERING Client: Far North Housing Ltd Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane #### ØØØ reading Remoulded shear Graphic vane reading Symbol **FILL** CLAY SILT SAND ROCK TOP Organic SOIL Soil Scale Penetrometer Soil **GEOLO Undrained Shear** Scala Penetrometer Depth /Rock LAYE **GWL Field Description** (mm) Graphi GY RS Strength (kPa) (blows/70mm) cal Log (0.00-4.95) SILT, some clay, minor to some sand, #### firm, moist, low to moderate plasticity. 300 #### (Natural crustal Layer) #### 600 #### #### 900 #### #### 1200 #### #### SPT 1.50-1.9m (1-0-Natural Crustal Layer 1500 #### 1-1-1-0) #### Tauraunga Group Holocene alluvium. (0-0.014ma) 1800 #### 3,0M 2100 #### Push Tube Sample taken from 2.20m -2.95m #### **a** #### 2400 **GROUND WATER ENCOUNTERED** #### #### 2700 #### #### 3000 <del>|| || || ||</del> #### (3.00- 21.00M) SILT, some clay, varying sand #### 3300 inclusions, light bluish grey, soft, #### saturated, beyond plastic limit. (Organic inclusions) #### (WEAK ALLUVIUM DEPOSITS) 3600 #### 3900 #### #### #### 4200 Push Tube Sample taken from 4.20m -4.95m #### Weker Alluvium #### 4500 #### 4800 #### #### SPT 4.95-5.40m (2-5100 1-1-0-1-2) #### 50 mm hand auger Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" **Drill Methods** Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. **Test Location** 7/10/2025 The data will not identify any variations away from the location. **Test Date** Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

BOREHOLE LOG NO - BH01 (B) Project: Old Whangae Road ENGINEERING Client: Far North Housing Ltd Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane ØØØ reading **####** Remoulded shear Graphic vane reading Symbol TOP Organic **FILL** CLAY SILT SAND ROCK SOIL Soil Scale Penetrometer **Undrained Shear** Depth **GEOLO** Scala Penetrometer /Rock **GWL Field Description** Graphi RS (mm) GY Strength (kPa) (blows/70mm) cal Log #### (3.0-21.00M) SILT, some clay, varying sand #### 5100 inclusions, light bluish grey, soft, #### saturated, beyond plastic limit. (Organic inclusions) #### (WEAK ALLUVIUM DEPOSITS) 5400 #### #### 5700 #### #### #### 6000 SPT 6.0-6.45m (1-0-#### 6300 1-1-1-0) #### Tauraunga Group Holocene alluvium. (0-0.014ma) 6700 #### #### 3,0M 7000 #### #### **@** #### GROUND WATER ENCOUNTERED 7300 #### #### 7600 #### #### #### 7900 #### #### **WEAK ALLUVIUM LAYER** 8200 #### #### 8500 #### #### 8800 #### #### 9100 #### #### 10400 #### #### 10700 #### 11000 #### 50 mm hand auger Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" **Drill Methods** Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. **Test Location** 7/10/2025 The data will not identify any variations away from the location. **Test Date** Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

BOREHOLE LOG NO -BH01 (C)

Project: Old Whangae Road Client: Far North Housing Ltd



Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane ØØØ reading Remoulded shear Graphic vane reading Symbol **FILL** CLAY SILT SAND ROCK TOP Organic SOIL Soil Scale Penetrometer **GEOLO Undrained Shear** Scala Penetrometer Depth /Rock LAYE **GWL Field Description** (mm) Graphi GY RS (blows/70mm) Strength (kPa) cal Log #### #### (3.0- 21.00M) SILT, some clay, varying sand 11300 #### inclusions, light bluish grey, soft, saturated, beyond plastic limit. (Organic inclusions) (WEAK ALLUVIUM DEPOSITS) 11600 #### #### 11900 #### #### 12200 #### #### 12500 #### #### Tauraunga Group Holocene alluvium. (0-0.014ma) 12800 #### #### 3,0M 13100 #### #### **a** #### 13400 **GROUND WATER ENCOUNTERED** #### #### 13700 #### 14000 #### #### **WEAK ALLUVIUM LAYER** 14300 #### #### #### 14700 #### #### 15000 #### #### 15300 #### #### #### 15600 #### 15900 #### #### 16200 #### 50 mm hand auger **Drill Methods** Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" 1. The subsurface data described above has been determined at a specific borehole location. Refer to site plan **Test Location** 7/10/2025 The data will not identify any variations away from the location. **Test Date** Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By

Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

BOREHOLE LOG NO -BH01 (D) Project: Old Whangae Road Far North Housing Ltd Client:

Job No: 25-058



CHARTERED PROFESSIONAL ENGINEERS In situ shear vane ØØØ reading Remoulded shear Graphic vane reading Symbol TOP **FILL** CLAY SILT SAND ROCK Organic SOIL Soil Scale Penetrometer Soil Depth **GEOLO Undrained Shear** Scala Penetrometer /Rock **GWL Field Description** RS (mm) Graphi GY Strength (kPa) (blows/70mm) cal Log #### #### (3.0- 21.00M) SILT, some clay, varying sand inclusions, light 16200 inclusions, light bluish grey, soft, #### saturated, beyond plastic limit. (Organic inclusions) (WEAK ALLUVIUM DEPOSITS) 16500 #### 16800 #### #### 17100 #### #### 17400 #### #### #### Tauraunga Group Holocene alluvium. (0-0.014ma) 17700 #### #### 3,0M 18000 #### **a** #### **GROUND WATER ENCOUNTERED** 18300 #### #### 18600 #### #### 18900 #### #### **WEAK ALLUVIUM LAYER** 19200 #### #### #### 19500 #### #### 19800 #### #### 20100 #### 20400 #### #### 20700 #### #### 21000 #### 50 mm hand auger Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" **Drill Methods** 1. The subsurface data described above has been determined at a specific borehole location. Refer to site plan Test Location 7/10/2025 The data will not identify any variations away from the location. **Test Date** Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By

Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

BOREHOLE LOG NO -BH01 (E) Project: Old Whangae Road ENGINE Far North Housing Ltd Client: Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane ØØØ reading Remoulded shear Graphic vane reading Symbol **FILL** TOP CLAY SILT SAND ROCK Organic SOIL Soil Scale Penetrometer Soil **Undrained Shear** Scala Penetrometer Depth /Rock **GEOLO** LAYE GWL **Field Description** Graphi GY RS (mm) Strength (kPa) (blows/70mm) cal Log #### (21.00-24.00M) Highly weathered to Moderately #### 21000 weathered greywacke rock. (BASEMENT ROCK) 21400 21700 22000 Waipapa Group (Greywacke) Siltstone and Sandstone 154-270ma 22300 22600 3,0M 22900 GROUND WATER ENCOUNTERED @ 23100 23400 23700 End of machine borehole @ 24.0m **WEAK ALLUVIUM LAYER** 24000 24300 24600 24900 25200 25500 25800 50 mm hand auger Drill Methods Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" 1. The subsurface data described above has been determined at a specific borehole location. Refer to site plan Test Location 7/10/2025 The data will not identify any variations away from the location. Test Date Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

BOREHOLE LOG NO -BH02 (A) Location of Borehole Project: Old Whangae Road ENGINEERING Client: Far North Housing Ltd Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS ..... ØØØ **±**±±± reading Remoulded shear Graphic vane reading Symbol CLAY SILT ROCK TOP Organic **FILL** SAND Soil SOIL Scale Penetrometer Soil **Undrained Shear** Scala Penetrometer Depth /Rock **GEOLO** LAYE **Field Description GWL** (mm) Graphi GY RS Strength (kPa) (blows/70mm) cal Log (0.00-3.0) SILT, some clay, minor to some sand, #### 300 firm, moist, low to moderate plasticity. (Natural crustal Layer) #### #### 600 #### **FIRM UPPER CRUST** #### 900 #### #### 1200 #### (1.5-8.60M) SILT/CLAY, varying sand inclusions, light blu 1500 #### SPT 1.50-1.95m (1saturated, soft-very soft beyond plastic limit. (Organic in (WEAK ALLUVIUM DEPOSITS) 1-1-1-1) Tauraunga Group Holocene alluvium. (0-0.014ma) 1800 #### 3,0M 2100 #### Push Tube Sample taken from 2.20m -2.95m **a** #### 2400 #### **GROUND WATER ENCOUNTERED** #### 2700 #### 3000 #### #### 3300 #### 3600 #### #### SPT 3.7-4.15m (1-1-3900 #### 0-0-0-0) 4200 #### **WEAK ALLUVIUM** #### 4500 #### 4800 #### #### 5100 Push Tube Sample taken from 5.2m -5.95m #### 50 mm hand auger **Drill Methods** Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. **Test Location** 7/10/2025 The data will not identify any variations away from the location. Test Date Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz

**BOREHOLE LOG NO -**BH01 (B) Project: Old Whangae Road ENGINEERING Client: Far North Housing Ltd Job No: 25-058 CHARTERED PROFESSIONAL ENGINEERS In situ shear vane #### ØØØ reading Remoulded shear Graphic vane reading Symbol TOP **FILL** CLAY SILT SAND ROCK Organic SOIL Soil Scale Penetrometer Soil **GEOLO Undrained Shear Scala Penetrometer** /Rock LAYE Depth GWL **Field Description** (mm) Graphi Strength (kPa) (blows/70mm) cal Log #### Tauraunga Group Holocene alluvium. (0-0.014ma) (3.0-8.60M) SILT/CLAY, varying sand inclusions, light blu saturated, soft-very soft beyond plastic limit. (Organic in 5100 #### (WEAK ALLUVIUM DEPOSITS) #### 5400 5700 #### #### **WEAK ALLUVIUM LAYER** 6000 #### 6300 #### #### 6700 SPT 6.7-7.15m (1-1-#### 1-0-0-0) 7000 #### 3,0M #### **a** 7300 **GROUND WATER ENCOUNTERED** #### 7600 #### 7900 #### 8200 #### Waipapa Group (Greywacke) Siltstone and Sandstone 154-270ma) #### 8500 #### (8.60- 10.25M) Highly to moderately weathered sandstone and siltstone Green and grey 8800 (Basement Rock) 9100 (10.25m) Unable to drill with tungsten tip 10400 End of Borehole @ 10.25m) 10700 Bedrock 11000 Note: All field logging made as per NZGS Guideline "Soil and Rock Field Descriptions" **Drill Methods** Test Location Refer to site plan 1. The subsurface data described above has been determined at a specific borehole location. 7/10/2025 The data will not identify any variations away from the location. **Test Date** Brown Bros Drilling 2. UTP - Unable to penetrate. Drilled By Level 1 ANZ Bank Building 90 Kerikeri Road, Kerikeri New Zealand, Telephone: 09 4073255 Email: TeamPK@pkengin.co.nz



# **SITE PHOTOGRAPHS**





Photo 1: Hand Auger Samples from AH1





Photo 2: Hand Auger Samples from AH2



Photo 3: Hand Auger Samples from AH3







Photo 4: Hand Auger Samples from AH4



Photo 5: Hand Auger Samples from AH5





Photo 6: Hand Auger Samples from AH6



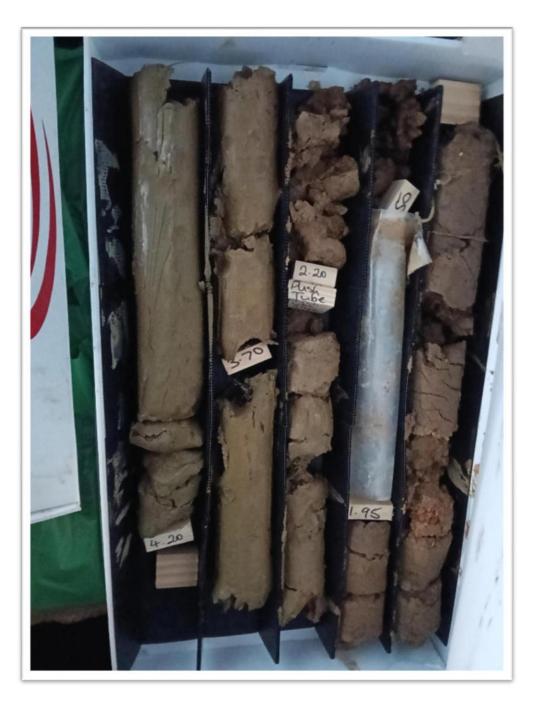


Photo 7: Machine Bore hole Samples from MB01(a)



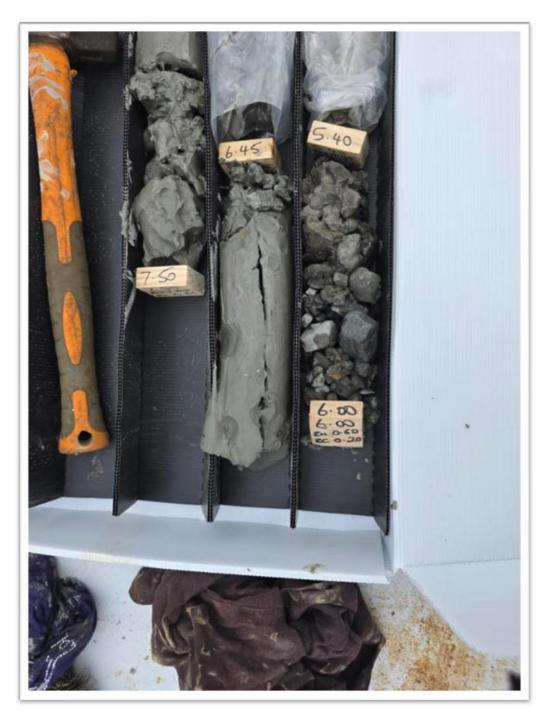


Photo 8: Machine Bore hole Samples from MB01(b)





Photo 9: Machine Bore hole Samples from MB01(b) - Zoomed





Photo 10: Machine Bore hole Samples from MB01(c)





Photo 11: Machine Bore hole Samples from MB02(a)





Photo 12: Machine Bore hole Samples from MB02(b)





Photo 13: Machine Bore hole Samples from MB02(c)





Photo 14: Push tube samples







Photo 15: Flood mitigation outflow



Photo 16: Northeast Corner of the site to be developed







Photo 17: Standing in the position where buildings are to be located.



Photo 18: Walkway along the edge of the sites northern flank looking south east with the riverbank to the north





Photo 19: Looking to the west with the site on the left



Photo 20: Looking at a portion of the building site back up towards Gillies street.





Photo 21: Standing in the middle of the site looking north west.

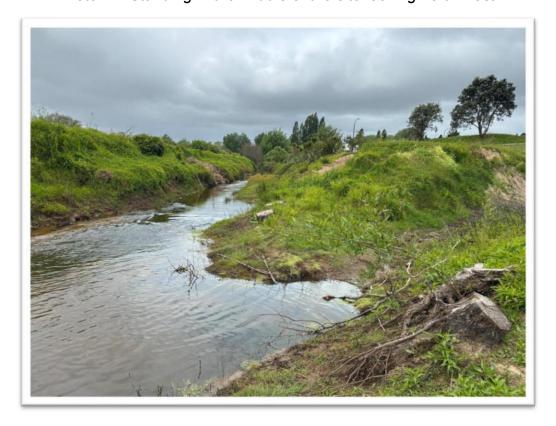


Photo 22: At river level, adjacent to the site.







Photo 23: Looking onto the centre of the building platform from the river bank bund



Photo 24: The existing stormwater swale along the east flank of the proposed site.



Geotechnical Report For Proposed Development At Old Whangae Rd, Kawakawa For Far North Housing Ltd Job# 25-058

Dec. 2025



CHARTERED PROFESSIONAL ENGINEERS

PROJECT:

# CONCEPTUAL DRAWINGS FOR PROPOSED DEVELOPMENT AT OLD WHANGAE RD FOR FAR NORTH HOUSING LTD

PROJECT ADDRESS:

# OLD WHANGAE ROAD KAWAKAWA

LEGAL DESCRIPTION

Lot 1 DP 63674

JDB ND:

25-058

DATE:

DECEMBER 2025

FIRST ISSUE (ISSUED FOR CONSENT)

### DRAWING INDEX:

SG1 SITE PLAN
SG2 CRUSS-SECTIUN - AA
SG3 CRUSS-SECTIUN - BB
SG4 CUNCEPTUAL CRUSS SECTIUN
SG5 CUNCEPTUAL DETAIL

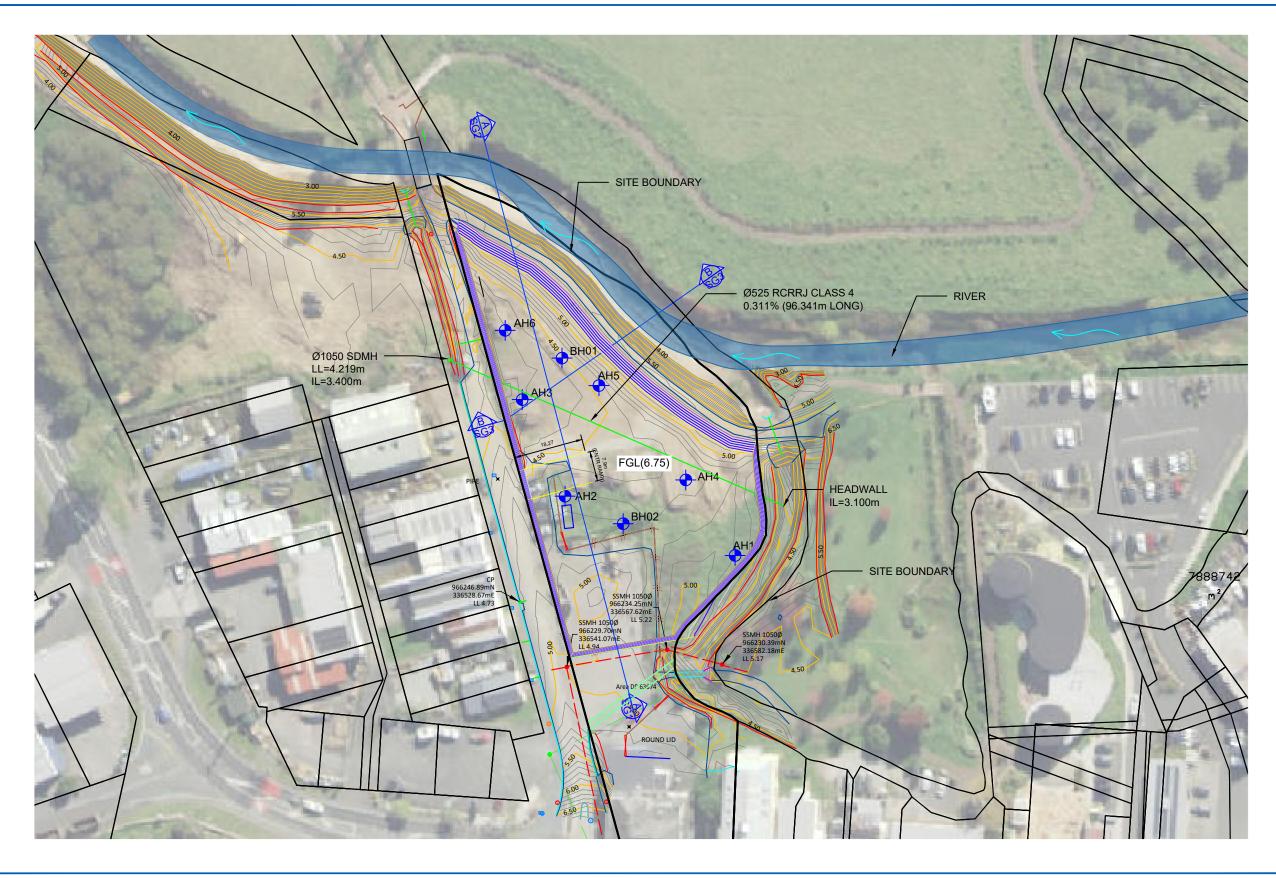
# ISSUED FOR CONSENT

# RO

LEVEL 2 ANZ Bank Building 90 Kerikeri road, P.D.Box 464 KERIKERI

Tel. (09) 4073255

E-mail. teampk@pkengin.co.nz







HAND AUGER LOCATION



MACHINE BOREHOLE LOCATION



PROPOSED OUTER EXTEND OF RAISED BUILDING PLATFORM



THIS PLAN IS ADAPTED FROM SURVEY WORX TOPOGRAPHIC SURVEY AND INFORMATION PROVIDED BY THE CLIENT FAR NORTH HOLDINGS LTD.

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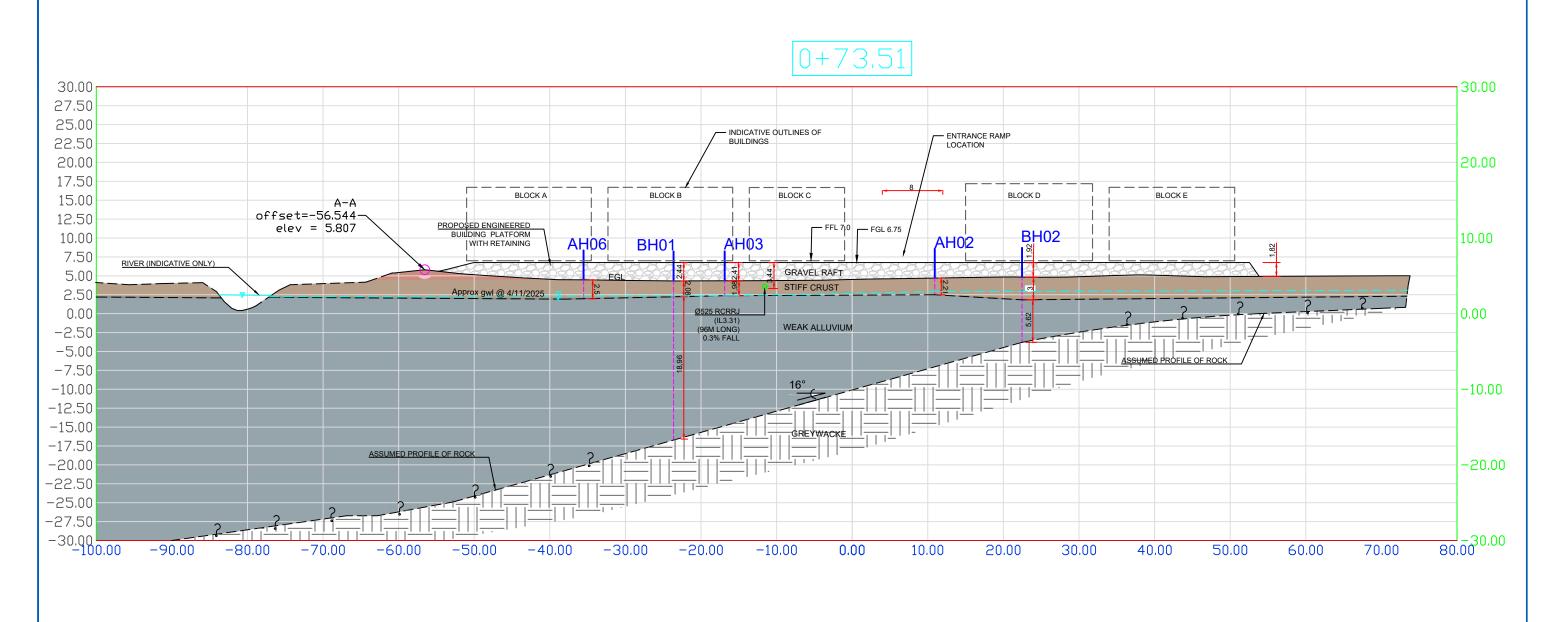
OLD WHANGAE RD, KAWAKAWA LOT 1 DP 63674

OLD WHANGAE ROAD

CHECKED:
CHECKED:
PK
REVISION:
RO



LEVEL 1, ANZ BANK 90 KERIKERI ROAD, KERIKERI PO BOX 464, KERIKERI Phone Number: 09 407 3255 Email: teampk@pkengin.co.nz



# CROSS SECTION A-A SCALE 1:500

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CLIENT: FAR NORTH HOUSING LTD

OLD WHANGAE RD KAWAKAWA LOT 1 DP 63674

ITILE: OLD WHANGAE ROAD

CROSS SECTION A-A

CROSS SECTION A-A

SCALE AT A3: DATE: DRAWN: DEC 25 JW PK

PROJECT NO: DRAWNIG NO: REVISION: 25-058 A3/SG2 RO

REV: DESCRIPTION: BY: DATE:

STATUS

STATUS

STATUS

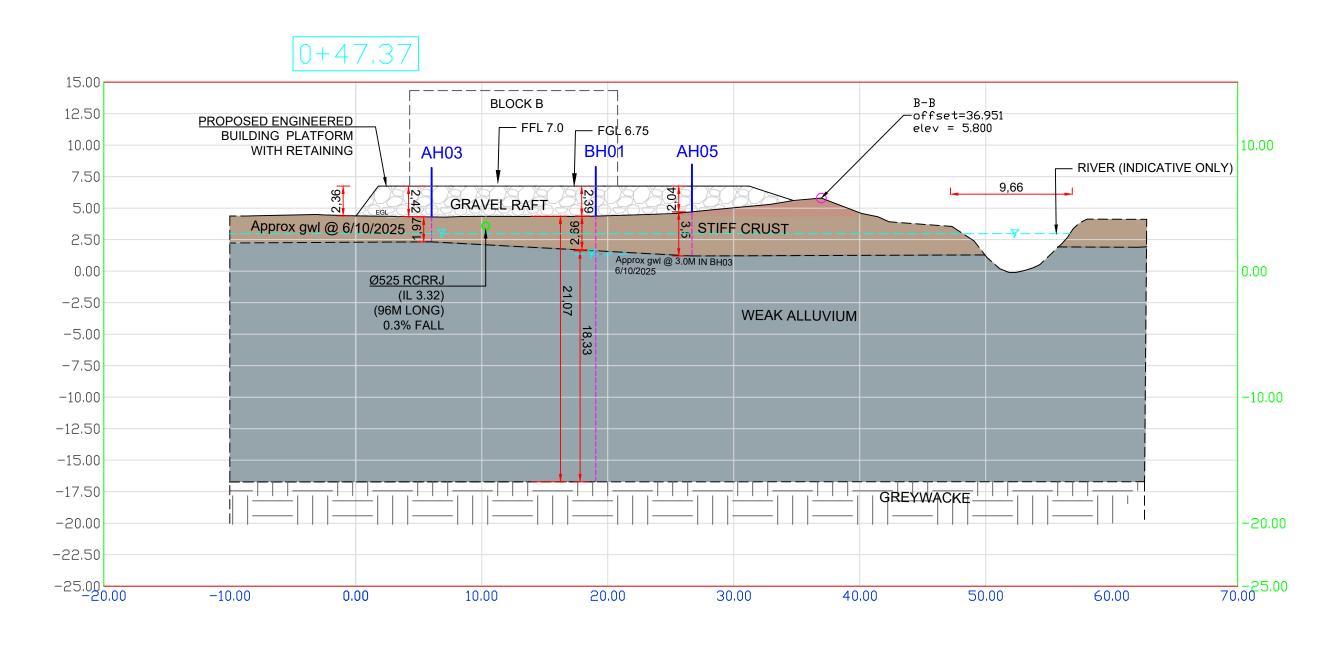
STATUS

SOURCE

ENGINEERING

LEVEL 1, ANZ BANK
90 KERIKERI ROAD, KERIKERI
PO BOX 464, KERIKERI
Phone Number: 09 407 3255

Email: teampk@pkengin.co.nz



## **CROSS SECTION B-B SCALE 1:300**

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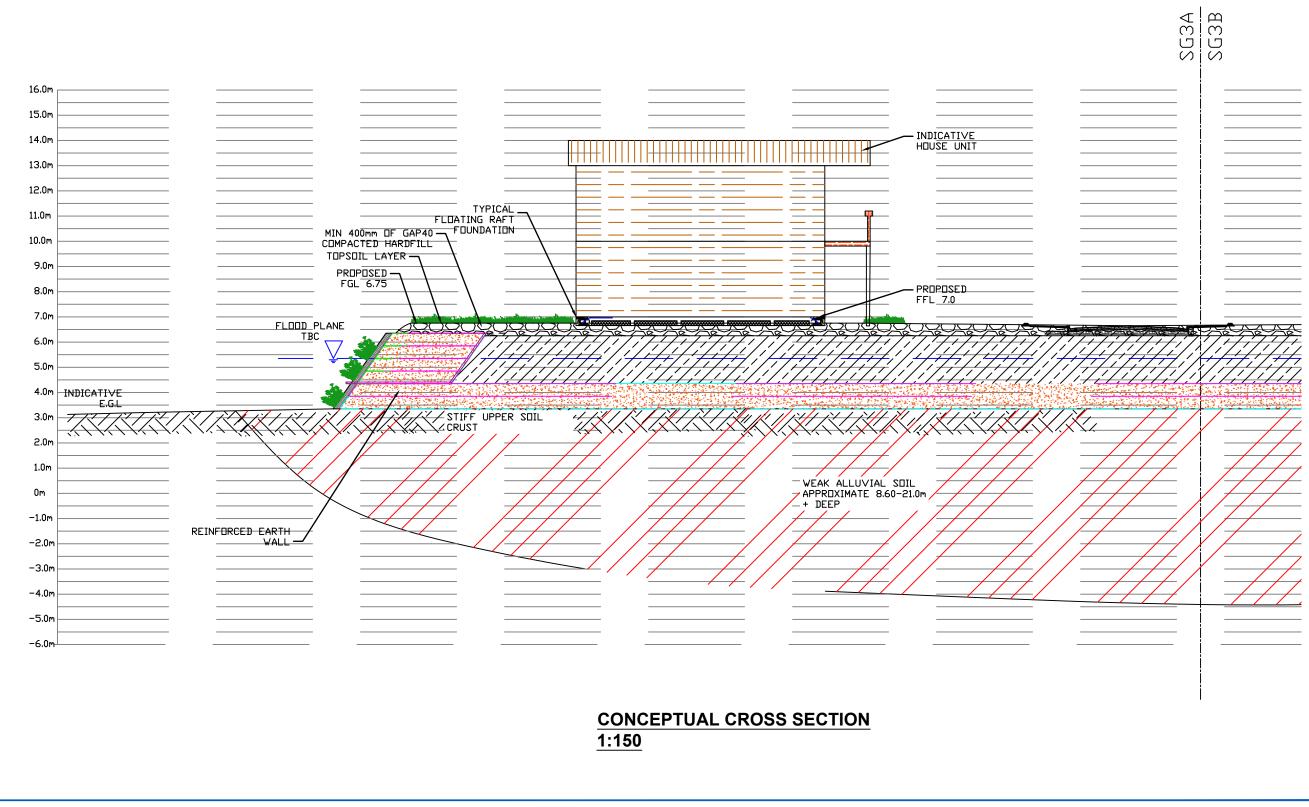
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OLD WHANGAE RD KAWAKAWA LOT 1 DP 63674

OLD WHANGAE ROAD

CROSS SECTION B-B			
SCALE AT A3:	DATE:	DRAWN:	CHECKED:
1:300	SEPT 25	JW	PK
PROJECT NO:	DRAWING NO:		REVISION:
25-058	A3/SG3		R0

BY: DATE: REV: DESCRIPTION: **ISSUED FOR CONSENT** ENGINEERING PO BOX 464, KERIKERI Phone Number: 09 407 3255 Email: teampk@pkenain.co.nz



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SITE: OLD WHANGAE RD KAWAKAWA
LOT 1 DP 63674

TITLE: OLD WHANGAE ROAD
CONCEPTUAL CROSS SECTION

SCALE AT A3: DATE: DRAWN: CHECKED:
1:150 DEC 25 JW PK

PROJECT NO: DRAWING NO: REVISION:
25-058 A3/SG4 RO

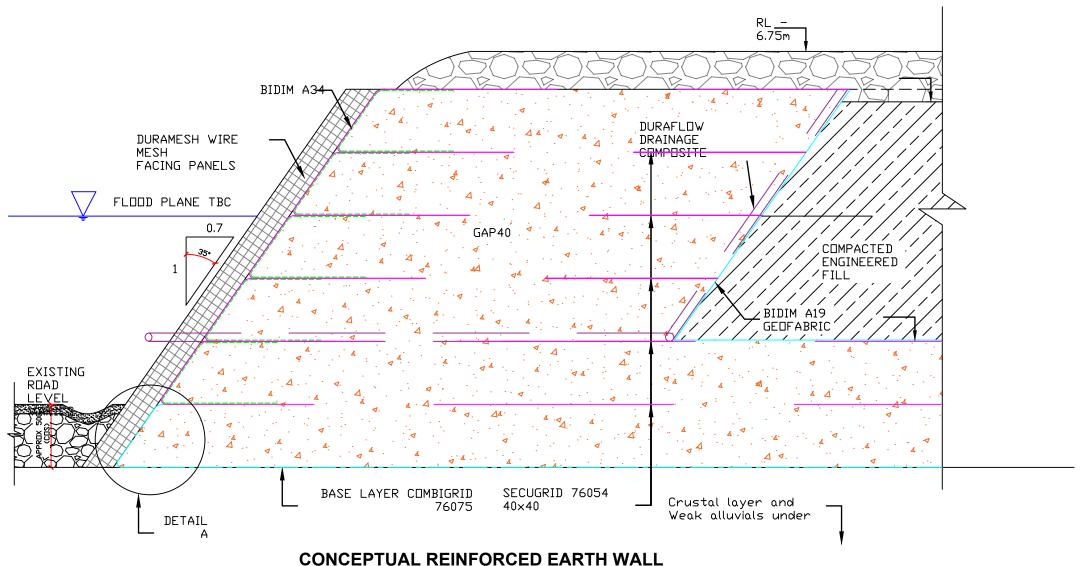
CLIENT: FAR NORTH HOUSING LTD

REV: DESCRIPTION:

STATUS

SSUED FOR CONSENT

LEVEL 1, ANZ BANK
90 KERIKERI ROAD, KERIKERI
PO BOX 464, KERIKERI
Phone Number: 09 407 3255
Email: teampk@pkengin.co.nz



CONCEPTUAL REINFORCED EARTH WALL CROSS-SECTION DETAIL

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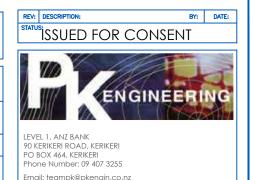


CLIENT: FAR NORTH HOUSING LTD

OLD WHANGAE RD KAWAKAWA LOT 1 DP 63674

OLD WHANGAE ROAD
REINFORCED EARTH WALL DETAIL

CHECKED:
/ PK
REVISION:
R0





# **APPENDIX B**





## **CONTENTS**

## **APPENDIX B**

**B.1 LAB RESULTS** 

**B.2 SLOPE STABILITY MODELS** 



### Whangarei Laboratory

166 Bank Street, Whangarei M: 022 590 3121 E: james@geocivil.co.nz

## **TEST REPORT**

**Lab Job No**: 8441-005

Your ref.: AT010024

**Date of Issue:** 4/12/2025

Date of Re-Issue: -

Test Report No. WRE8441-005-R001

PROJECT: Old Whangae - Soil Classification

CLIENT: Far North Holdings Ltd

9 Baffin Street, Opua 0200

ATTENTION: C/O PK Engineering Ltd Jonty White

TEST METHODS: Determination of the Water Content of soils

NZS 4402:1986 Test 2.1

Determination of the liquid & plastic limits, plasticity index and water content

NZS 4402:1986 Tests 2.1,2.2,2.3,2.4 Determination of the Linear Shrinkage

NZS 4402:1986 Test 2.6

Determination of the Shrinkage Index of a Soil

AS 1289.7.1.1 - 2003

Determination of the Solid Density of fine materials

NZS 4402:1986 Test 2.7.2

SAMPLING METHOD: Sampled by client - Sampling not accredited

TEST RESULTS: As per attached sheets

Laboratory Technician

A. Agnew

Approved Signatory

D. Krissansen

All results obtained in accordance with the test methods listed above.

Any material descriptions included in this report are

Test results relate only to the sample tested.

excluded from IANZ endorsement.



All tests reported herein have been performed in accordance with the laboratory's scope of accreditation



#### **DETERMINATION OF WATER CONTENT**

NZS 4402:1986 Test 2.1

Lab Job No: 8441-005
Client: Far North Holdings Ltd

Client: Far North Holdings Ltd
Project/Site: Old Whangae

 Tested By:
 N.K

 Date:
 3/11/2025

 Checked By:
 A.A

Date: 11/11/2025

Report No: WRE8441-005-R001

**Date Received:** 13/10/2025

Date Sampled: 7/10/2025 Sampler: Client

Sampling Method: Sampled by client – Sampling not accredited

Sample Number	Location	Sample Description	Water Content (%)
WRE8441-005-S001	MB01 2.20m - 2.95m	Silty CLAY, minor fine sands, traces of organic matter, grey mottled orange, wet.	34.2
WRE8441-005-S002	MB01 4.20m - 4.95m	Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.	61.5
WRE8441-005-S003	MB02 2.20m - 2.95m	Silty CLAY, traces of fine sands, grey mottled orange, wet.	39.2
WRE8441-005-S004	MB02 5.20m - 5.95m	Silty CLAY, traces of shell fragments to 15mm and organic matter, grey, wet.	49.5

4/12/2025 Issue 3 Page 2 of 18



NZS 4402:1986 Test 2.2,2.3,2.4

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S001

Client:Far North Holdings LtdTested By:N.KProject/Site:Old WhangaeDate:21/10/2025Sample Location:MB01 2.20m - 2.95mChecked By:A.A

Date: 11/11/2025

Date Received: 13/10/2025

 Date Sampled:
 7/10/2025
 Report No:
 WRE8441-005-R001

 Sampler:
 Client
 REF:
 AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, minor fine sands, traces of organic matter, grey mottled orange, wet.

**Test Details:** 

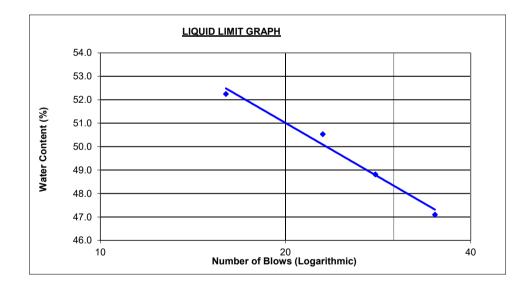
Test performed on: Fraction passing 425 µm sieve

Sample history: As received

	Liquid Limit			
No. of blows	16	23	28	35
Water content (%)	52.2	50.5	48.8	47.1

Plastic Limit		
25.6	25.6	

NWC	34.2
Liquid Limit	50
Plastic Limit	26
Plasticity Index	24





NZS 4402:1986 Test 2.2,2.3,2.4

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S002

 Client:
 Far North Holdings Ltd
 Tested By:
 N.K

 Project/Site:
 Old Whangae
 Date:
 21/10/2025

 Sample Location:
 MB01 4.20mm - 4.95m
 Checked By:
 A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.

**Test Details:** 

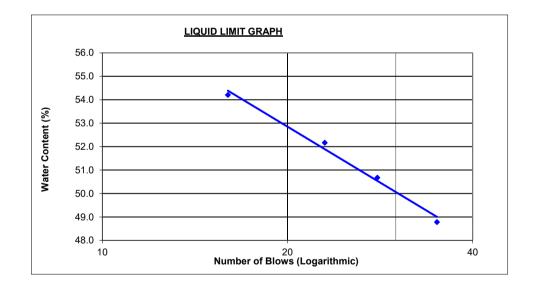
Test performed on: Fraction passing 425 µm sieve

Sample history: As received

	Liquid Limit			
No. of blows	16	23	28	35
Water content (%)	54.2	52.2	50.7	48.8

Plastic Limit		
25.8	25.7	

NWC	61.5
Liquid Limit	51
Plastic Limit	26
Plasticity Index	25





NZS 4402:1986 Test 2.2,2.3,2.4

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S003

 Client:
 Far North Holdings Ltd
 Tested By:
 N.K

 Project/Site:
 Old Whangae
 Date:
 21/10/2025

 Sample Location:
 MB02 2.20m - 2.95m
 Checked By:
 A.A

Date: 11/11/2025

Date Received: 13/10/2025

 Date Sampled:
 7/10/2025
 Report No:
 WRE8441-005-R001

 Sampler:
 Client
 REF:
 AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, grey mottled orange, wet.

**Test Details:** 

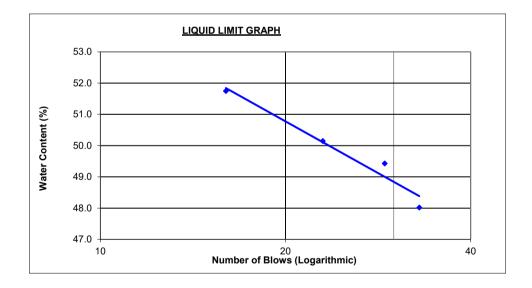
Test performed on: Fraction passing 425µm sieve

Sample history: As received

	Liquid Limit			
No. of blows	16	23	29	33
Water content (%)	51.7	50.1	49.4	48.0

Plastic Limit		
26.2	26.1	

NWC	39.2
Liquid Limit	50
Plastic Limit	26
Plasticity Index	24





NZS 4402:1986 Test 2.2,2.3,2.4

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S004

 Client:
 Far North Holdings Ltd
 Tested By:
 N.K

 Project/Site:
 Old Whangae
 Date:
 31/10/2025

 Sample Location:
 MB02 5.20m - 5.95m
 Checked By:
 A.A

 Date:
 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of shell fragments to 15mm and organic matter, grey, wet.

**Test Details:** 

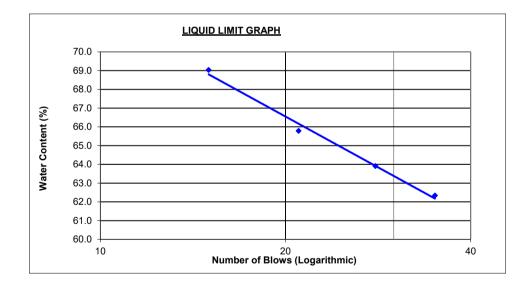
Test performed on: Fraction passing 425µm sieve

Sample history: As received

	Liquid Limit			
No. of blows	15	21	28	35
Water content (%)	69.0	65.8	63.9	62.3

Plastic Limit			
25.7	25.7		

NWC	49.5
Liquid Limit	65
Plastic Limit	26
Plasticity Index	39





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**Geocivil Laboratory** 

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E: info@geocivil.co.nz

## **DETERMINATION OF THE LINEAR SHRINKAGE**

NZS 4402:1986 Test 2.6

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S001

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 21/10/2025

Sample Location: MB01 2.20m - 2.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, minor fine sands, traces of organic matter, grey mottled

orange, wet.

**Test performed on:** Fraction passing 425mm sieve

History: As received

Linear shrinkage 14

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## **DETERMINATION OF THE LINEAR SHRINKAGE**

NZS 4402:1986 Test 2.6

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S002

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 21/10/2025

Sample Location: MB01 4.20mm - 4.95m Checked By: A.A

**Date**: 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.

**Test performed on:** Fraction passing 425mm sieve

History: As received

Linear shrinkage 13

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## **DETERMINATION OF THE LINEAR SHRINKAGE**

NZS 4402:1986 Test 2.6

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S003

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 21/10/2025

Sample Location: MB02 2.20m - 2.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, grey mottled orange, wet.

Test performed on: Fraction passing 425mm sieve

History: As received

Linear shrinkage 13



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## **DETERMINATION OF THE LINEAR SHRINKAGE**

NZS 4402:1986 Test 2.6

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S004

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 31/10/2025

Sample Location: MB02 5.20m - 5.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of shell fragments to 15mm and organic matter, grey,

wet.

Test performed on: Fraction passing 425mm sieve

History: As received

Linear shrinkage 16

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AS 1289.7.1.1 - 2003

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S001

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 15/10/2025

Sample Location: MB01 2.20m - 2.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, minor fine sands, traces of organic matter, grey mottled orange, wet.

**Test Details:** 

Test performed on: Undisturbed sample - from core

Issue 3

Sample condition on receipt: At natural water content

Coi	Moisture ntent (%): as received	Swell Test Moisture Content @ test completion (%)	Total Swell Strain (%)	Total Shrinkage Strain (%)	Shrink - Swell Index (%)
	34.2	41.3	-0.4	8.5	4.7

Sample condition during shrinkage: No cracking, 0 % Inert Particles.



AS 1289.7.1.1 - 2003

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S002

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 16/10/2025

Sample Location: MB01 4.20mm - 4.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.

**Test Details:** 

Test performed on: Undisturbed sample - from core

Issue 3

Sample condition on receipt: At natural water content

Moisture Content (%): as received	Swell Test Moisture Content @ test completion (%)	Total Swell Strain (%)	Total Shrinkage Strain (%)	Shrink - Swell Index (%)
61.5	61.5 62.6		9.9	5.5

Sample condition during shrinkage:

Some transvese cracking, 0 % Inert Particles.



AS 1289.7.1.1 - 2003

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S002

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 16/10/2025

Sample Location: MB01 4.20mm - 4.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.

**Test Details:** 

Test performed on: Undisturbed sample - from core

Issue 3

Sample condition on receipt: At natural water content

Moisture Content (%): as received	Swell Test Moisture Content @ test completion (%)	Total Swell Strain (%)	Total Shrinkage Strain (%)	Shrink - Swell Index (%)
39.2	39.0	-0.6	8.9	5.0

Sample condition during shrinkage: No cracking, 0 % Inert Particles.



AS 1289.7.1.1 - 2003

**Lab Job No:** 8441-005 **Sample No.:** WRE8441-005-S004

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 28/10/2025

Sample Location: MB02 5.20m - 5.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of shell fragments to 15mm and organic matter, grey, wet.

**Test Details:** 

Test performed on: Undisturbed sample - from core

Sample condition on receipt: At natural water content

Moisture Content (%): as received	Swell Test Moisture Content @ test completion (%)	Total Swell Strain (%)	Total Shrinkage Strain (%)	Shrink - Swell Index (%)
49.5	51.4	-0.1	8.0	4.4

Sample condition during shrinkage:

Some transverse Cracking, 2.2% Inert Particles (shell fragments).



## **DETERMINATION OF THE SOLID DENSITY OF FINE MATERIALS**

NZS 4402:1986 Test 2.7.2

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S001

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 5/11/2025

Sample Location: MB01 2.20m - 2.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, minor fine sands, traces of organic matter, grey mottled orange, wet.

Test performed on: Whole soil
History: As received

Temperature:  $20 \, ^{\circ}\text{C}$   $\rho\text{W}= 0.9982 \, \text{t/m}^{3}$ 

Bottle No.	S9	S10
Solid density of soil particles (ρs) t/m <sup>3</sup>	2.705	2.701
Average solid density (ρs) t/m³	2.7	<b>'</b> 0

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## **DETERMINATION OF THE SOLID DENSITY OF FINE MATERIALS**

NZS 4402:1986 Test 2.7.2

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S002

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 22/10/2025

Sample Location: MB01 4.20mm - 4.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

**Sampling Method:** Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, minor organic matter, dark grey, wet.

Test performed on: Whole soil
History: As received

Temperature: 20 °C  $\rho$ W= 0.9982 t/m<sup>3</sup>

Bottle No.	S9	S10
Solid density of soil particles (ρs) t/m <sup>3</sup>	2.667	2.670
Average solid density (ρs) t/m³	2.6	<b>37</b>



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## **DETERMINATION OF THE SOLID DENSITY OF FINE MATERIALS**

NZS 4402:1986 Test 2.7.2

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S003

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 23/10/2025

Sample Location: MB02 2.20m - 2.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

**Sampling Method:** Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of fine sands, grey mottled orange, wet.

Test performed on: Whole soil
History: As received

Temperature: 20 °C  $\rho$ W= 0.9982 t/m<sup>3</sup>

Bottle No.	M2	M17
Solid density of soil particles (ps) t/m <sup>3</sup>	2.696	2.708
Average solid density (ρs) t/m³	2.7	0



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## **DETERMINATION OF THE SOLID DENSITY OF FINE MATERIALS**

NZS 4402:1986 Test 2.7.2

**Lab Job No:** 8441-005 **Sample No.**: WRE8441-005-S004

Client: Far North Holdings Ltd Tested By: N.K

Project/Site: Old Whangae Date: 4/11/2025

Sample Location: MB02 5.20m - 5.95m Checked By: A.A

**Date:** 11/11/2025

**Date Received:** 13/10/2025

**Date Sampled:** 7/10/2025 **Report No:** WRE8441-005-R001

Sampler: Client REF: AT010024

Sampling Method: Sampled by client – Sampling not accredited

Sample Description: Silty CLAY, traces of shell fragments to 15mm and organic matter, grey, wet.

Test performed on: Whole soil
History: As received

Temperature: 19 °C  $\rho$ W= 0.9984 t/m<sup>3</sup>

Bottle No.	S100	S101
Solid density of soil particles (ρs) t/m <sup>3</sup>	2.688	2.688
Average solid density (ρs) t/m³	2.6	9



### **Christchurch Laboratory**

18B Birmingham Drive, Middleton, Christchurch M: 027 6565 317 E: nick@geocivil.co.nz

## **TEST REPORT**

**Lab Job No:** 8441-005

Your ref.: AT010024

**Date of Issue:** 5/12/2025

Date of Re-Issue:

Test Report No. CHC8441-005-R002

PROJECT: Old Whangae - Conslidation testing

CLIENT: Far North Holdings Ltd

9 Baffin Street, Opua 0200

ATTENTION: C/O PK Engineering Ltd Jonty White

TEST METHODS: Consolidation testing

ASTM D2435/D2435M-11

SAMPLING METHOD: Push Tube - Sampling not accredited

TEST RESULTS: As per attached sheets

M. Adams

Mudams

General Manager Approved Signatory

All results obtained in accordance with the test methods listed above.

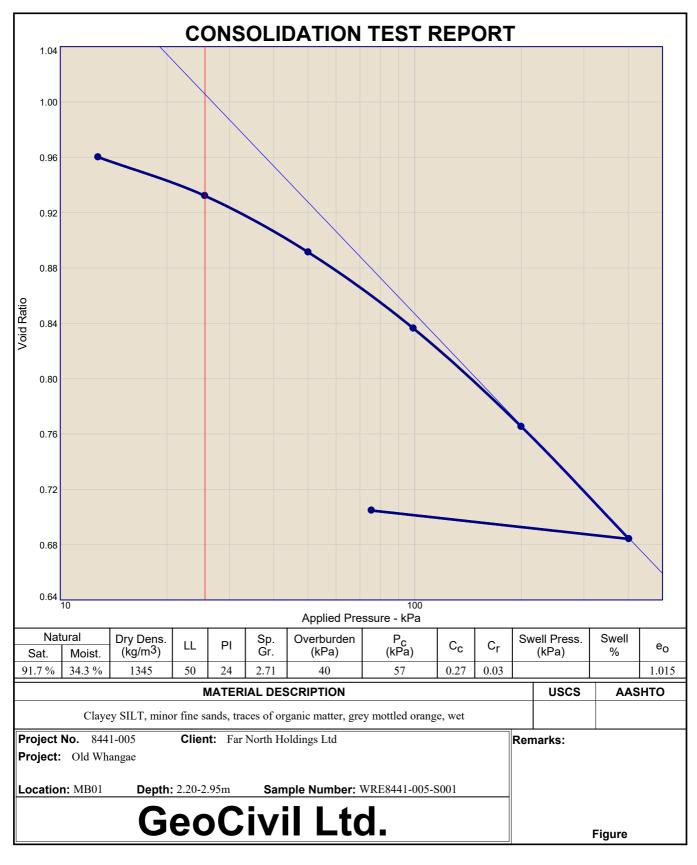
Any material descriptions included in this report are excluded from IANZ endorsement.

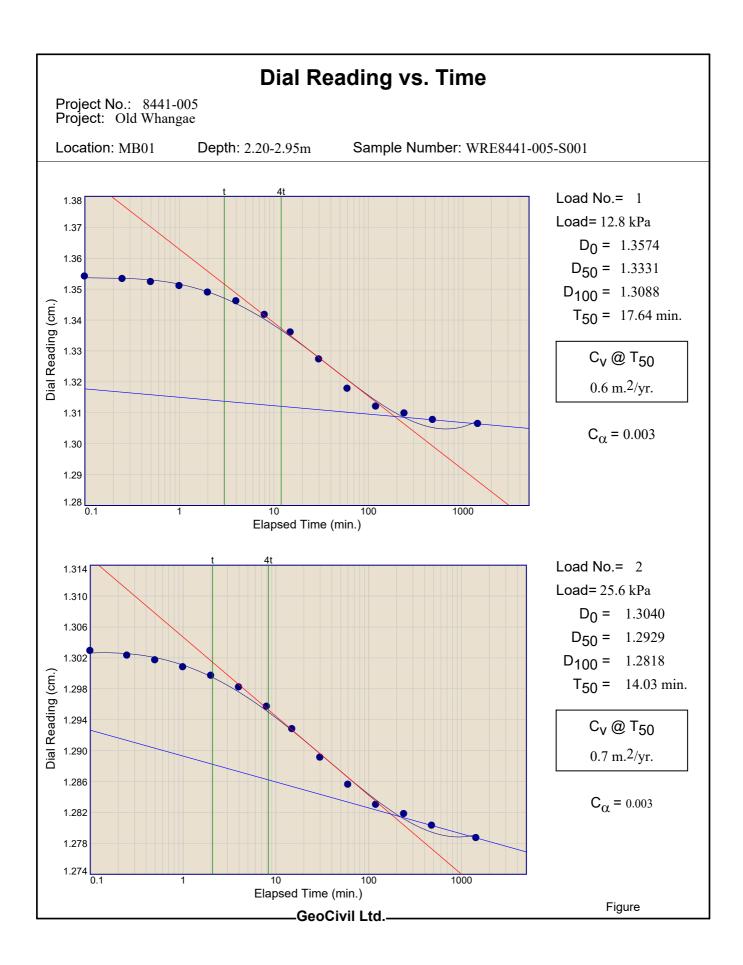
Test results relate only to the sample tested.

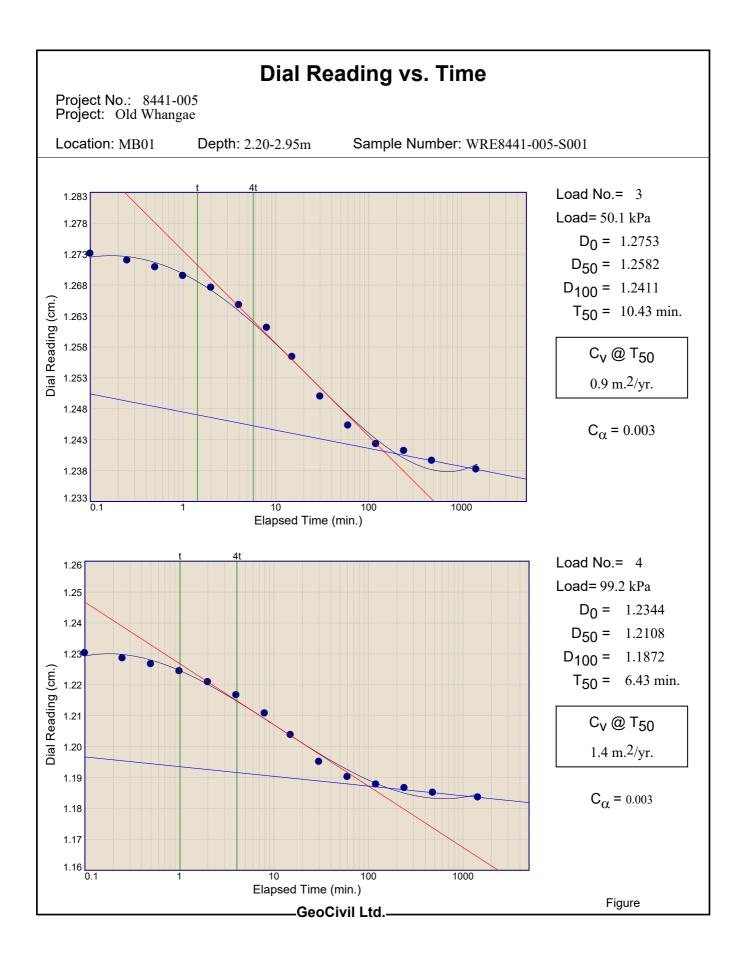


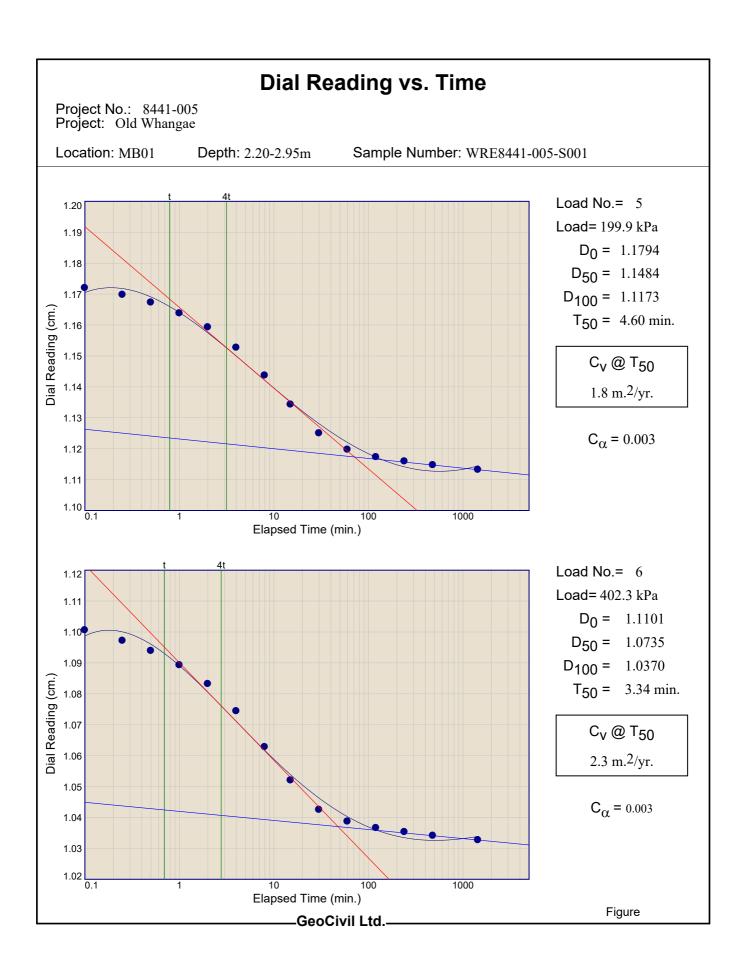
All tests reported herein have been performed in accordance with the laboratory's scope of accreditation

N. van Warmerdam









### **CONSOLIDATION TEST DATA**

5/12/2025

Client: Far North Holdings Ltd

**Project:** Old Whangae **Project Number:** 8441-005

Location: MB01

Liquid Limit: 50 Plasticity Index: 24

Tested by: N.K.

75.6

1.05310

Test Specimen Data							
NATURAL MOISTURE	VOID RATIO	AFTER TEST					
Wet w+t = 255.28 g.	<b>Spec. Gr.</b> = 2.71	Wet w+t = $116.97$ g.					
<b>Dry w+t</b> = 216.85 g.	<b>Est. Ht. Solids =</b> $0.992 \text{ cm}$ .	<b>Dry w+t</b> = $102.04$ g.					
<b>Tare Wt. =</b> 104.92 g.	Init. V.R. = $1.015$	<b>Tare Wt.</b> = $51.39$ g.					
Moisture = 34.3 %	Init. Sat. = 91.7 %	<b>Moisture =</b> 29.5 %					
UNIT WEIGHT	TEST START	<b>Dry Wt.</b> = 50.65 g.					
<b>Height</b> = 1.998 cm.	<b>Height</b> = 1.998 cm.						
Diameter = 4.991 cm.	Diameter = 4.991 cm.						
Weight = 70.63 g.							
<b>Dry Dens. =</b> 1345 kg/m <sup>3</sup>							

End-Of-Load Summary

0.705

15.4 Comprs.

Pressure (kPa)	Final Dial (cm.)	Deformation (cm.)	C <sub>V</sub> (m. <sup>2</sup> /yr.)	$\mathbf{c}_{lpha}$	Void Ratio	% Strain
start	1.36060	0.00000			1.015	
12.8	1.30640	0.05420	0.6	0.003	0.960	2.7 Comprs.
25.6	1.27870	0.08190	0.7	0.003	0.932	4.1 Comprs.
50.1	1.23820	0.12240	0.9	0.003	0.891	6.1 Comprs.
99.2	1.18360	0.17700	1.4	0.003	0.836	8.9 Comprs.
199.9	1.11320	0.24740	1.8	0.003	0.765	12.4 Comprs.
402.3	1.03270	0.32790	2.3	0.003	0.684	16.4 Comprs.

0.30750

Compression index (C<sub>C</sub>), kPa = 0.27 Preconsolidation pressure (P<sub>p</sub>), kPa = 57 Void ratio at P<sub>p</sub> (e<sub>m</sub>) = 0.882 Overburden ( $\sigma_{\text{VO}}$ ), kPa = 40 Void ratio at  $\sigma_{\text{VO}}$  (e<sub>o</sub>) = 0.907 Recompression index (C<sub>r</sub>) = 0.03

\_ GeoCivil Ltd. \_\_\_\_\_



ASTM D2435/D2435M-11

Lab Job No: 8441-005 Tested By: N.K Far North Holdings Ltd 15/10/2025 Client: Date: Old Whangae Project: Checked By: M.A Location: MB01 Date: 5/12/2025

**Depth:** 2.20-2.95m **Report No:** CHC8441-005-R002

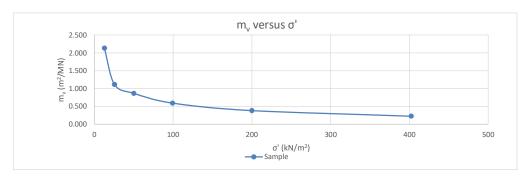
**Sample No.:** WRE8441-005-S001

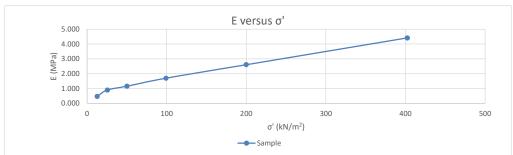
Sample Description: Clayey SILT, minor fine sands, traces of organic matter, grey mottled orange, wet

Void ratio before loading:

1.015
-------

Load (kPa)	e <sub>f</sub>	e <sub>0</sub>	σ' (kN/m²)	σ' <sub>0</sub> (kN/m <sup>2</sup> )	$\Delta\sigma'$ (kN/m <sup>2</sup> )	m <sub>v</sub> (m <sup>2</sup> /MN)	E (MPa)	C <sub>v</sub> (m <sup>2</sup> /yr)	k (m/s)
12.8	0.960	1.015	12.8	0	12.8	2.132	0.469	0.6	3.979E-10
25.6	0.932	0.960	25.6	12.8	12.8	1.116	0.896	0.7	2.430E-10
50.1	0.891	0.932	50.1	25.6	24.5	0.866	1.154	0.9	2.424E-10
99.2	0.836	0.891	99.2	50.1	49.1	0.592	1.688	1.4	2.579E-10
199.9	0.765	0.836	199.9	99.2	100.7	0.384	2.604	1.8	2.150E-10
402.3	0.684	0.765	402.3	199.9	202.4	0.227	4.410	2.3	1.622E-10





Note: It may not be possible to calculate a Cv for fast consolidating materials, or for low pressure cycles.



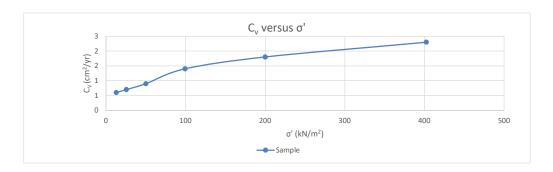
ASTM D2435/D2435M-11

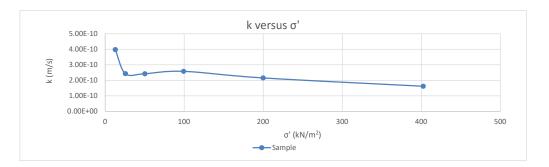
Lab Job No: 8441-005 Tested By: N.K Client: Far North Holdings Ltd Date: 15/10/2025 Project: Old Whangae Checked By: M.A Location: MB01 Date: 5/12/2025

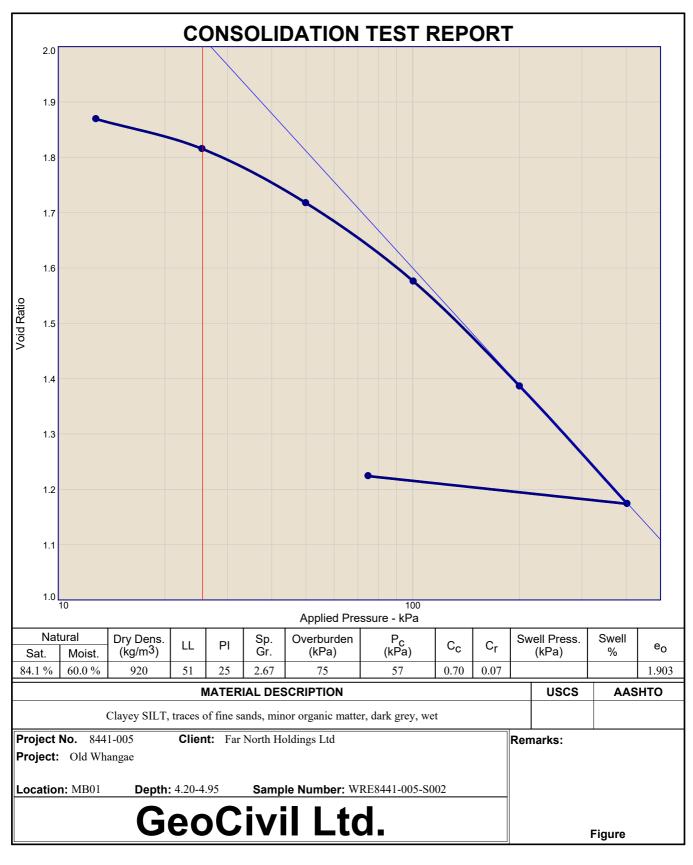
**Depth:** 2.20-2.95m **Report No:** CHC8441-005-R002

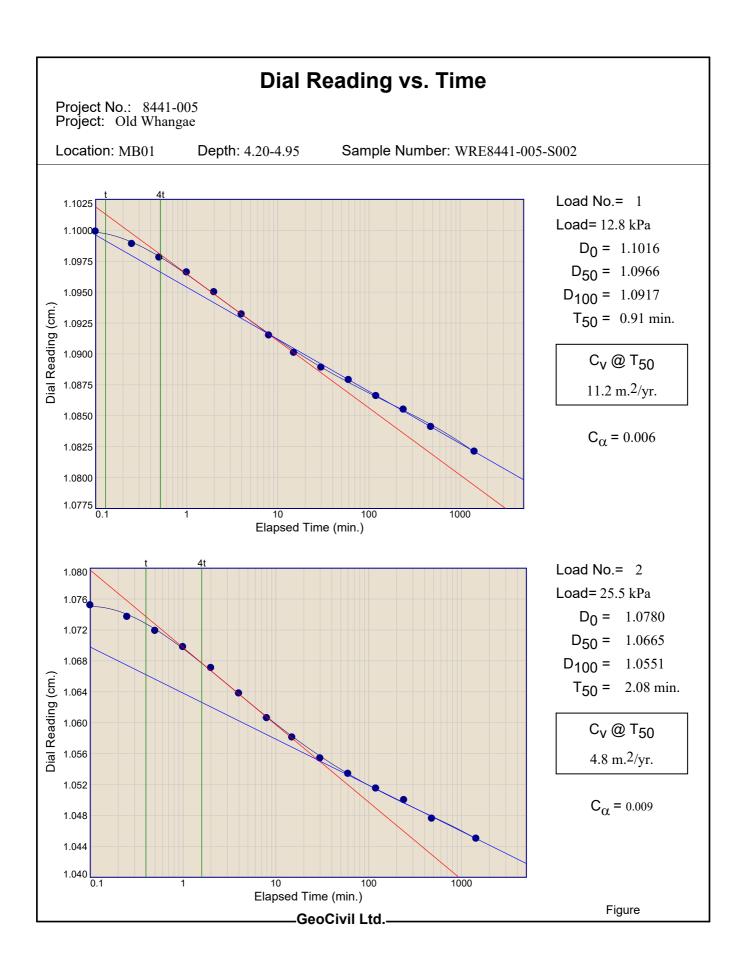
**Sample No.:** WRE8441-005-S001

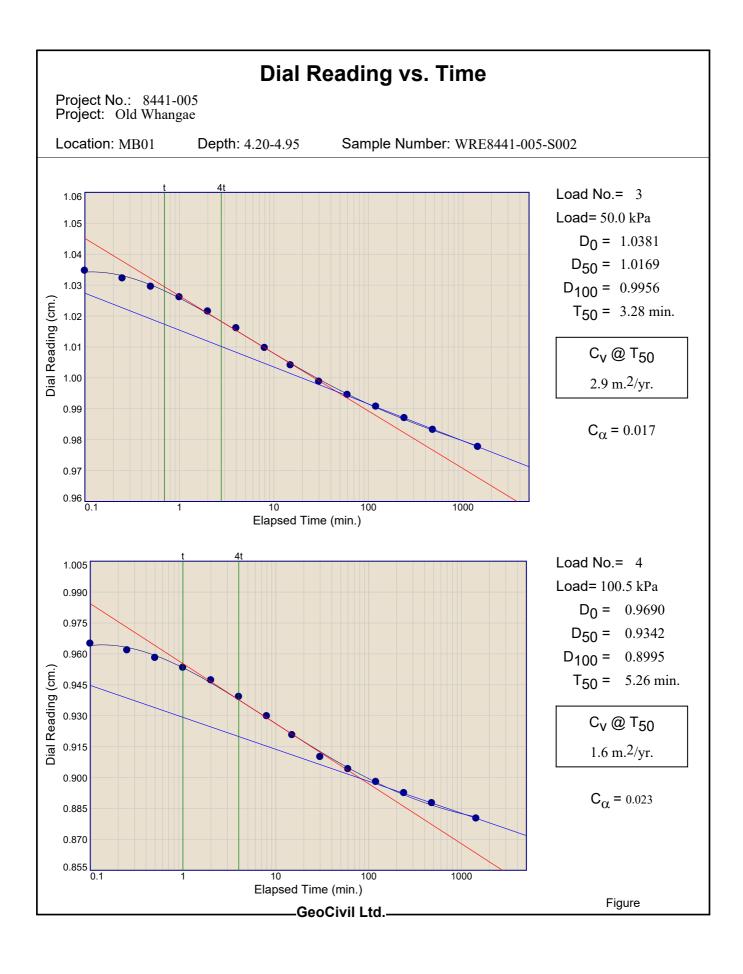
Sample Description: Clayey SILT, minor fine sands, traces of organic matter, grey mottled orange, wet

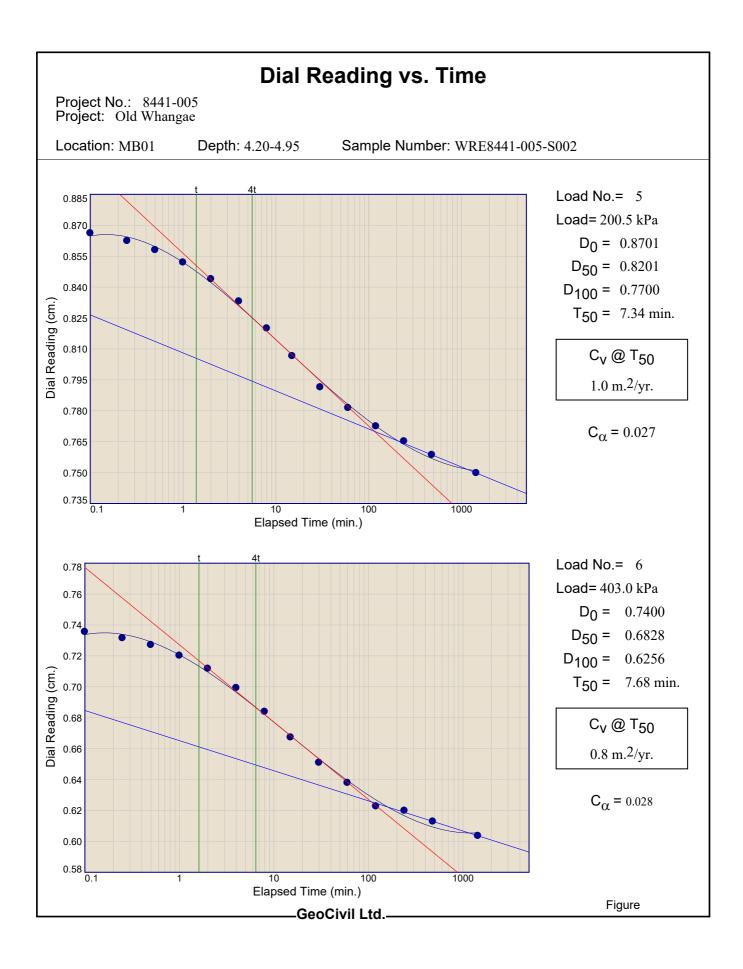












### **CONSOLIDATION TEST DATA**

5/12/2025

Client: Far North Holdings Ltd

**Project:** Old Whangae **Project Number:** 8441-005

Location: MB01

**Depth:** 4.20-4.95 **Sample Number:** WRE8441-005-S002 **Material Description:** Clayey SILT, traces of fine sands, minor organic matter, dark grey, wet

Liquid Limit: 51 Plasticity Index: 25

Tested by: N.K.

Test Specimen Data									
NATURAL MOISTURE	VOID RATIO	AFTER TEST							
Wet w+t = 223.73 g.	<b>Spec. Gr.</b> = 2.67	Wet w+t = $103.05$ g.							
<b>Dry w+t</b> = 179.04 g.	Est. Ht. Solids = $0.688$ cm.	<b>Dry w+t</b> = $84.72 \text{ g}$ .							
<b>Tare Wt.</b> = 104.53 g.	Init. V.R. = 1.903	<b>Tare Wt.</b> = $51.14 \text{ g.}$							
Moisture = 60.0 %	Init. Sat. = 84.1 %	<b>Moisture =</b> 54.6 %							
UNIT WEIGHT	TEST START	<b>Dry Wt.</b> = 33.58 g.							
Height = 1.998 cm.	<b>Height</b> = 1.998 cm.								
<b>Diameter =</b> 4.996 cm.	<b>Diameter</b> = 4.996 cm.								
Weight = 57.62 g.									
Dry Dens. = $920 \text{ kg/m}^3$									

			Ellu	-OI-LOau	Sullillary	
Pressure (kPa)	Final Dial (cm.)	Deformation (cm.)	C <sub>V</sub> (m. <sup>2</sup> /yr.)	$c_{lpha}$	Void Ratio	% Strain
start	1.10560	0.00000			1.903	
12.8	1.08210	0.02350	11.2	0.006	1.869	1.2 Comp

start	1.10560	0.00000			1.903	
12.8	1.08210	0.02350	11.2	0.006	1.869	1.2 Comprs.
25.5	1.04500	0.06060	4.8	0.009	1.815	3.0 Comprs.
50.0	0.97770	0.12790	2.9	0.017	1.717	6.4 Comprs.
100.5	0.88020	0.22540	1.6	0.023	1.576	11.3 Comprs.
200.5	0.74980	0.35580	1.0	0.027	1.386	17.8 Comprs.
403.0	0.60360	0.50200	0.8	0.028	1.174	25.1 Comprs.
75.0	0.63810	0.46750			1.224	23.4 Comprs.

Compression index (C<sub>c</sub>), kPa = 0.70 Preconsolidation pressure (P<sub>p</sub>), kPa = 57 Void ratio at P<sub>p</sub> (e<sub>m</sub>) = 1.694 Overburden ( $\sigma_{\text{VO}}$ ), kPa = 75 Void ratio at  $\sigma_{\text{VO}}$  (e<sub>o</sub>) = 1.641 Recompression index (C<sub>r</sub>) = 0.07

GeoCivil Ltd. \_\_\_\_\_



ASTM D2435/D2435M-11

Lab Job No: 8441-005 Tested By: N.K Client: Far North Holdings Ltd 16/10/2025 Date: Old Whangae Project: Checked By: M.A Location: MB01 Date: 5/12/2025

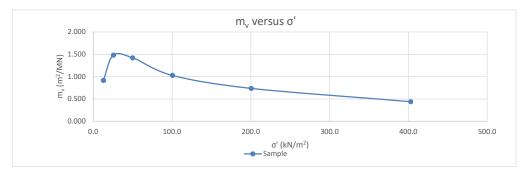
**Depth:** 4.20-4.95m **Report No:** CHC8441-005-R002

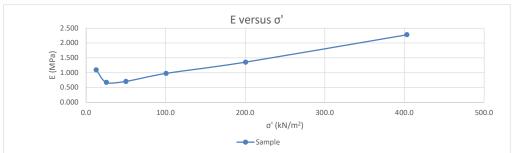
**Sample No.:** WRE8441-005-S002

Sample Description: Clayey SILT, traces of fine sands, minor organic matter, dark grey, wet

Void ratio before loading: 1.903

Load (kPa)	e <sub>f</sub>	e <sub>0</sub>	$\sigma' (kN/m^2)$	σ' <sub>0</sub> (kN/m <sup>2</sup> )	$\Delta\sigma'$ (kN/m <sup>2</sup> )	m <sub>v</sub> (m <sup>2</sup> /MN)	E (MPa)	C <sub>v</sub> (m <sup>2</sup> /yr)	k (m/s)
12.8	1.869	1.903	12.8	0.0	12.8	0.915	1.093	11.2	3.187E-09
25.5	1.815	1.869	25.5	12.8	12.7	1.482	0.675	4.8	2.212E-09
50.0	1.717	1.815	50.0	25.5	24.5	1.421	0.704	2.9	1.282E-09
100.5	1.576	1.717	100.5	50.0	50.5	1.028	0.973	1.6	5.114E-10
200.5	1.386	1.576	200.5	100.5	100.0	0.738	1.356	1.0	2.294E-10
403.0	1.174	1.386	403.0	200.5	202.5	0.439	2.279	0.8	1.092E-10





 $Note: It \ may \ not \ be \ possible \ to \ calculate \ a \ Cv \ for \ fast \ consolidating \ materials, \ or \ for \ low \ pressure \ cycles.$ 



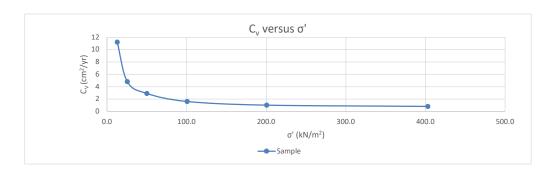
### Consolidometer Test ASTM D2435/D2435M-11

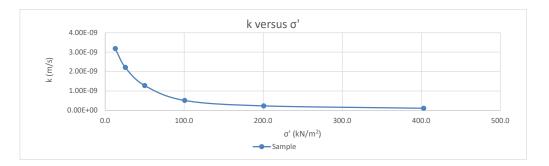
Lab Job No: 8441-005 Tested By: N.K Client: Far North Holdings Ltd Date: 16/10/2025 Project: Old Whangae Checked By: M.A Location: MB01 Date: 5/12/2025

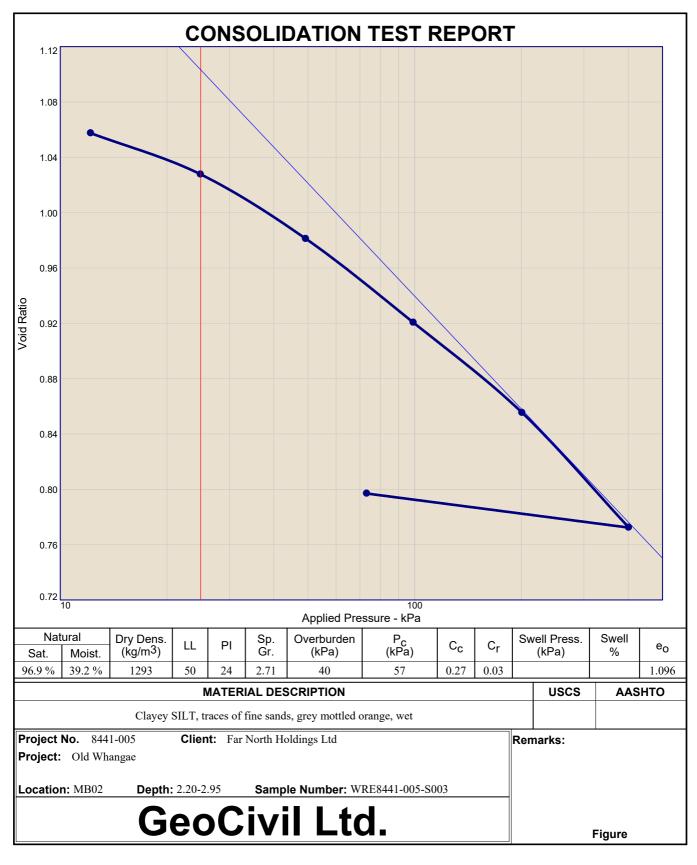
**Depth:** 4.20-4.95m **Report No:** CHC8441-005-R002

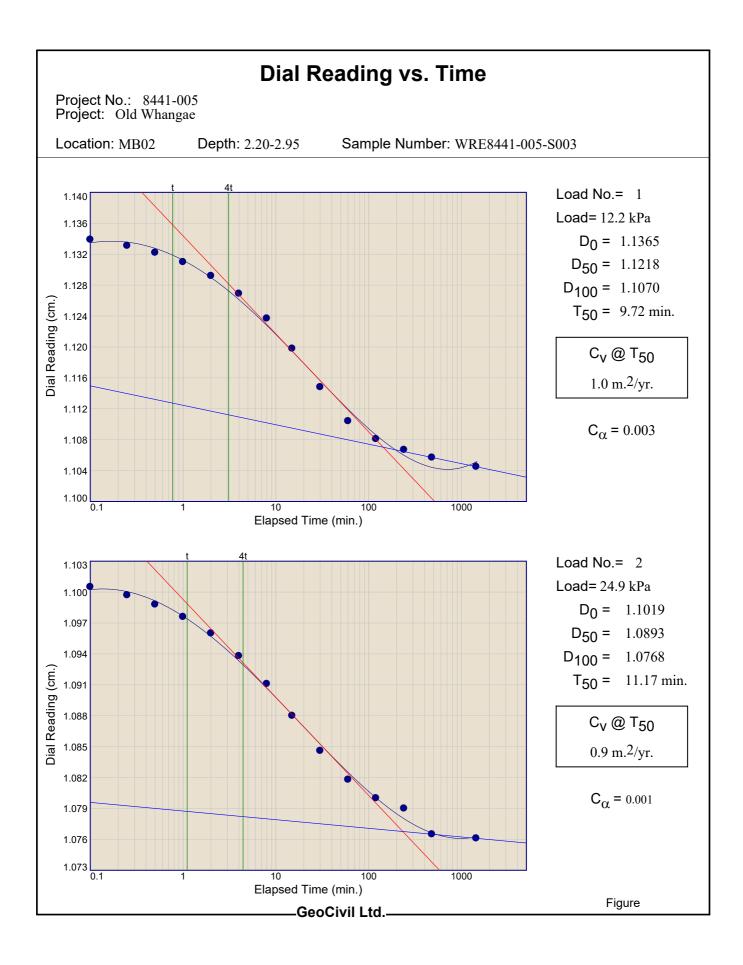
Sample No.: WRE8441-005-S002

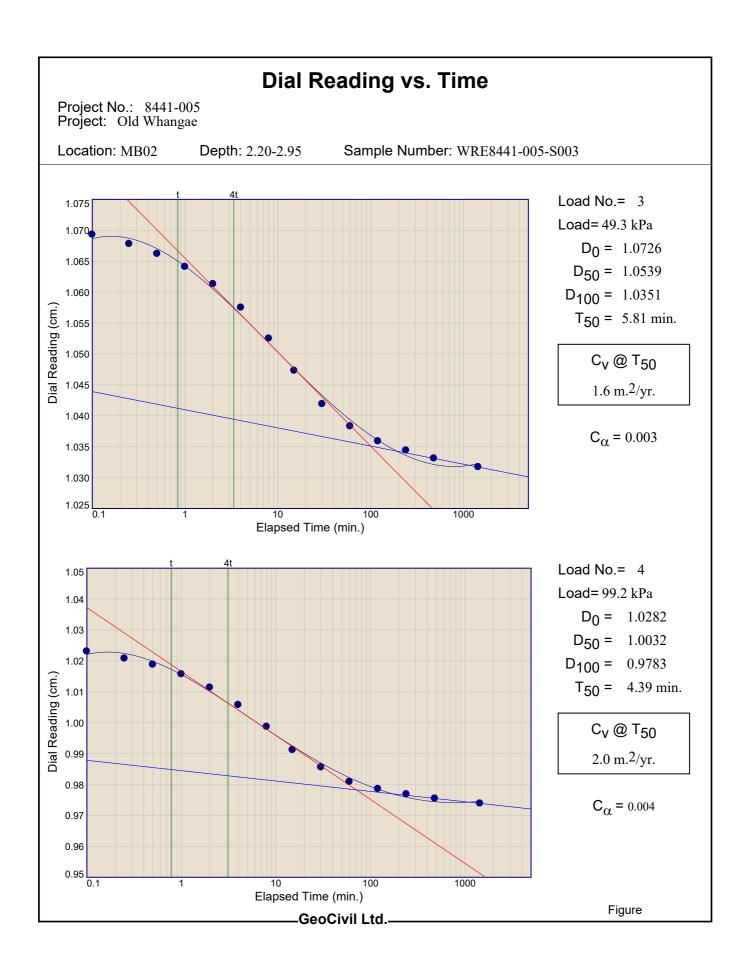
Sample Description: Clayey SILT, traces of fine sands, minor organic matter, dark grey, wet

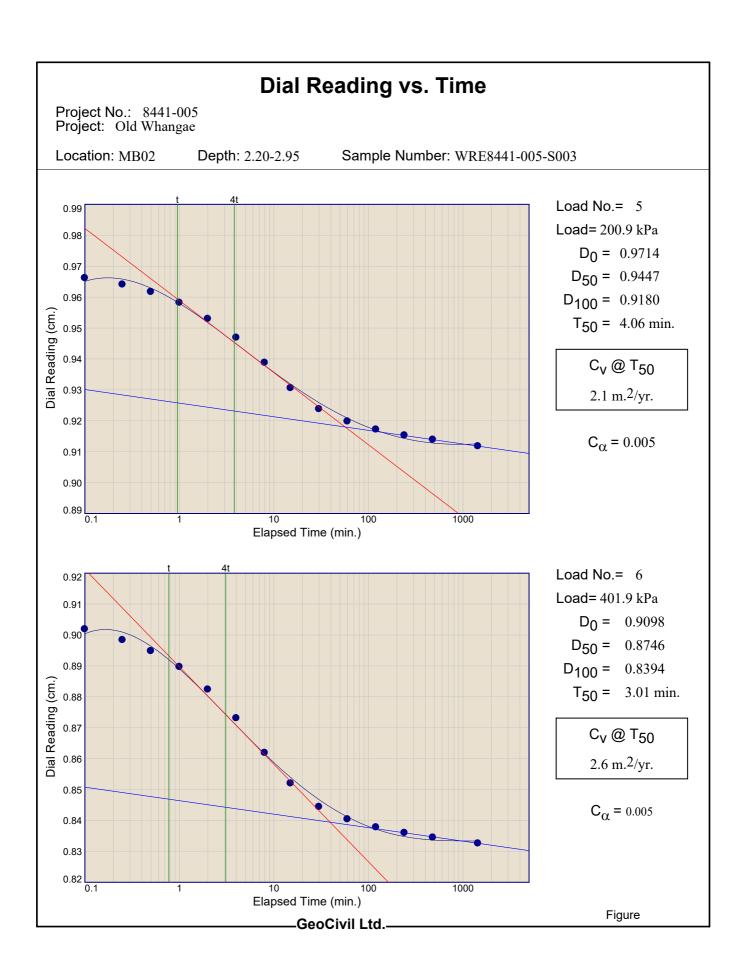








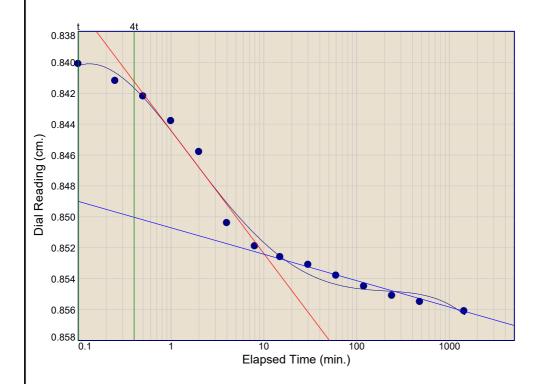






Project No.: 8441-005 Project: Old Whangae

Location: MB02 Depth: 2.20-2.95 Sample Number: WRE8441-005-S003



Load No.= 7 Load= 73.3 kPa  $D_0 = 0.8388$   $D_{50} = 0.8456$   $D_{100} = 0.8524$  $T_{50} = 1.41 \text{ min.}$ 

> C<sub>V</sub> @ T<sub>50</sub> 5.3 m.2/yr.

-GeoCivil Ltd. Figure

### **CONSOLIDATION TEST DATA**

5/12/2025

Client: Far North Holdings Ltd

**Project:** Old Whangae **Project Number:** 8441-005

Location: MB02

**Depth:** 2.20-2.95 **Sample Number:** WRE8441-005-S003

**Material Description:** Clayey SILT, traces of fine sands, grey mottled orange, wet **Liquid Limit:** 50 **Plasticity Index:** 24

Tested by: N.K

	Test Specimen Data	
NATURAL MOISTURE	VOID RATIO	AFTER TEST
Wet w+t = 232.33 g.	<b>Spec. Gr.</b> = $2.71$	Wet w+t = $119.98$ g.
<b>Dry w+t</b> = 197.21 g.	<b>Est. Ht. Solids =</b> $0.953$ cm.	<b>Dry w+t</b> = $103.37$ g.
<b>Tare Wt. =</b> 107.58 g.	Init. V.R. = $1.096$	<b>Tare Wt.</b> = $52.90 \text{ g}$ .
Moisture = 39.2 %	Init. Sat. = 96.9 %	Moisture = $32.9\%$
UNIT WEIGHT	TEST START	<b>Dry Wt.</b> = 50.48 g.
<b>Height =</b> 1.998 cm.	<b>Height</b> = 1.998 cm.	
<b>Diameter =</b> 5.003 cm.	<b>Diameter</b> = $5.003$ cm.	
Weight = 70.70 g.		
Dry Dens = $1293 \text{ kg/m}^3$		

End-Of-Load Summary

vvoigiit	10.10	5.
Dry Dens. =	1293	kg/m <sup>3</sup>

Pressure (kPa)	Final Dial (cm.)	Deformation (cm.)	C <sub>V</sub> (m. <sup>2</sup> /yr.)	$\mathbf{c}_{lpha}$	Void Ratio	% Strain
start	1.14100	0.00000			1.096	
12.2	1.10450	0.03650	1.0	0.003	1.057	1.8 Comprs.
24.9	1.07610	0.06490	0.9	0.001	1.028	3.2 Comprs.
49.3	1.03170	0.10930	1.6	0.003	0.981	5.5 Comprs.
99.2	0.97390	0.16710	2.0	0.004	0.920	8.4 Comprs.
200.9	0.91180	0.22920	2.1	0.005	0.855	11.5 Comprs.
401.9	0.83260	0.30840	2.6	0.005	0.772	15.4 Comprs.
73.3	0.85610	0.28490	5.3		0.797	14.3 Comprs.

Compression index (C<sub>C</sub>), kPa = 0.27 Preconsolidation pressure (P<sub>p</sub>), kPa = 57 Void ratio at P<sub>p</sub> (e<sub>m</sub>) = 0.969 Overburden ( $\sigma_{\text{VO}}$ ), kPa = 40 Void ratio at  $\sigma_{\text{VO}}$  (e<sub>o</sub>) = 0.997 Recompression index (C<sub>r</sub>) = 0.03

\_ GeoCivil Ltd. \_\_\_\_\_



ASTM D2435/D2435M-11

N.K Lab Job No: 8441-005 Tested By: Client: Far North Holdings Ltd 16/10/2025 Date: Old Whangae Project: Checked By: M.A Location: MB02 Date: 5/12/2025

**Depth:** 2.20-2.95m **Report No:** CHC8441-005-R002

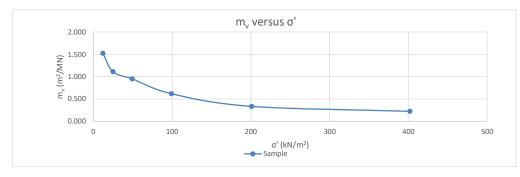
**Sample No.:** WRE8441-005-S003

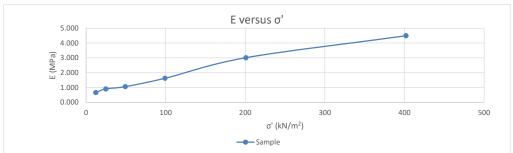
Sample Description: Clayey SILT, traces of fine sands, grey mottled orange, wet

Void ratio before loading:

Load (kPa)	e <sub>f</sub>	e <sub>0</sub>	$\sigma'$ (kN/m <sup>2</sup> )	$\sigma'_0$ (kN/m <sup>2</sup> )	$\Delta\sigma'$ (kN/m <sup>2</sup> )	m <sub>v</sub> (m <sup>2</sup> /MN)	E (MPa)	C <sub>V</sub> (m <sup>2</sup> /yr)	k (m/s)
12.2	1.057	1.096	12.2	0	12.2	1.525	0.656	1.0	4.743E-10
24.9	1.028	1.057	24.9	12.2	12.7	1.110	0.901	0.9	3.107E-10
49.3	0.981	1.028	49.3	24.9	24.4	0.950	1.053	1.6	4.726E-10
99.2	0.920	0.981	99.2	49.3	49.9	0.617	1.621	2.0	3.838E-10
200.9	0.855	0.920	200.9	99.2	101.7	0.333	3.004	2.1	2.174E-10
401.9	0.772	0.855	401.9	200.9	201	0.223	4.492	2.6	1.800E-10

1.096





 $Note: It \ may \ not \ be \ possible \ to \ calculate \ a \ Cv \ for \ fast \ consolidating \ materials, \ or \ for \ low \ pressure \ cycles.$ 



### Consolidometer Test ASTM D2435/D2435M-11

 Lab Job No:
 8441-005
 Tested By:
 N.K

 Client:
 Far North Holdings Ltd
 Date:
 16/10/2025

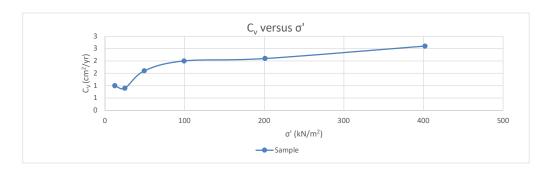
 Project:
 Old Whangae
 Checked By:
 M.A

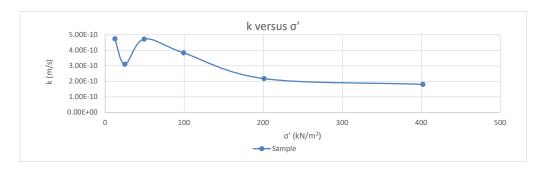
 Location:
 MB02
 Date:
 5/12/2025

 Depth:
 2.20-2.95m
 Report No:
 CHC8441-005-R002

Sample No.: WRE8441-005-S003

Sample Description: Clayey SILT, traces of fine sands, grey mottled orange, wet







### Whangarei Laboratory

166 Bank Street, Whangarei M: 022 590 3121 E: james@geocivil.co.nz

# **TEST REPORT**

**Lab Job No**: 8441-005

Your ref.: AT010024

**Date of Issue:** 8/12/2025

Date of Re-Issue:

Test Report No. WRE8441-005-R003

PROJECT: Old Whangae - Consolidation Analysis

CLIENT: Far North Holdings Ltd

9 Baffin Street, Opua 0200

ATTENTION: C/O PK Engineering Ltd Jonty White

TEST METHODS: Consolidation testing

ASTM D2435/D2435M-11

SAMPLING METHOD: Push Tube - Sampling not accredited

TEST RESULTS: As per attached sheets

S. Kokich

D. Krissansen

Senior Technician Approved Signatory

All results obtained in accordance with the test methods listed above.

Any material descriptions included in this report are excluded from IANZ endorsement.

Test results relate only to the sample tested.



All tests reported herein have been performed in accordance with the laboratory's scope of accreditation



ASTM D2435/D2435M-11

Lab Job No: 8441-005

Tested By: N.K Client: Far North Holdings Ltd Date: 28/10/2025 Old Whangae Checked By: D.K. Project: MB02 8/12/2025 Location: Date: Report No: WRE8441-005-R003

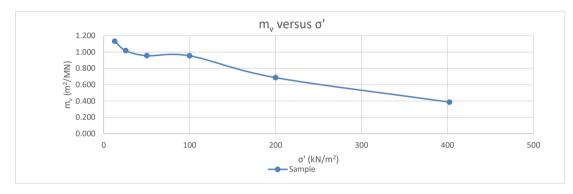
Depth: 5.20 - 5.95m WRE8441-005-S004 Sample No.:

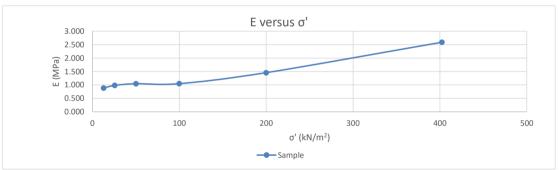
Clayey SILT, traces of shells to 15mm, traces organics, grey, wet. Sample Description:

Void ratio before loading:

1.414

Load (kPa)	e <sub>f</sub>	e <sub>0</sub>	$\sigma'$ (kN/m <sup>2</sup> )	$\sigma'_0$ (kN/m <sup>2</sup> )	$\Delta\sigma'$ (kN/m <sup>2</sup> )	m <sub>v</sub> (m <sup>2</sup> /MN)	E (MPa)	C <sub>v</sub> (m <sup>2</sup> /yr)	k (m/s)
12.8	1.379	1.414	12.8	0	12.8	1.133	0.883	2.3	8.102E-10
25.6	1.348	1.379	25.6	12.8	12.8	1.018	0.982	1.6	5.066E-10
50.1	1.293	1.348	50.1	25.6	24.5	0.956	1.046	3.5	1.041E-09
99.9	1.184	1.293	99.9	50.1	49.8	0.955	1.048	0.9	2.672E-10
199.9	1.034	1.184	199.9	99.9	100	0.687	1.456	1.0	2.136E-10
402.3	0.875	1.034	402.3	199.9	202.4	0.386	2.589	1.3	1.561E-10





 $Note: It \ may \ not \ be \ possible \ to \ calculate \ a \ Cv \ for \ fast \ consolidating \ materials, \ or \ for \ low \ pressure \ cycles.$ 



ASTM D2435/D2435M-11

Lab Job No: 8441-005 Client: Far North Holdings Ltd

Project: Old Whangae Location: MB02

Depth: 5.20 - 5.95m

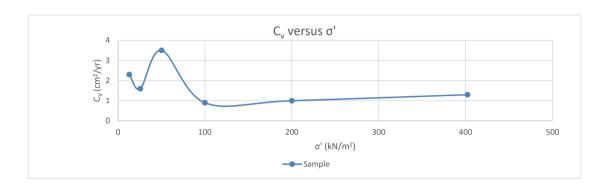
WRE8441-005-S004 Sample No.:

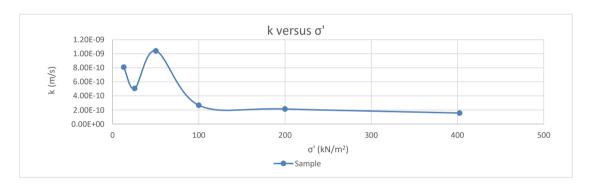
Tested By: N.K Date: 28/10/2025

Checked By: D.K. Date: 8/12/2025

Report No: WRE8441-005-R003

Sample Description: Clayey SILT, traces of shells to 15mm, traces organics, grey, wet.





### **CONSOLIDATION TEST DATA**

Client: Far North Holdings Ltd

Project: Old Whangae Project Number: 8441-005

Location: MB02

**Depth:** 5.20 - 5.95m **Sample Number:** WRE8441-005-S004

Material Description: Clayey SILT, traces of shells to 15mm, traces organics, grey, wet. Tested by: N.K. Checked by: D.K.

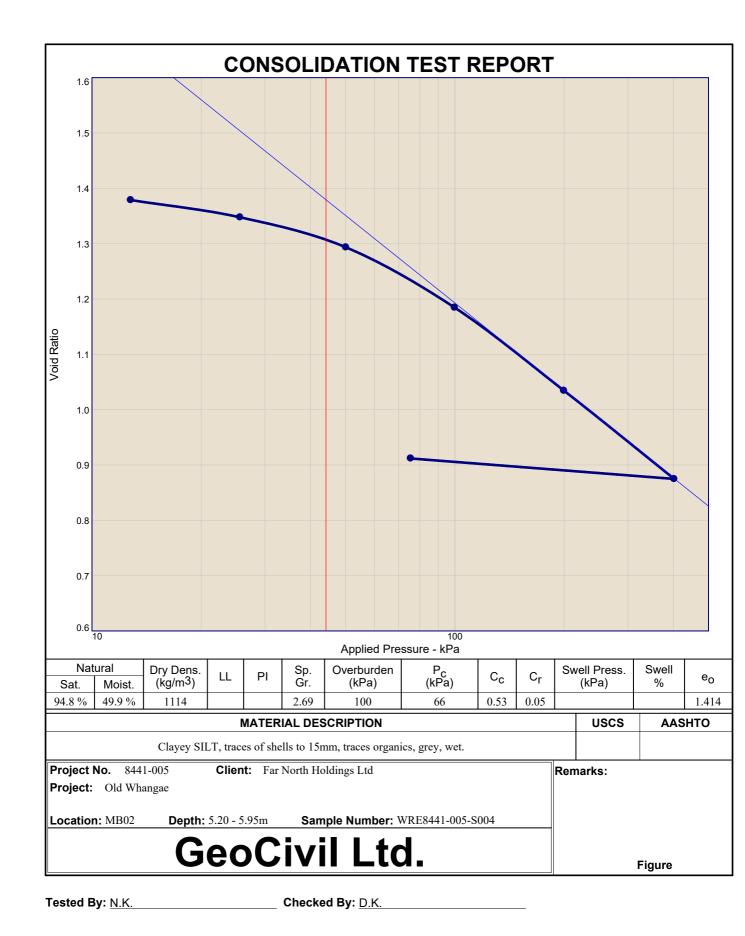
	Test Specimen Data	
NATURAL MOISTURE	VOID RATIO	AFTER TEST
Wet w+t = 209.12 g.	<b>Spec. Gr.</b> = 2.69	Wet w+t = $112.15 \text{ g}$ .
<b>Dry w+t</b> = 174.45 g.	<b>Est. Ht. Solids =</b> $0.828 \text{ cm}$ .	<b>Dry w+t</b> = $96.25 \text{ g}$ .
<b>Tare Wt.</b> = 104.94 g.	Init. V.R. = $1.414$	<b>Tare Wt.</b> = $53.15$ g.
<b>Moisture =</b> 49.9 %	Init. Sat. = 94.8 %	<b>Moisture =</b> 36.9 %
UNIT WEIGHT	TEST START	<b>Dry Wt.</b> = 43.10 g.
Height = 1.998 cm.	<b>Height</b> = 1.998 cm.	
Diameter = 4.991 cm.	<b>Diameter</b> = 4.991 cm.	
Weight = $65.27  \text{g}$		

Diameter = 4.991 cm. Weight = 65.27 g. Dry Dens. = 1114 kg/m<sup>3</sup>

			End-C	f-Load Sun	nmary			
Pressure (kPa)	Final Dial (cm.)	Machine Defl. (cm.)	Deformation (cm.)	C <sub>V</sub> (m. <sup>2</sup> /yr.)	$c_{lpha}$	Void Ratio	% Strain	
start	1.10090		0.00000			1.414		
12.8	1.06870	0.00270	0.02950	2.3	0.003	1.379	1.5 Comprs.	
25.6	1.04340	0.00030	0.05720	1.6	0.004	1.348	2.8 Comprs.	
50.1	0.99990	0.00080	0.10020	3.5	0.008	1.293	5.0 Comprs.	
99.9	0.90780	0.00270	0.19040	0.9	0.014	1.184	9.5 Comprs.	
199.9	0.78410	0.00220	0.31460	1.0	0.014	1.034	15.7 Comprs.	
402.3	0.65140	0.00290	0.44660	1.3	0.013	0.875	22.4 Comprs.	
75.6	0.68270	0.00220	0.41600	3.1		0.912	20.8 Comprs.	
0.0	0.68270	0.00220	0.41600				_	

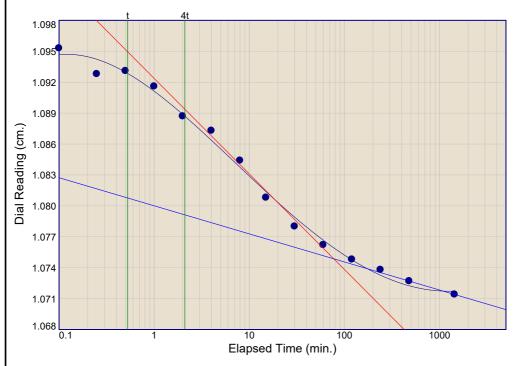
Compression index (C<sub>C</sub>), kPa = 0.53 Preconsolidation pressure (P<sub>p</sub>), kPa = 66 Void ratio at P<sub>p</sub> (e<sub>m</sub>) = 1.256 Overburden ( $\sigma_{VO}$ ), kPa = 100 Void ratio at  $\sigma_{VO}$  (e<sub>O</sub>) = 1.184 Recompression index (C<sub>r</sub>) = 0.05

\_\_\_\_ GeoCivil Ltd. \_\_\_\_\_



Project No.: 8441-005 Project: Old Whangae

Location: MB02 Depth: 5.20 - 5.95m Sample Number: WRE8441-005-S004



Load No.= 1 Load= 12.8 kPa

 $D_0 = 1.0970$ 

 $D_{50} = 1.0859$ 

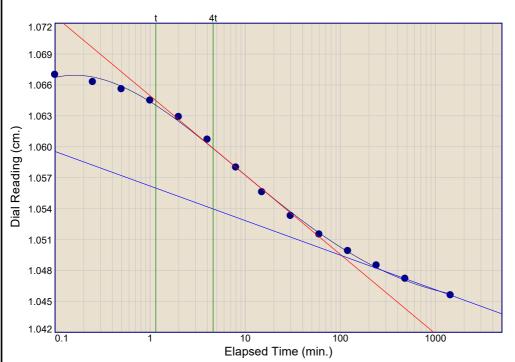
 $D_{100} = 1.0749$ 

 $T_{50} = 4.48 \text{ min.}$ 

 $\mathtt{C_{V}} \ @ \ \mathtt{T_{50}}$ 

2.3 m.<sup>2</sup>/yr.

 $C_{\alpha} = 0.003$ 



GeoCivil Ltd.

Load No.= 2

Load= 25.6 kPa

 $D_0 = 1.0682$ 

 $D_{50} = 1.0588$ 

 $D_{100} = 1.0494$ 

 $T_{50} = 6.25 \text{ min.}$ 

 $C_v @ T_{50}$ 

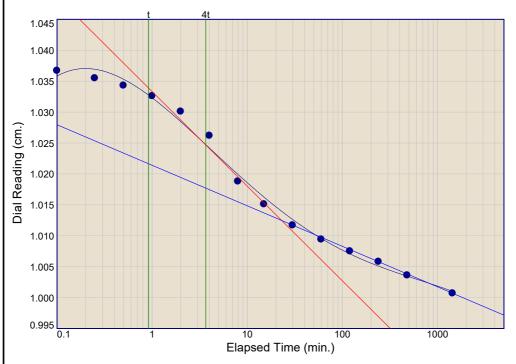
1.6 m.2/yr.

 $C_{\alpha} = 0.004$ 

Figure

Project No.: 8441-005 Project: Old Whangae

Location: MB02 Depth: 5.20 - 5.95m Sample Number: WRE8441-005-S004



Load No.= 3 Load= 50.1 kPa

 $D_0 = 1.0408$ 

 $D_{50} = 1.0266$ 

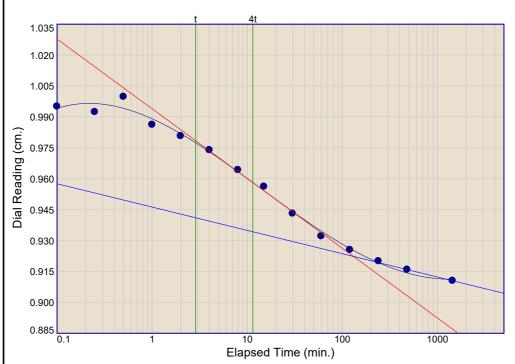
 $D_{100} = 1.0125$ 

 $T_{50} = 2.71 \text{ min.}$ 

 $\mathtt{C_{V}} \ @ \ \mathtt{T_{50}}$ 

3.5 m.2/yr.

 $C_{\alpha} = 0.008$ 



GeoCivil Ltd.

Load No.= 4

Load= 99.9 kPa

 $D_0 = 0.9968$ 

 $D_{50} = 0.9596$ 

 $D_{100} = 0.9223$ 

 $T_{50} = 10.35 \text{ min.}$ 

C<sub>V</sub> @ T<sub>50</sub>

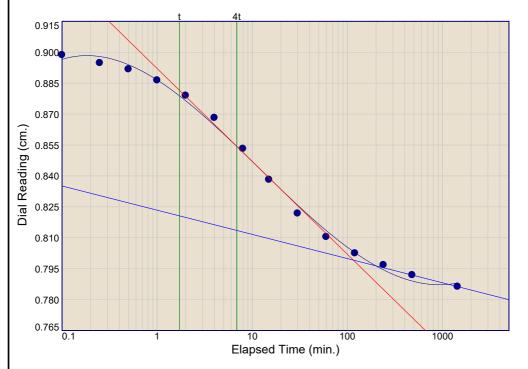
 $0.9 \text{ m.}^{2/\text{yr.}}$ 

 $C_{\alpha} = 0.014$ 

Figure

Project No.: 8441-005 Project: Old Whangae

Location: MB02 Depth: 5.20 - 5.95m Sample Number: WRE8441-005-S004



Load No.= 5 Load= 199.9 kPa

 $D_0 = 0.9035$ 

 $D_{50} = 0.8513$ 

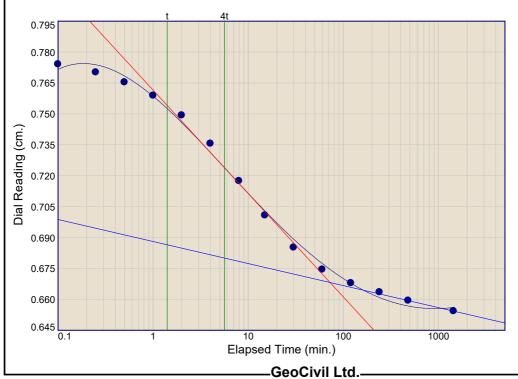
 $D_{100} = 0.7992$ 

 $T_{50} = 8.03 \text{ min.}$ 

C<sub>v</sub> @ T<sub>50</sub>

1.0 m.<sup>2</sup>/yr.

 $C_{\alpha} = 0.014$ 



Load No.= 6

Load= 402.3 kPa

 $D_0 = 0.7813$ 

 $D_{50} = 0.7247$ 

 $D_{100} = 0.6682$ 

 $T_{50} = 5.41 \text{ min.}$ 

 $C_{V} @ T_{50}$ 

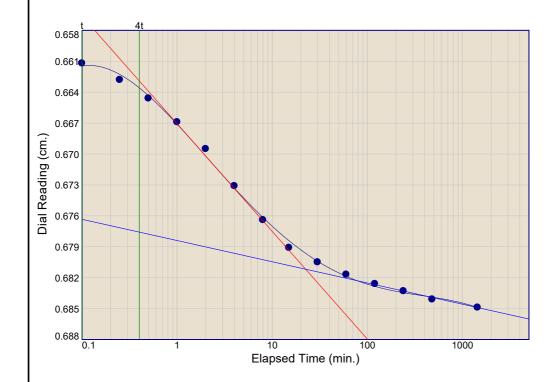
1.3 m.2/yr.

 $C_{\alpha} = 0.013$ 

Figure

Project No.: 8441-005 Project: Old Whangae

Location: MB02 Depth: 5.20 - 5.95m Sample Number: WRE8441-005-S004



Load No.= 7 Load= 75.6 kPa

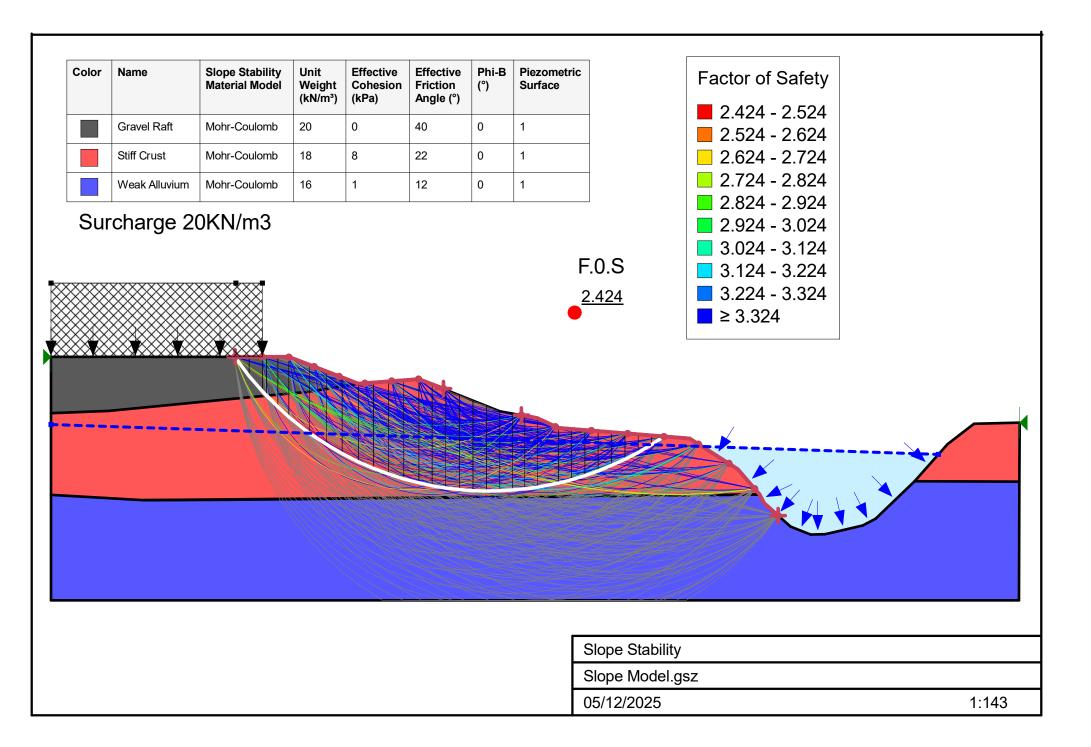
 $D_0 = 0.6594$ 

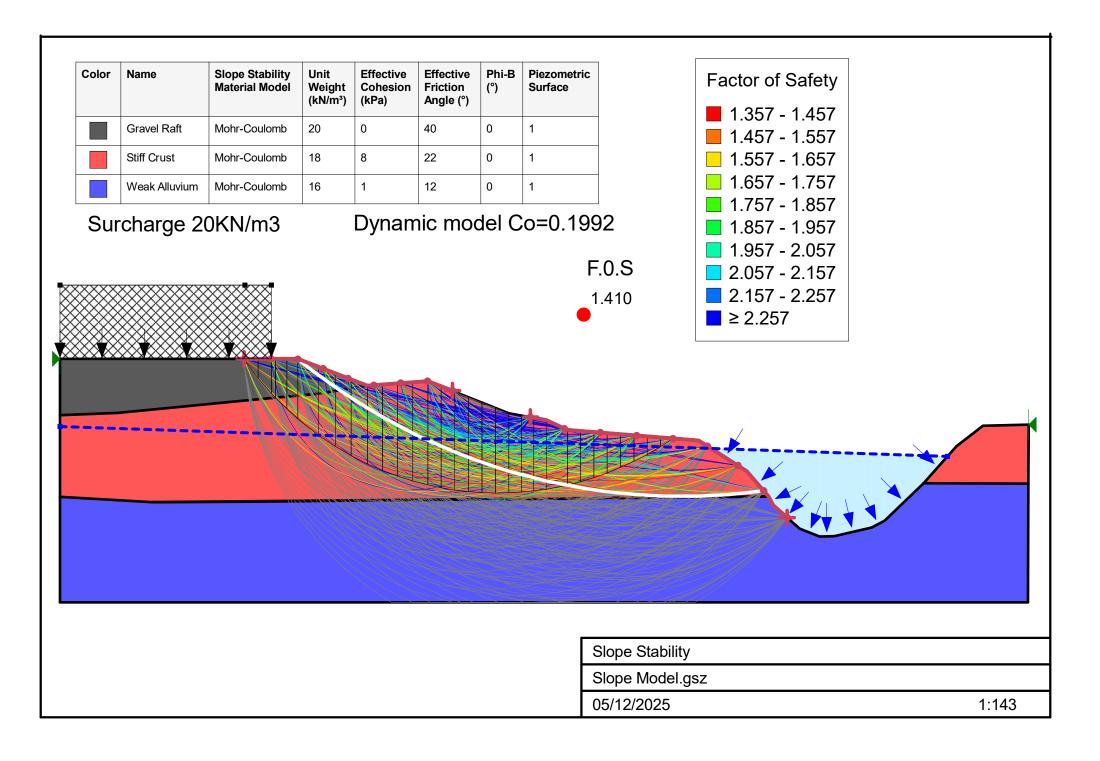
 $D_{50} = 0.6703$ 

 $D_{100} = 0.6812$  $T_{50} = 2.03 \text{ min.}$ 

> C<sub>V</sub> @ T<sub>50</sub> 3.1 m.<sup>2</sup>/yr.

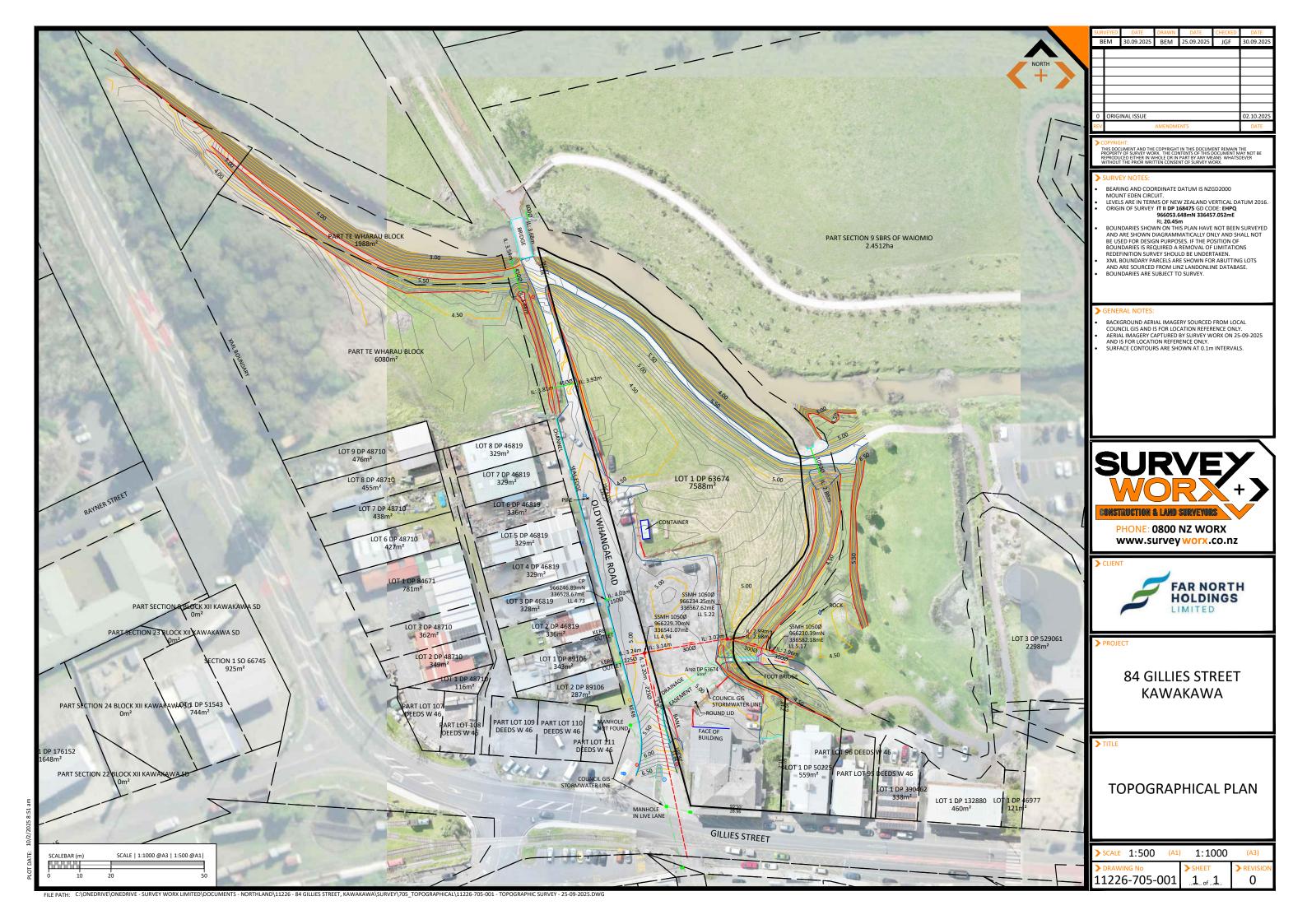
-GeoCivil Ltd. Figure







## **APPENDIX C**





LOCALITY MAP - LARGE SCALE

NTS@A1 HALF-SCALE@A3

DESTINATION	DISTANCE	TIME BY WALK
LOCAL TOWN CENTER	100M-500M	1-10 MIN
CULTURAL CENTER	300M	5 MIN
SPORTS / RECREATION	650M	10 MIN
CHURCH	400M	7 MIN
PRIMARY SCHOOL	450M	8 MIN
HIGH SCHOOL	1.4KM	20 MIN





SITE LOCATION

NTS@A1 HALF-SCALE@A3

























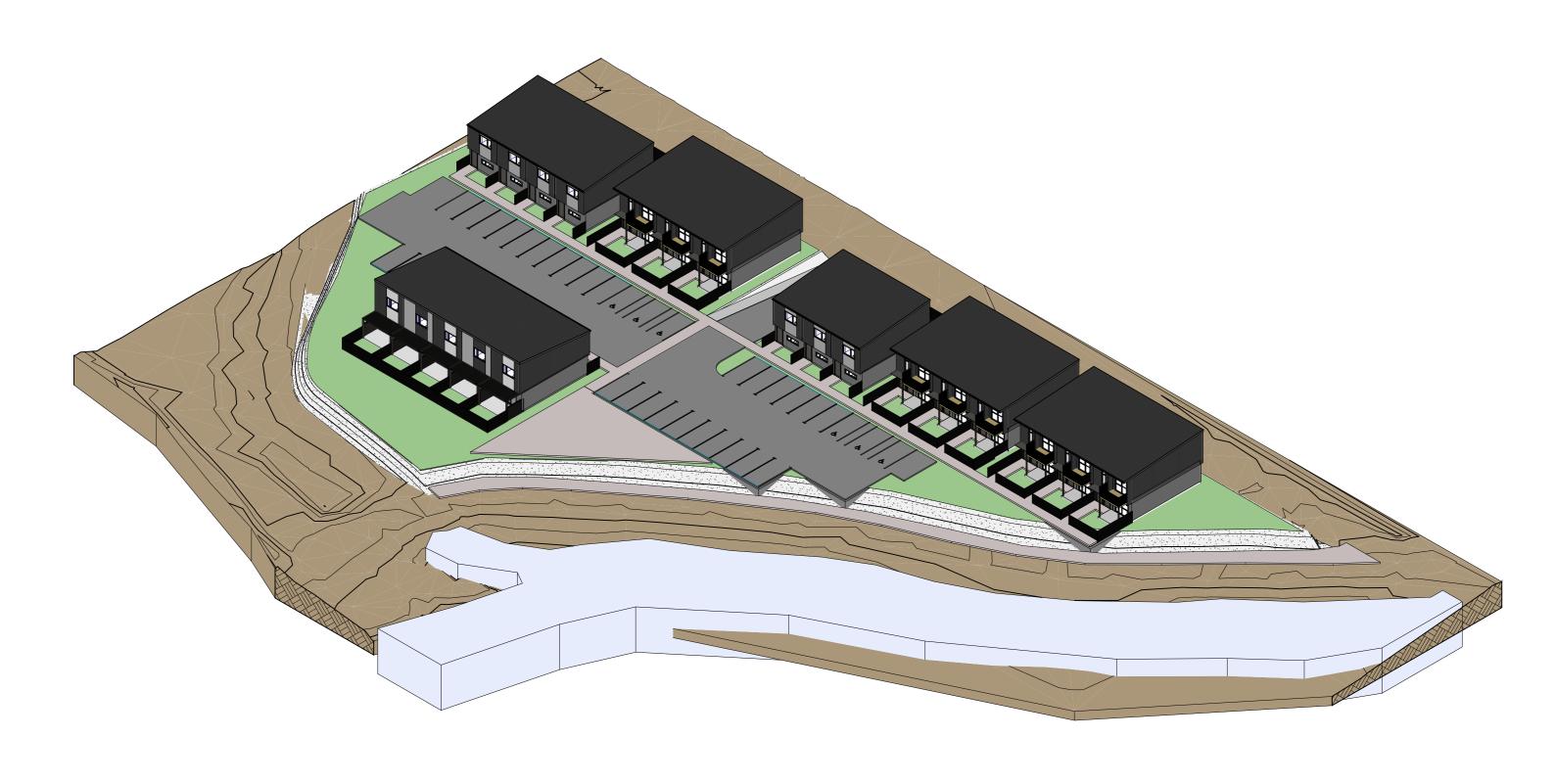
MEDIUM DENSITY HOUSING OLD WHANGAE RD, KAWAKAWA dwg title
VISUALS

RESOURCE CONSENT
scale

AS SHOWN@A1

COURCE CONSENT

AS SHOWN@A1
HALF-SCALE@A3









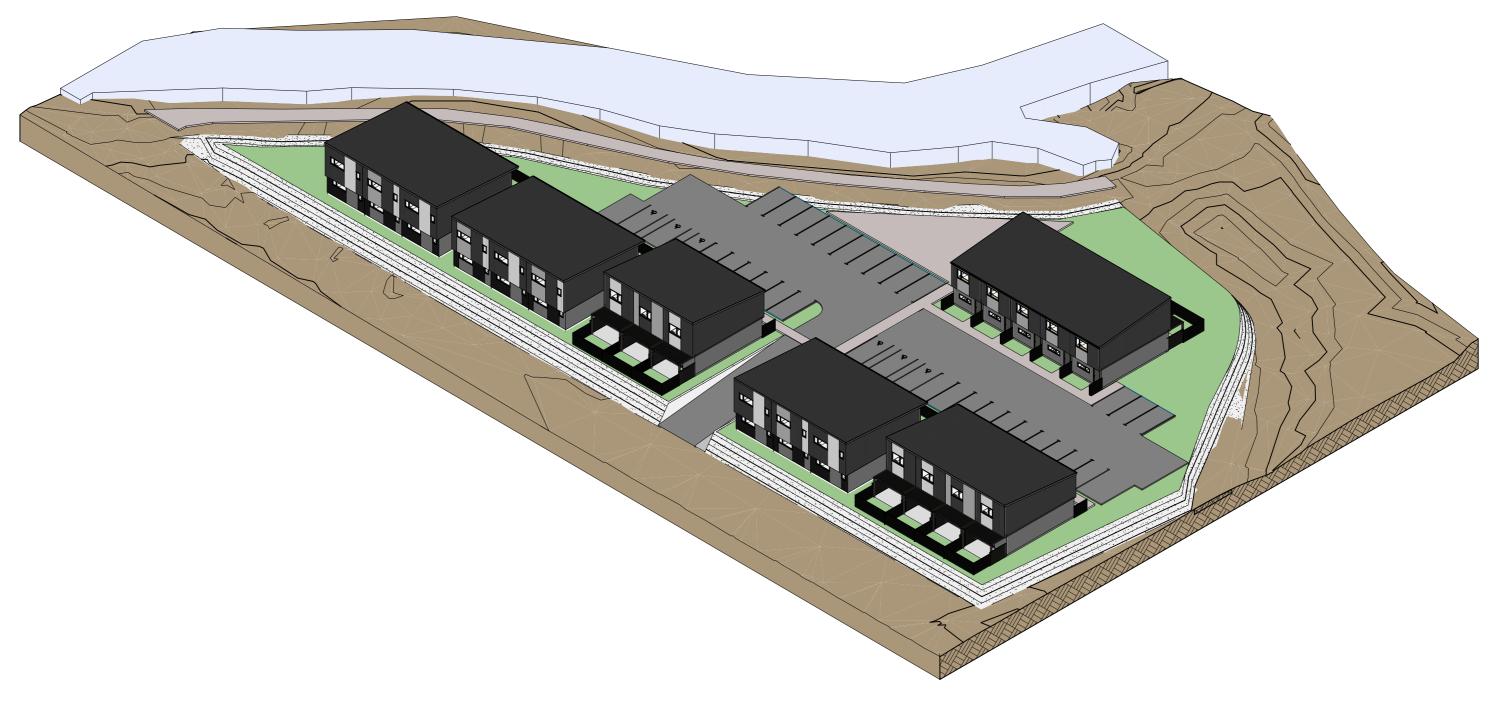










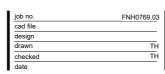












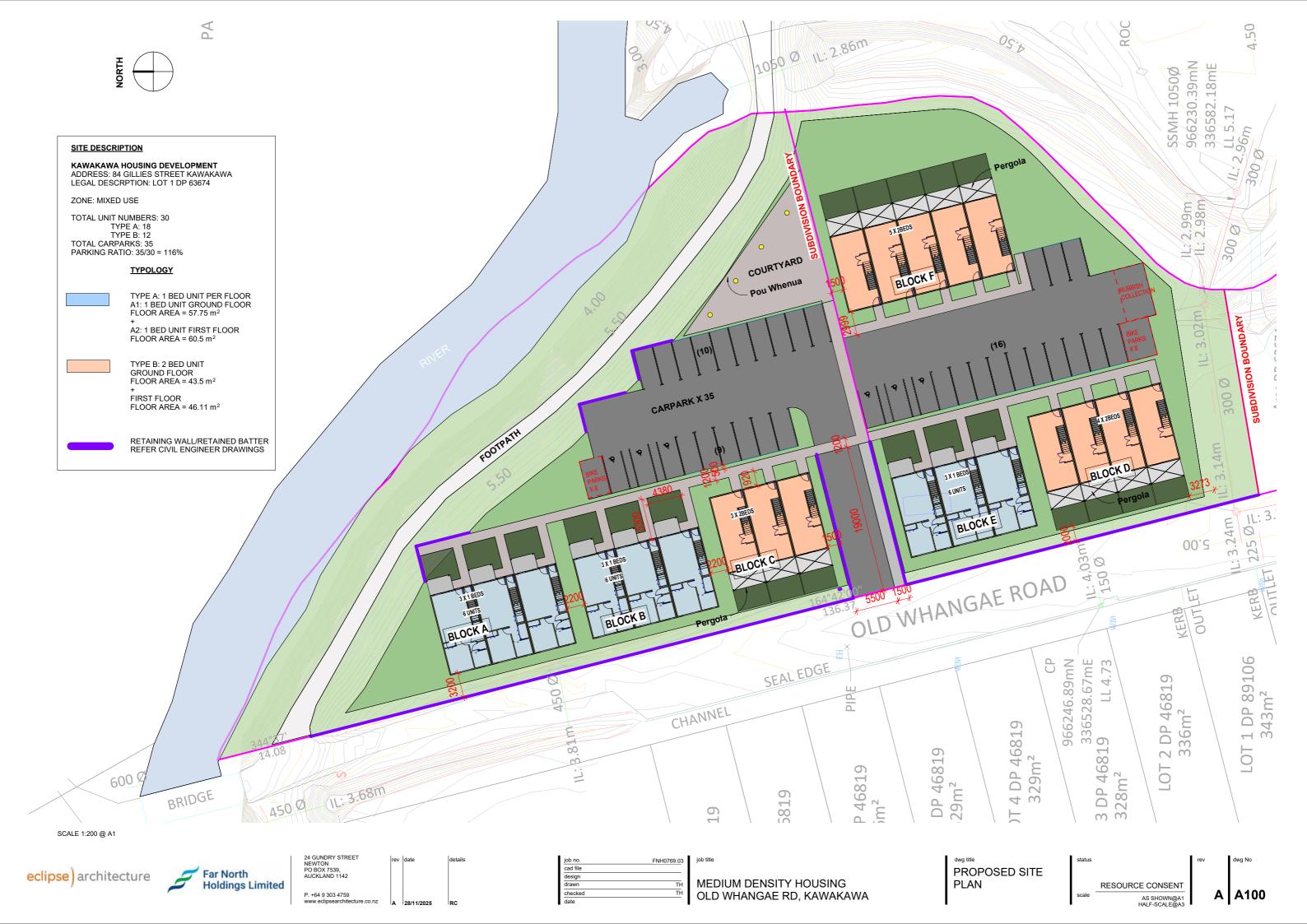
MEDIUM DENSITY HOUSING OLD WHANGAE RD, KAWAKAWA 3D OVERVIEW -MASTER PLAN status

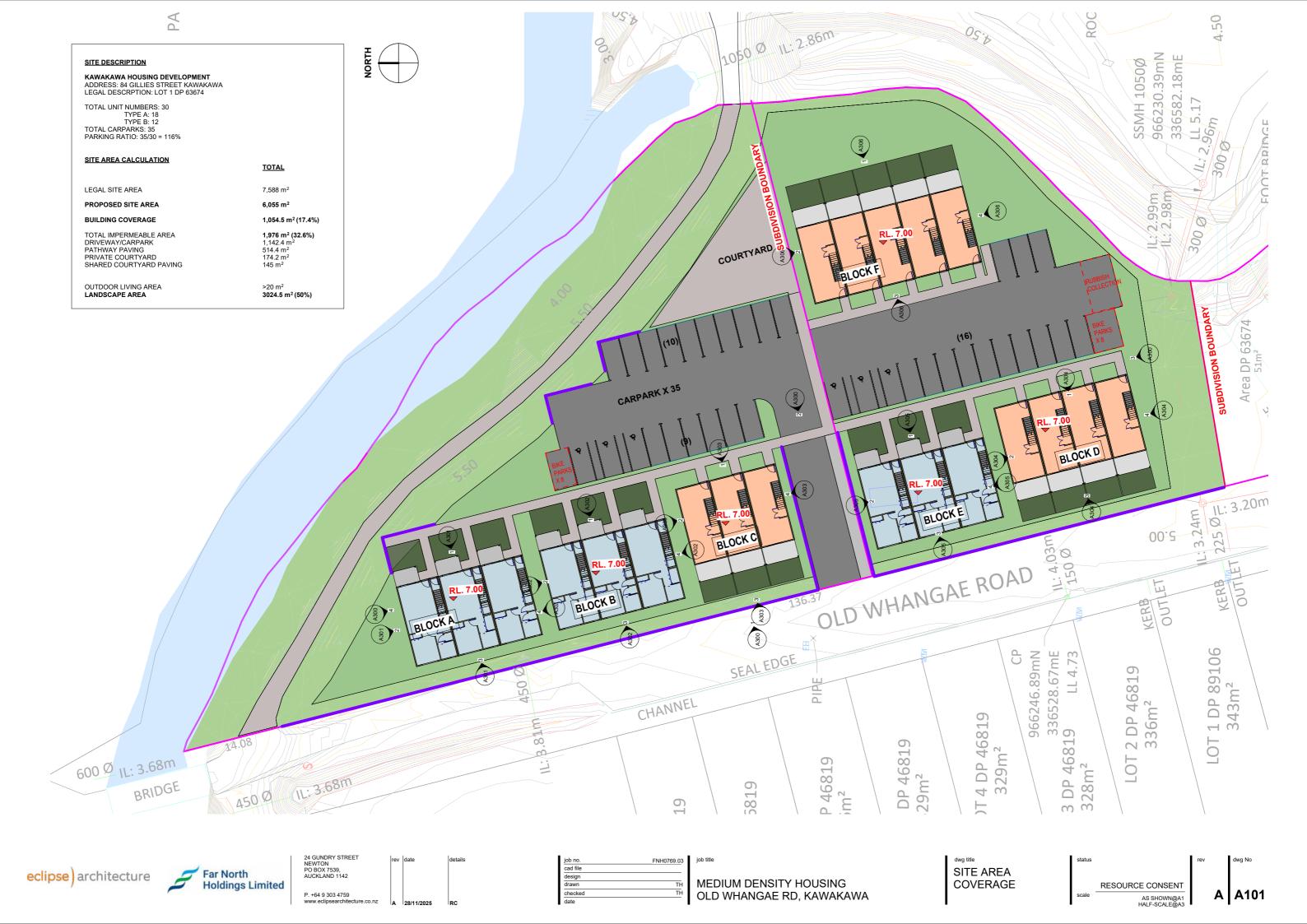
RESOURCE CONSENT

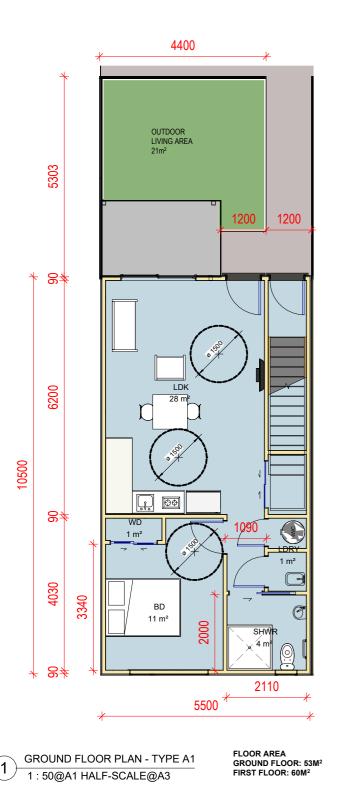
scale

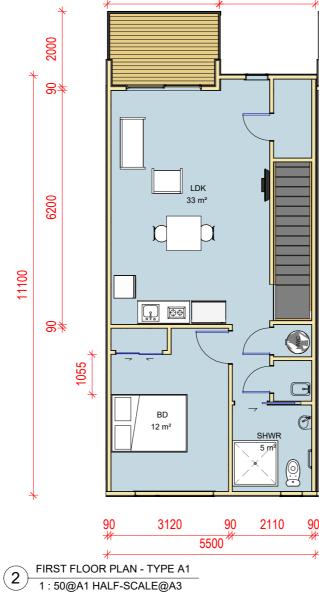
AS SHOWN@A1
HALF-SCALE@A3

A A012

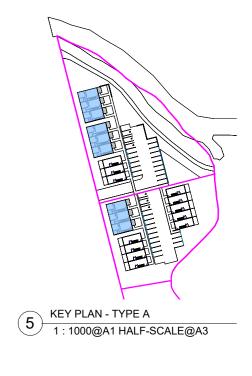








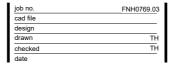




Parking	One carpark is provided per dwelling	YES
raikiliy	One carpaix is provided per dwelling	IES
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES
	Apartment complexes and multi-unit developments: Drop-off zone for customers 'use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	YES
	One path is at least 600mm wide between the dwelling and the clothesline	YE
	Where Timber landings and decks are provided, they are level entry.	YE
	All exterior doors have a clear opening width of at least 810mm.	YE
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YE
	There is step-free access from the main-entry to the main living-area.	YE
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YE
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YE
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YE
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YE
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YE
Fixtures and Fittings	To be compliant during BC Stage	YE
Finishes	To be compliant during BC Stage	YE

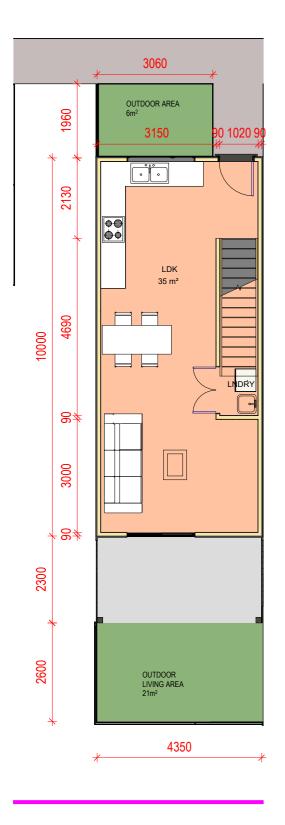


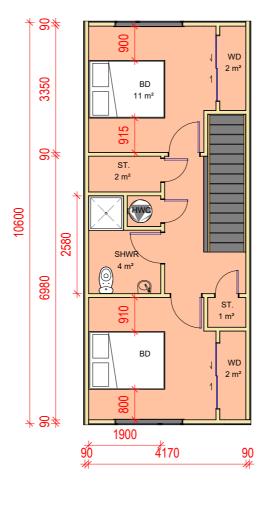












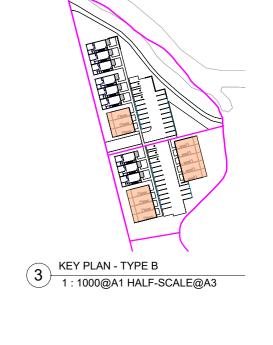
FLOOR AREA GROUND FLOOR:42M<sup>2</sup> FIRST FLOOR: 46M<sup>2</sup> TOTAL: 88M<sup>2</sup>

GROUND FLOOR PLAN - TYPE B

1:50@A1 HALF-SCALE@A3

PIRST FLOOR PLAN - TYPE B

1:50@A1 HALF-SCALE@A3



STANDARD UNIVERSAL DES	SIGN COMPLAINCE	
Parking	One carpark is provided per dwelling	YES
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES
	Apartment complexes and multi-unit developments: Drop-off zone for customers 'use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	
	One path is at least 600mm wide between the dwelling and the clothesline	YES
	Where Timber landings and decks are provided, they are level entry.	YES
	All exterior doors have a clear opening width of at least 810mm.	YES
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YES
	There is step-free access from the main-entry to the main living-area.	YES
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YES
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YES
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YES
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YES
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YES
Fixtures and Fittings	To be compliant during BC Stage	YES
Finishes	To be compliant during BC Stage	YES

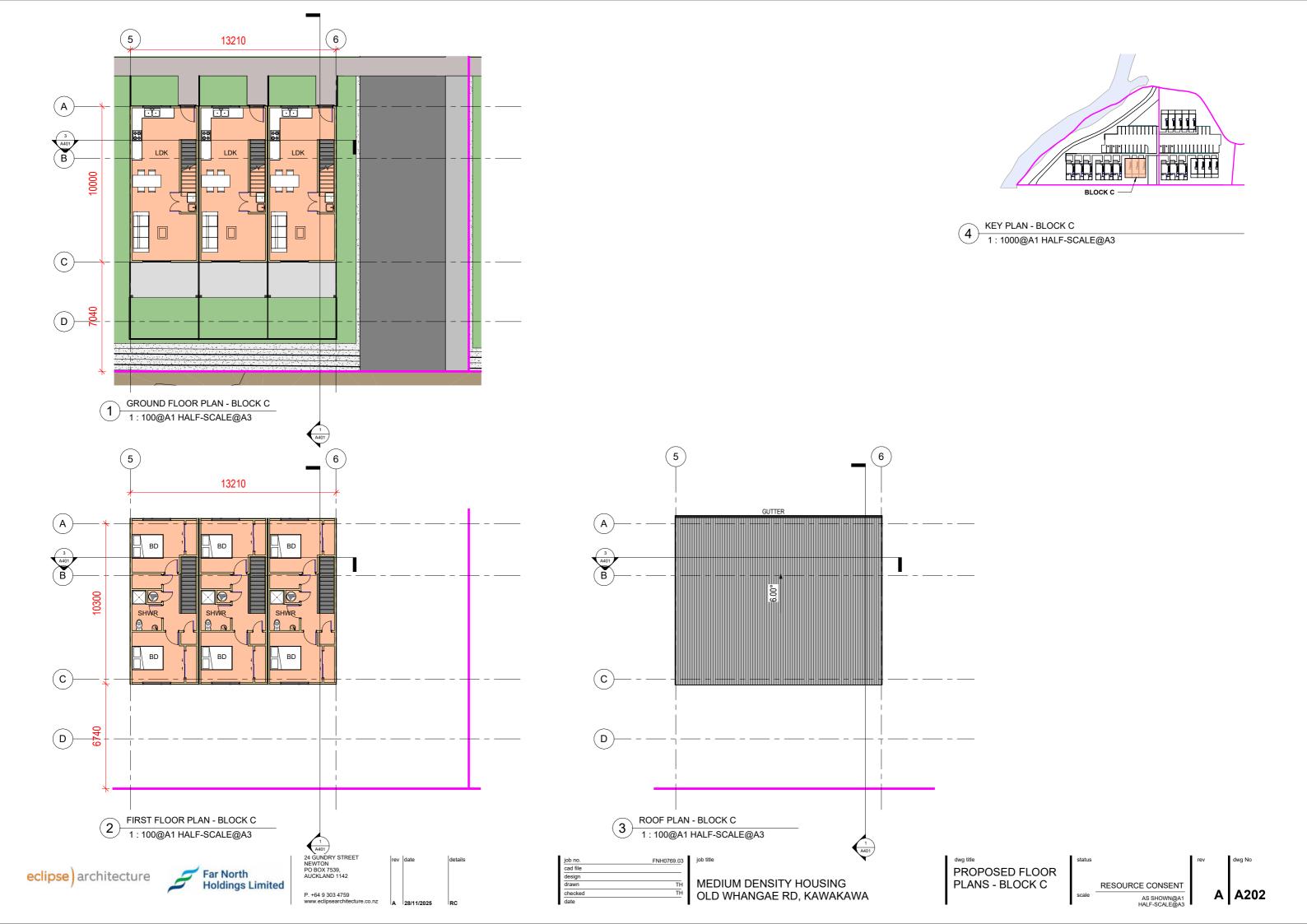


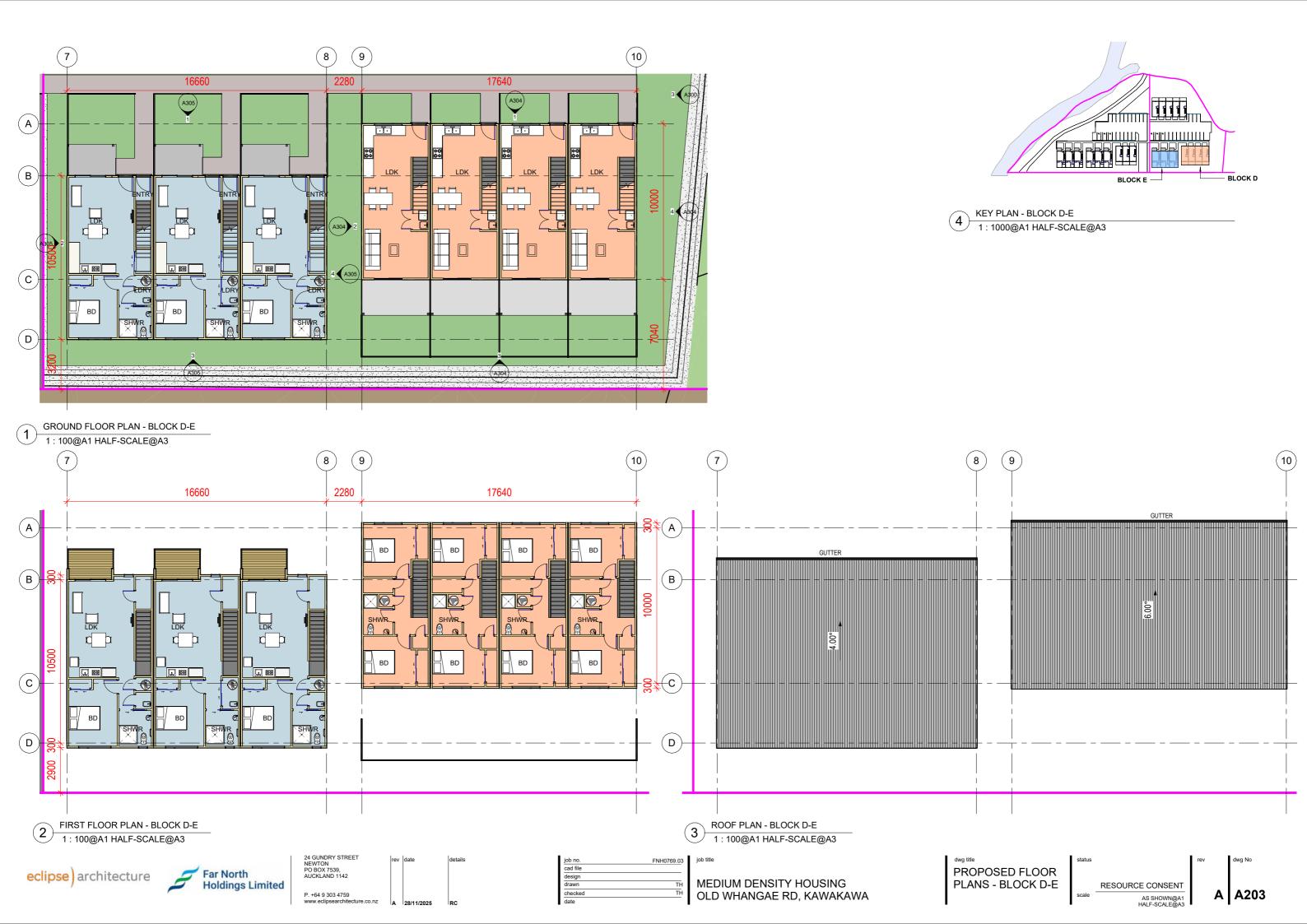


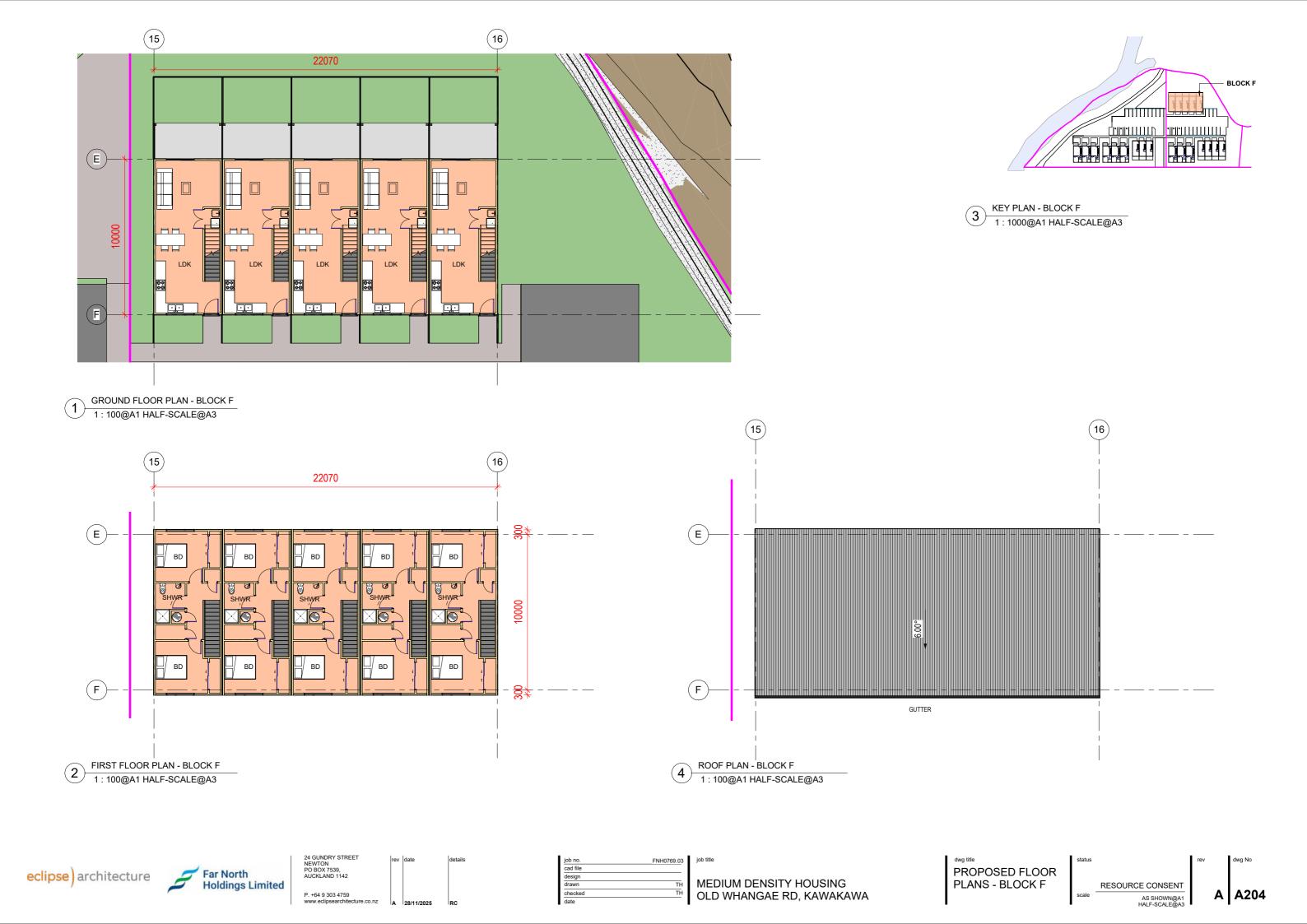


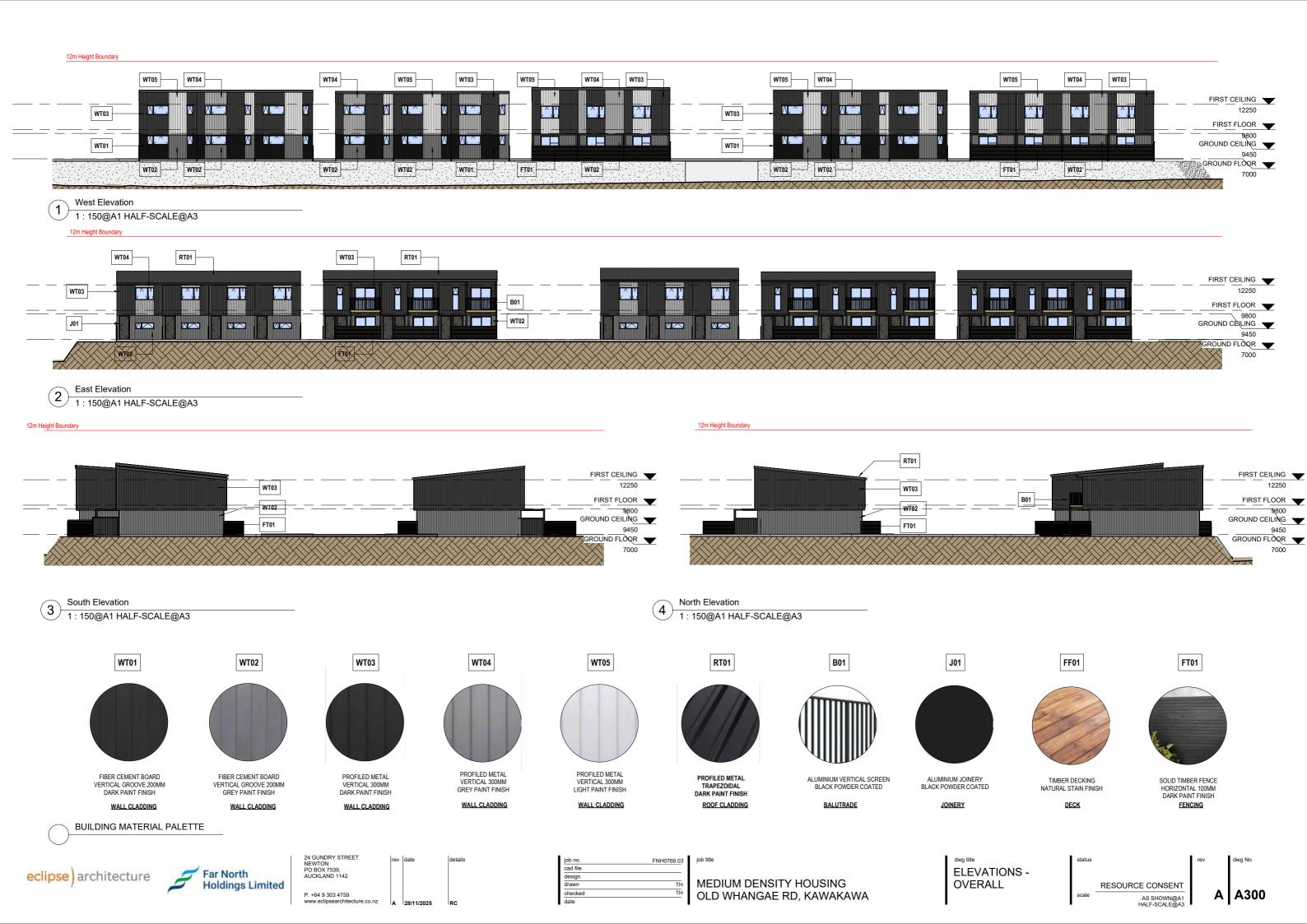


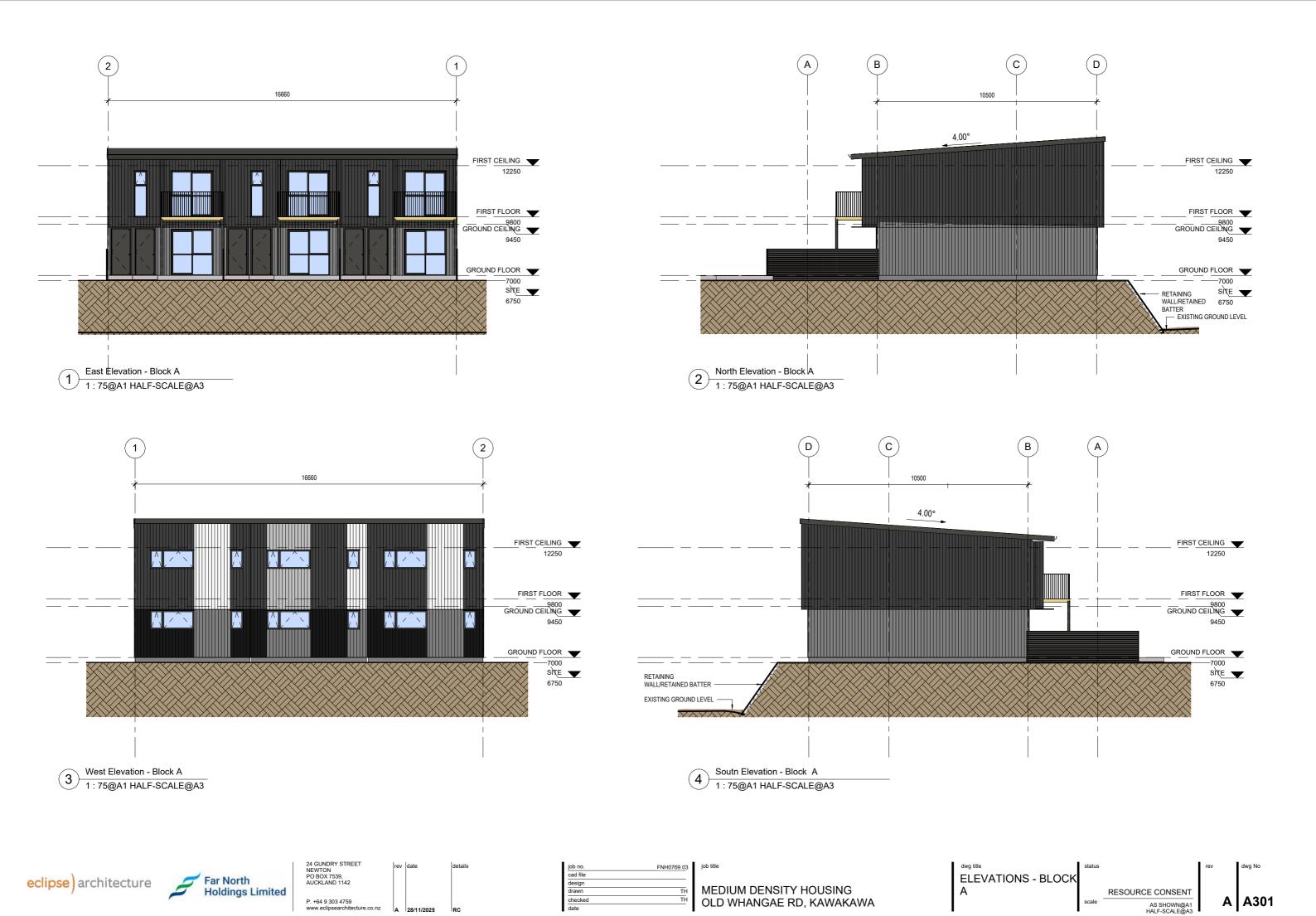


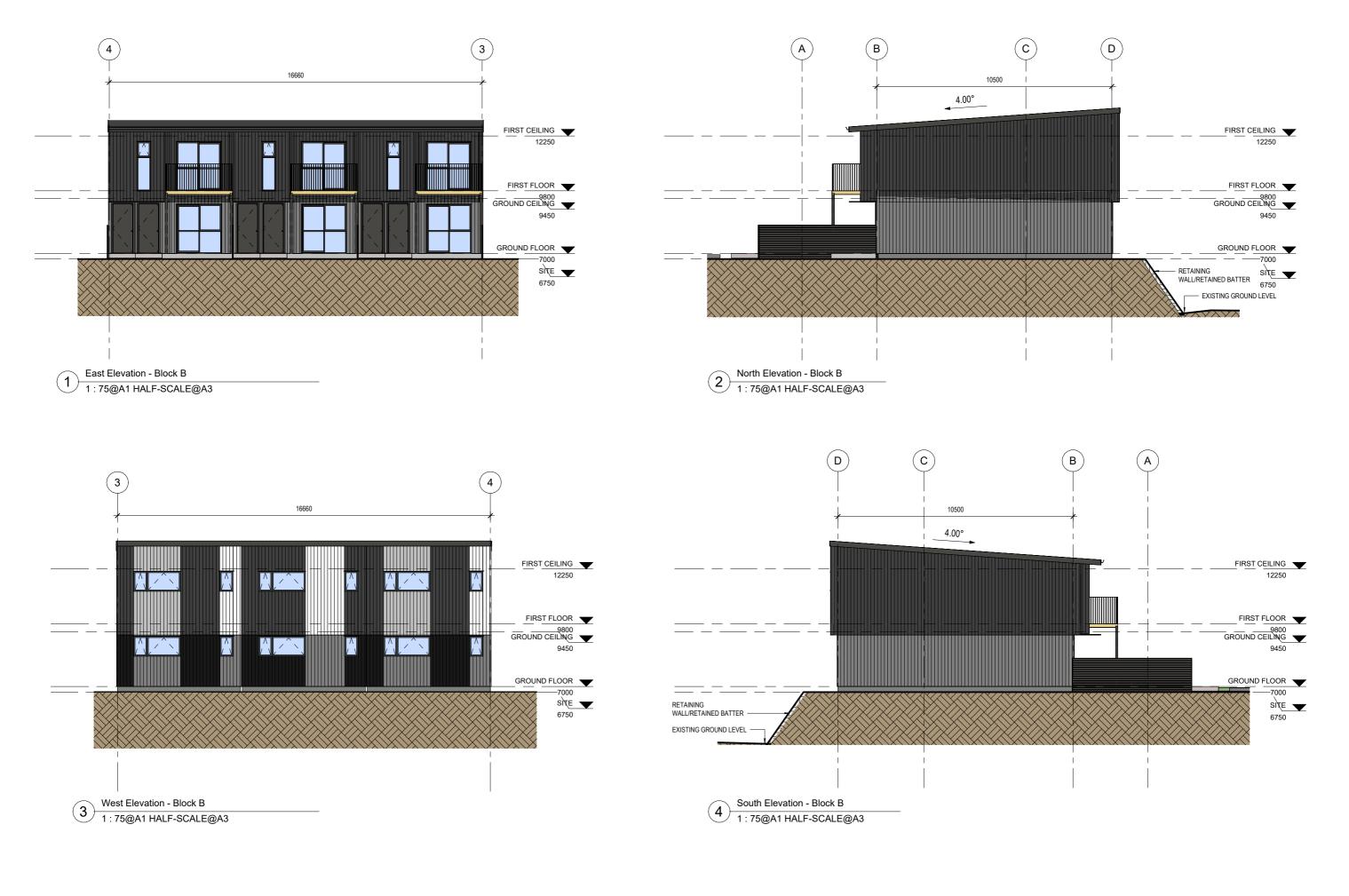










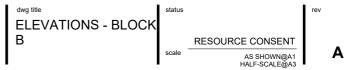


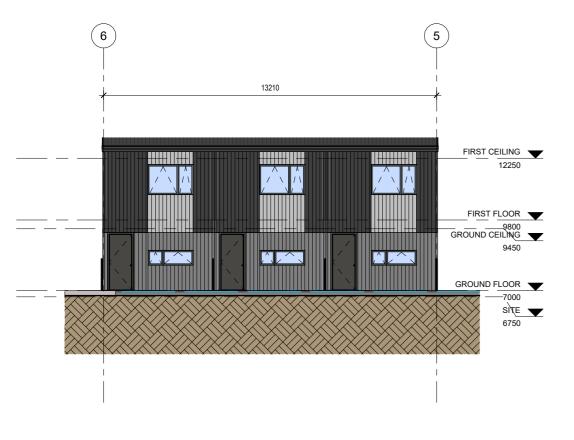




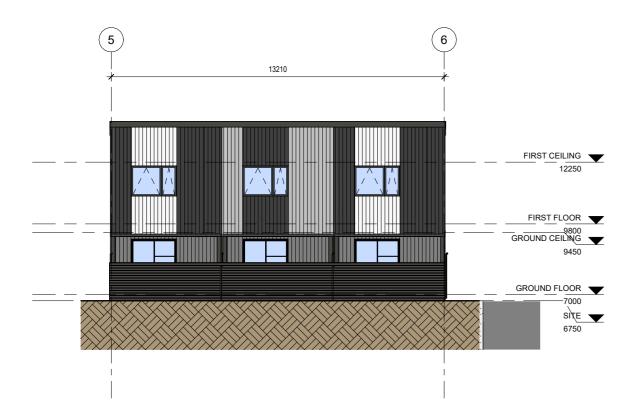








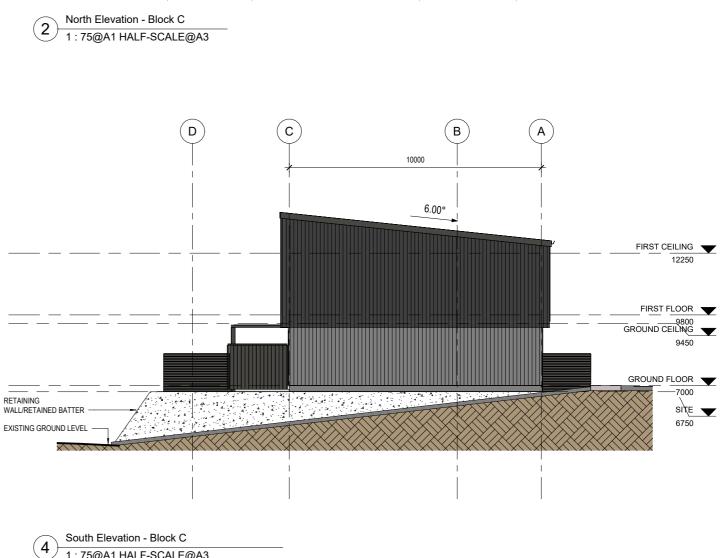
East Elevation - Block C 1 : 75@A1 HALF-SCALE@A3



West Elevation - Block C 3 1 : 75@A1 HALF-SCALE@A3



ELEVATIONS - BLOCK C RESOURCE CONSENT AS SHOWN@A1 HALF-SCALE@A3



(c)

(D)

FIRST CEILING 12250

FIRST FLOOR

GROUND CEILING

GROUND FLOOR

WALL/RETAINED BATTER 6750 - EXISTING GROUND LEVEL

RETAINING

SITE \_

(B)

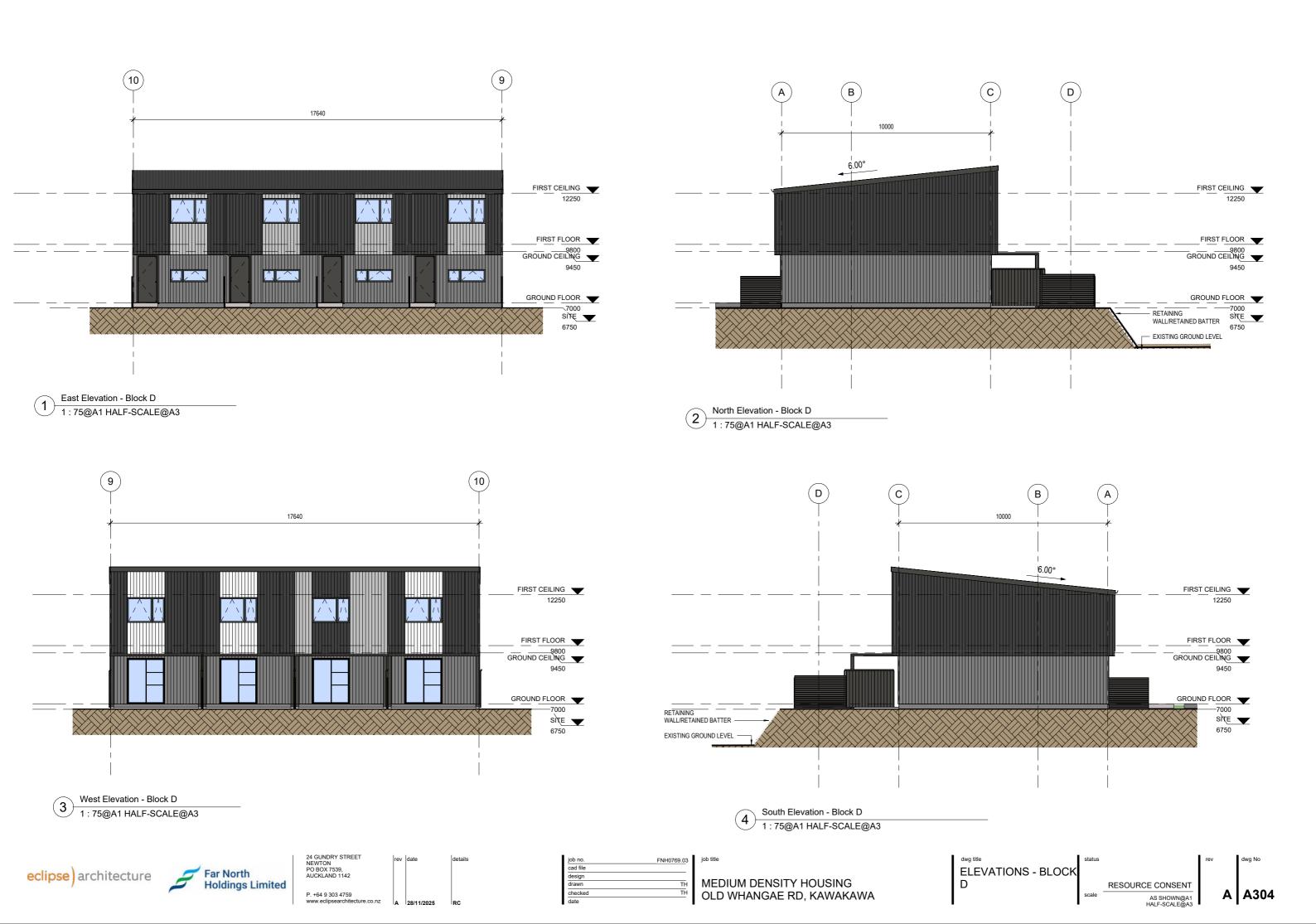
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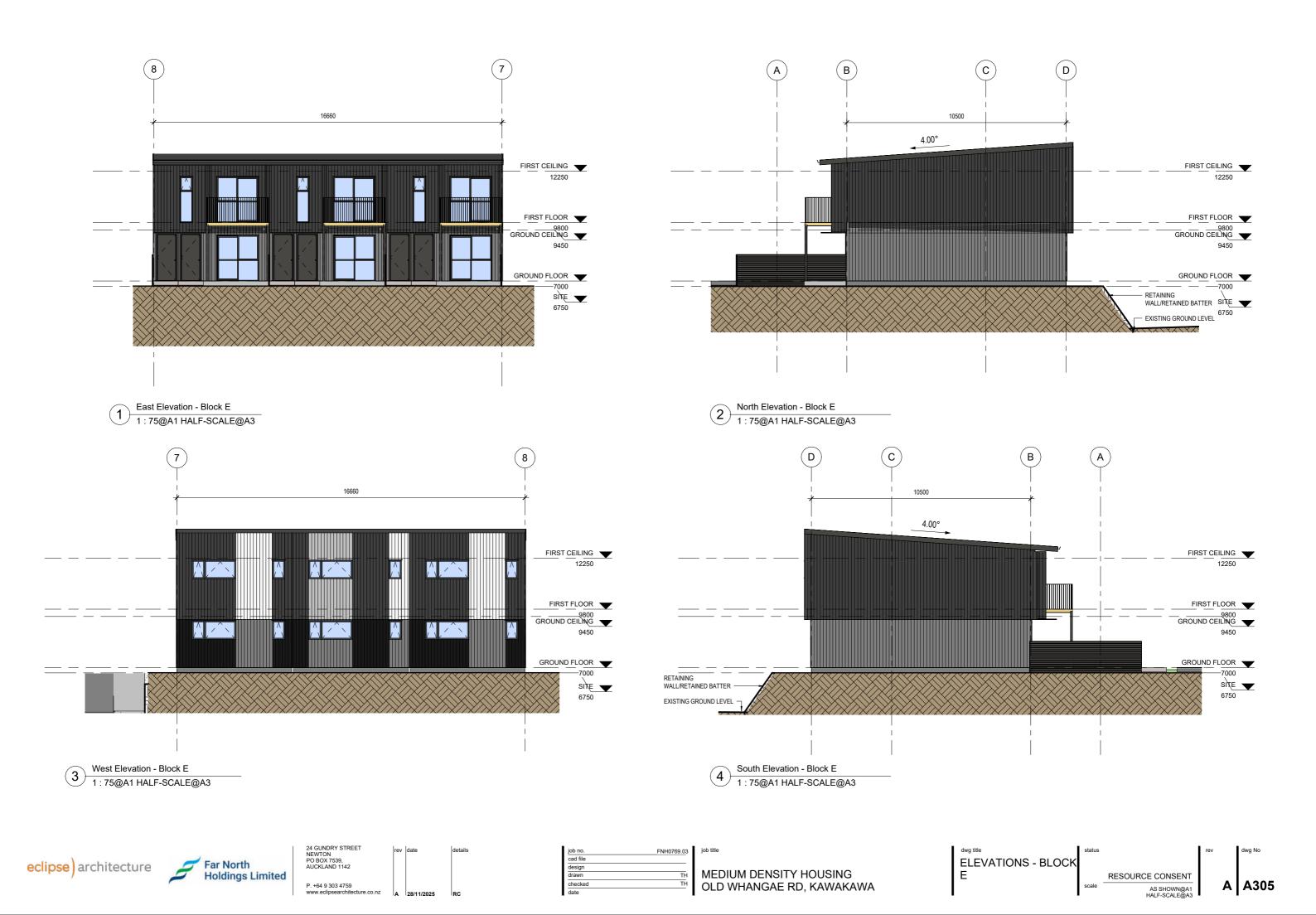
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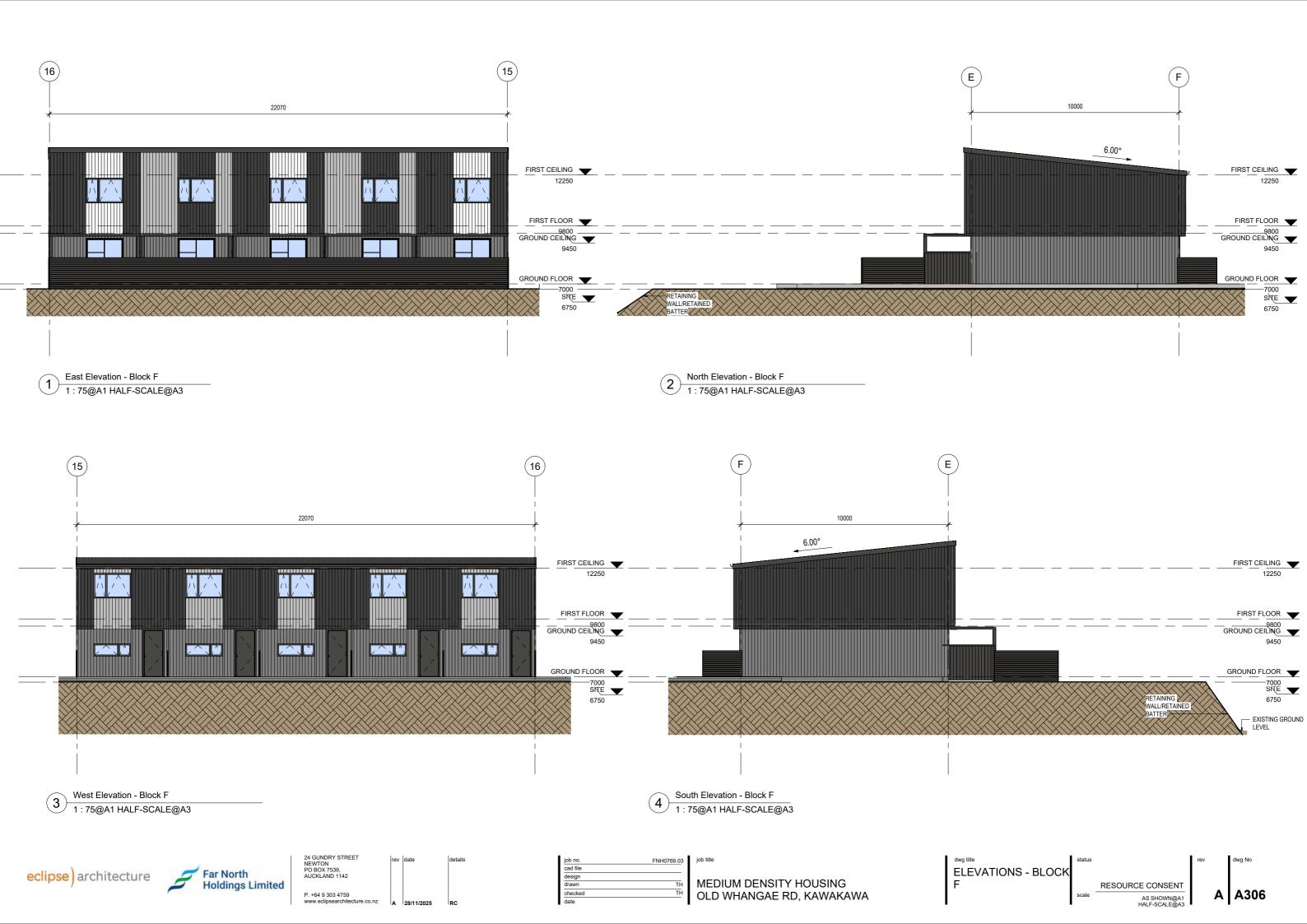


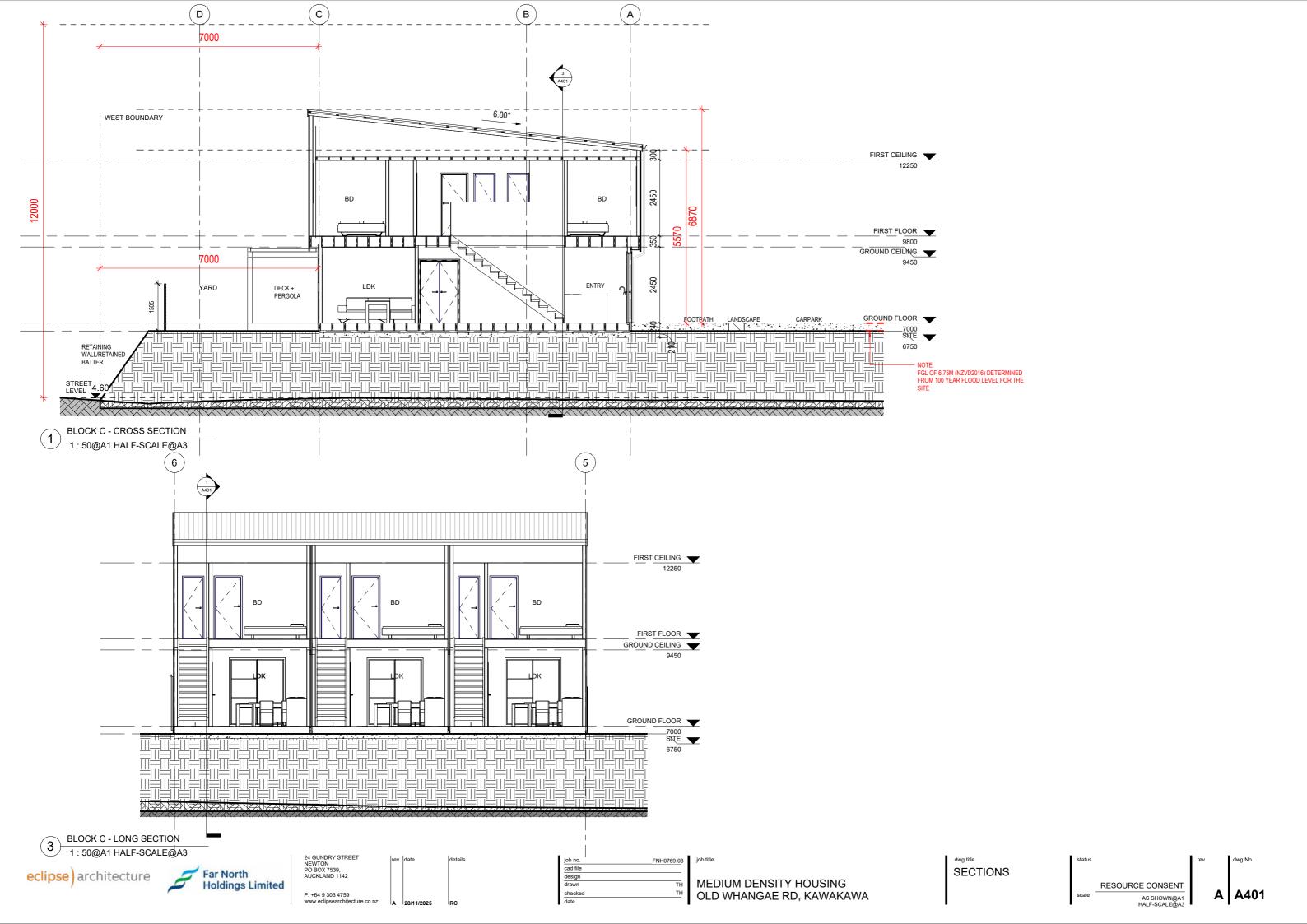


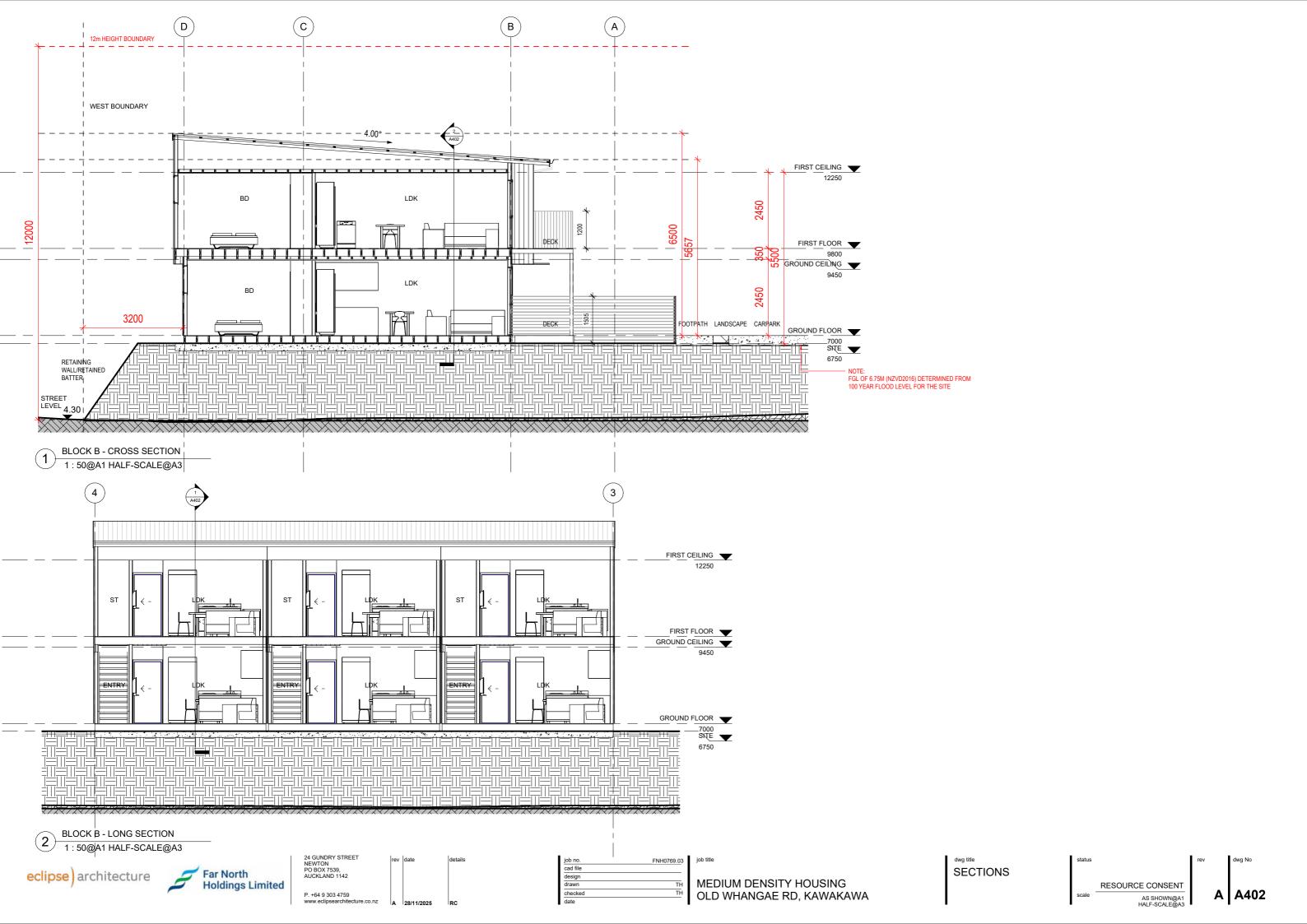
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Far North Housing Limited

# Old Whangae Road Development, Kawakawa Three Waters Report

078-3WR-01\_Rev00



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#### 1. Introduction

This Three Waters Report has been prepared to support the proposed Far North Housing Limited development at Old Whangae Road Development, Kawakawa, shown in Figure 1. The purpose of the report is to assess the servicing requirements for water supply, wastewater, and stormwater, and to confirm that appropriate and compliant infrastructure solutions are available to support the development.

The assessment has been informed by a review of existing public infrastructure, proposed site layout drawings, regional flood information, and the FNDC Engineering Standards (May 2023). Proposed servicing solutions have been developed to ensure that the development can be integrated into the existing networks while meeting performance, resilience, and compliance requirements.

This report must be read in conjunction with the supporting appendices, which form an integral part of the assessment. These include:

- **Appendix A**: Proposed site development layout from Eclipse Architecture (20251128 FNH0769.03 Kawakawa Housing RC).
- **Appendix B**: Resource consent engineering drawings prepared for the Old Whangae Road Development.
- Appendix C: Flood Modelling Maps Outputs
- **Appendix D**: NRC Flood Level Report (Parcel ID 4991387), providing modelled flood information for the site.

Together, the report and its appendices provide a comprehensive overview of the existing and proposed Three Waters servicing arrangements for the proposed development.



Figure 1: Old Whangae Road Development, Kawakawa

### 2. Water Supply

#### 2.1 Existing and Proposed Water Network

The site is currently serviced by two water mains:

- an existing 50 mm diameter MDPE water rider main along the east side of Old Whangae Road, and
- an existing 100 mm diameter MDPE water main along the west side of Old Whangae Road.

As illustrated in **Figure 2**, it is proposed to extend the existing 50mm rider main along the eastern side of Old Whangae Road.

Water supply connections to each development block are proposed as follows:

- **Block A & Block B**: Connected to the new extended 50 mm main on Old Whangae Road (west boundary).
- **Block C, D,E & F**: Connected to the existing 50 mm rider main on Old Whangae Road (west boundary).

This configuration ensures each block has a suitably sized service connection consistent with expected demand and network configuration.

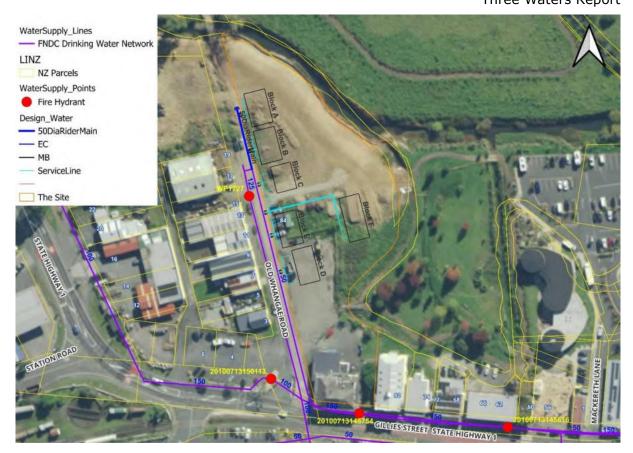


Figure 2: Existing & Proposed Water Supply Network

#### 2.2 Demand Calculation

Water demand has been calculated in accordance with the FNDC Engineering Standards (May 2023, Section 6.2.2).

**Table 1** summarises the adopted design criteria. These criteria form the basis for domestic, peak day, and peak hourly demand calculations for the proposed development.

Domestic water demand for each block, based on the proposed unit types and expected household population, is summarised in **Table 2**. The total demand summary is presented in **Table 3**.

**Table 1: Demand Calculation Criteria** 

Demand Calculation Criteria		
Average Domestic Day Demand	300 L/person/day	
Peak Domestic & Commercial Day Factor	2	
Peak Domestic & Commercial Hourly Factor	5	
Average Hourly Demand on peak day	12.5 L/person/hour	

**Table 2: Estimated Domestic Day Demand** 

	Block A	Block B	Block C	Block D	Block E	Block F
Number of Units	6	6	3	4	6	5
Number of Beds per unit	1	1	2	2	1	2
Population Per Unit	2	2	4	4	2	4
Total Population per Block	12	12	12	16	12	20
Average Day Demand (L/s)	0.04	0.04	0.04	0.06	0.04	0.07
Peak Day Demand (L/s)	0.08	0.08	0.08	0.11	0.08	0.14
Peak Hourly Demand (L/s)	0.21	0.21	0.21	0.28	0.21	0.35

**Table 3: Estimated Total Demand** 

Total Estimated Commercial Day Demand (L/s)			
Average Day Demand (L/s)	0.29		
Peak Day Demand (L/s)	0.58		
Peak Hourly Demand (L/s)	1.46		

## 2.3 Existing Capacity

### 2.3.1 Current Peak Day

Existing network capacity was assessed using the FNDC Kawakawa Hydraulic Water Model (2023). As shown in **Figure 3**, a current peak-day simulation indicates that pressures within the mains supplying the site range from:

Minimum pressure: 73 mMaximum pressure: 88 m

These modelled results include existing demand allocations for the parcels within the development footprint. The existing modelled pre-development demand for the existing Hunter Star Hotel is summarised in **Table 4**.

The available pressure range demonstrates that the existing network is capable of supplying the development under typical peak-day conditions, with ample residual pressure above FNDC's minimum 25m service level requirement.



Figure 3: FNDC Kawakawa Hydraulic Model Peak Day Scenario

Table 4: Existing Modelled Demand

	Hunter Star Hotel Modelled Demand
Parcel ID	Average Demand (I/s)
4991387	0.0341

## 2.3.2 Firefighting

A Fire Hydrant Test was conducted using the FNDC Kawakawa hydraulic model. As shown in **Table 5**, the nearby hydrants are capable of providing:

- FW2 (12.5 L/s) with residual pressures between 42-44 m, and
- Max Fire Flow (18 L/s) with residual pressures at 11 m,

all of which exceed the minimum 10 m residual pressure required in SNZ PAS 4509:2008.

Given that the development's Peak Hourly Demand is only 1.46 L/s, the additional demand loading is negligible relative to the tested FW2/Max firefighting flows. The network therefore has sufficient capacity to meet both domestic peak demands and firefighting requirements.

**Table 5: Fire Flow Analysis** 

Hydrant	Minimu m Fire Flow FW2 (L/s)	Residual Pressure at Minimum Fire Flow (m)	Maximu m Fire Flow FW3 (L/s)	Residual Pressure at Maximum Fire Flow (m)	Pre-Test Pressure (m)
WP1727	12.5	43.87	18.47	11.28	83.24
20100713150113	12.5	42.56	18.37	11.16	81.46
20100713145754	12.5	42.03	18.38	11.17	80.34

## 2.4 Summary

The following conclusions are made with respect to the water supply servicing for the Old Whangae Raod development:

- Blocks A & B will be serviced from the new extended 50 mm main on Old Whangae Road (west boundary).
- Block C, D,E & F will connect to the existing 50 mm rider main on Old Whangae Road (west boundary).

The calculated Peak Hourly Demand of 1.46 L/s is minor relative to the available network capacity. The existing hydraulic model demonstrates a minimum pressure of 73 m under peak-day conditions. A 12.5 L/s firefighting drawdown reduces pressure by approximately 40 m, meaning the significantly smaller development demand will not compromise minimum pressure requirements.

Firefighting performance meets SNZ PAS 4509:2008 requirements up to a FW2 classification, retaining the required 10 m residual pressure. The system does not meet category FW3.

Overall, the existing water supply network has sufficient capacity to service the proposed development.

# 3. Wastewater

#### 3.1 Existing and Proposed Wastewater Network

The site is currently serviced by a 300 mm concrete gravity wastewater main that runs from West to through the southern side of the proposed development.

As shown in **Figure 4**, the development will be reticulated internally by a series of 150 mm PVC gravity wastewater lines that will collect flows from each block and convey them to the receiving public network.

Wastewater connections for each block are proposed as follows:

• Block A to F: Connected to a new private 150 mm network discharging to the existing 300mm concrete gravity main.

This configuration ensures that each block is serviced by an appropriately sized wastewater connection, consistent with expected flow contributions and FNDC reticulation requirements.



Figure 4: Existing and Proposed Wastewater Network

## 3.2 Contributing Flows Calculation

Wastewater flow contributions have been calculated in accordance with the FNDC Engineering Standards (May 2023, Section 5.2.2).

**Table 6** summarises the adopted design criteria, which form the basis for calculating:

- Average Daily Dry Weather Flow (ADWF)
- Peak Dry Weather Flow (PDWF)
- Peak Wet Weather Flow (PWWF)

Residential wastewater contributions from each block are summarised in **Table 7** and the total estimated development flows are summarised in **Table 8**.

**Table 6: Wastewater Flow Contribution Design Criteria** 

Wastewater Flow Contribution Calculation Criteria				
Average Daily Dry Weather Flows (ADWF) for Residential Activities	200 L/person/day			
Peaking Factors to be applied to ADWF Flows for Dry weather peak daily flow (PDWF)	2.5			
Peaking Factors to be applied to ADWF Flows for Peak wet weather flow (PWWF)	5			

**Table 7: Residential Flow Contribution** 

	Block A	Block B	Block C	Block D	Block E	Block F
Number of Units	6	6	3	4	6	5
Number of Beds per unit	1	1	2	2	1	2
Population Per Unit	2	2	4	4	2	4
Total Population per Block	12	12	12	16	12	20
ADWF (L/s)	0.03	0.03	0.03	0.04	0.03	0.05
PDWF (L/s)	0.06	0.06	0.06	0.07	0.06	0.09
PWWF (L/s)	0.14	0.14	0.14	0.19	0.14	0.23

**Table 8: Estimated Total Flow Contribution** 

Estimated Total Flow Contribution (L/s)			
ADWF (L/s)	0.19444		
PDWF (L/s)	0.38889		
PWWF (L/s)	0.97222		

## 3.3 Existing Capacity

As part of the Local Water Done Well programme, a previous wastewater network capacity assessment was undertaken using the hydraulic performance criteria requested by Far North District Council (FNDC). The following hydraulic capacity criteria were applied to determine the pass/fail results:

• FNDC ES FNDC ES - May 2023 Final, Clause 5.1.3. Performance Standards, d) Ensure that the proposed system does not surcharge at the peak design wet weather flow and is designed not to overflow.

**Figure 5** (site outlined in blue) presents the traffic-light assessment of the wastewater reticulation network. The results indicate that there are no immediate capacity constraints at the proposed development's discharge point. However, capacity limitations do exist further downstream within the trunk network conveying flows toward the wastewater treatment plant.

FNDC is currently progressing a programme of wastewater network and treatment upgrades in Kawakawa through the Infrastructure Acceleration Fund (IAF) administered by Kāinga Ora. These works are intended to increase conveyance capacity, reduce wetweather overflows, and improve overall system resilience to accommodate future township

growth. The upgrade package includes improvements to key reticulation routes, additional network storage, and enhancements to the treatment process.

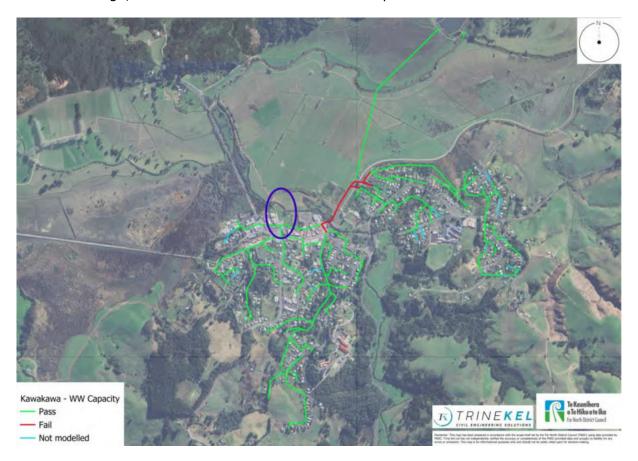


Figure 5: Local Water Done Well Capacity Assessments

#### 3.4 Summary

The proposed development will connect to the existing 300 mm concrete gravity wastewater main located along the southern boundary of the site, with internal reticulation provided by new 150 mm PVC gravity lines servicing each block.

Wastewater flows have been calculated in accordance with FNDC Engineering Standards (May 2023), using standard ADWF, PDWF, and PWWF design criteria. The resulting total Peak Wet Weather Flow for the development is estimated at 0.97 L/s, confirming relatively low contributing flows.

A review of the Local Water Done Well wastewater capacity assessment indicates that while the development's discharge point has no immediate capacity constraints, sections of the downstream trunk network do exhibit existing limitations under peak wet-weather conditions. FNDC is addressing these constraints through planned upgrades funded via the Kāinga Ora Infrastructure Acceleration Fund, including reticulation improvements, increased storage, and treatment plant enhancements. These works are expected to improve conveyance capacity, reduce overflows, and support future growth in Kawakawa.

# 4. Stormwater

## 4.1 Existing and Proposed Stormwater Network

The site is currently serviced by an unlined channel to the east, with only minor existing stormwater infrastructure located within Old Whangae Road. As shown in **Figure 6**, a new 525 mm diameter pipe is proposed to replicate pre-development overflow behaviour from the unlined channel. This is described in further detail in **Section 4.2: Flood Modelling**.

Stormwater reticulation for each block is proposed as follows:

• Blocks A to F will be serviced via a new private stormwater network discharging to the northern side of the existing diversion bank.

Stormwater neutrality (attenuation) is not required for this development because the site is located at the lower end of the catchment, and all stormwater discharges north of the diversion bank. Potential changes to overland flow paths resulting from raising site levels have been assessed, with only minor effects observed between pre- and post-development scenarios.

This design ensures that stormwater runoff is managed in a manner consistent with existing discharge pathways, without generating adverse effects on the upstream or downstream public systems or properties.



Figure 6: Existing and Proposed Stormwater Network

## 4.2 Flood Modelling

Trine Kel Limited have been engaged by Far North Housing Limited to undertake comprehensive 2D flood modelling to assess the post-development impacts of the proposed medium-density housing project at Old Whangae Road, Kawakawa (Lot 1 DP 63674). The objective of the modelling is to compare existing flood conditions with those under the proposed development and to assess any potential changes in flood behaviour.

The modelling was based on the Northland Regional Council's Regionwide Kawakawa Catchment TUFLOW Model (M15). The regional model does not explicitly include detailed local stormwater infrastructure. For application to the proposed development site, the model was refined using updated topographical data, surveyed culverts, and key stormwater assets, providing a more representative basis for comparing existing and proposed scenarios. Refer to **Figure 7**, which provides an overview of the model extent and key features.

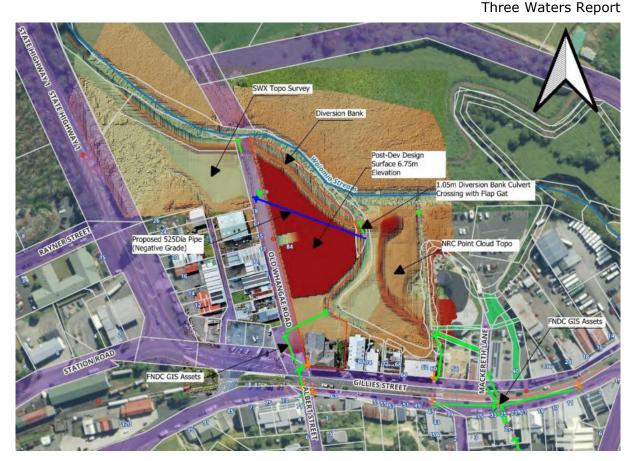


Figure 7: New Proposed Old Whangae Road, Kawakawa (Lot 1 DP 63674) FNHL Development, Flood Model

#### 4.2.1 Model Development

#### 4.2.1.1 Methodology

The modelling involved the following key steps:

- 1. Base Model Review: Set up the NRC M15 base model, ran initial simulations, and compared outputs against NRC results to confirm suitability as the foundation.
- 2. Data Collection:
  - Relevant FNDC stormwater infrastructure (FNDC online GIS data).
  - Survey Worx Topographical Survey.
  - NRC Topographical Point Cloud containing the deflection bank.
  - Proposed Post Development Surface from FNHL/Hoskin Civil.
- 3. Build the pre-development (existing) 1% AEP + CC model run (Model 2):
  - Base Model: NRC M15 with 1.25 m quadtree refinement in the development area.
  - Rainfall: 1% AEP 24-hour storm event, RCP 8.5 scenario, for the 2081–2100.
  - Existing Infrastructure: 3 x Culverts crossing the deflection bank + 1 Culvert Crossing Old Whangae Road + Relevant FNDC Stormwater Network.
  - DEM: NRC M15 Model DEM + NRC Point Cloud (Deflection Bank) + SWX Topo Survey (Pre-Development Site).
- 4. Built the proposed post-development 1% AEP + CC model run (Model 5):

Old Whangae Road Development, Kawakawa – Far North Housing Limited

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- Base Model: NRC M01 with 1.25 m quadtree refinement in the Springs Flat area.
- Rainfall: 1% AEP 12-hour storm event, RCP 8.5 scenario, for the 2081–2100.
- Existing Infrastructure: 3 x Culverts crossing the deflection bank + 1 Culvert Crossing Old Whangae Road + Relevant FNDC Stormwater Network + **Proposed 525mm Dia negative grade stormwater pipe**.
- DEM: NRC M15 Model DEM + NRC Point Cloud (Deflection Bank) + SWX Topo Survey (Pre-Development Site) + Proposed Post Development Design Surface at elevation 6.75m (NZVD 2016).
- 5. Produce final model runs on the existing and proposed model scenarios.
- 6. Produce afflux (flood depth difference) maps between pre-development and post development scenarios.

#### 4.2.1.2 Calibration & Validation

The NRC M15 Regionwide TuFlow model was previously calibrated against the January 2011 flood event using two river gauges: Waiharakeke River at Willowbank and Tirohanga River below Old Mill. This calibration was retained as part of the proposed medium-density housing project at Old Whangae Road, Kawakawa refinement to ensure consistency with the NRC model. No additional calibration was carried out, as the model builds directly on NRC's validated model and retains its calibration parameters.

#### 4.2.1.3 Model Outputs

**Table 9** shows the deliverables that were generated refer to **Appendix C**:

Table 9: Flood Modelling Maps Output Register (Appendix C)

Flood Depth Mapping: Maximum depth for existing and proposed cases.	Difference Mapping: Raster outputs highlighting increases/decreases in flood depth between the existing (pre-development) and post-development scenarios.
• <b>078-SWC-100_00</b> : Pre-Development (Existing) Ground + Deflection bank Flood Depth - Model 2 (100yr + CC)	• <b>078-SWC-103_01</b> : Pre & Post Maximum Flood Depth Differences (100yr + CC)
• <b>078-SWC-102_01</b> : Post-Development Ground + Deflection bank Flood Depth - Model 4 (100yr + CC)	• <b>078-SWC-104_01</b> : Pre & Post Flood Depth Differences (100yr+CC 16hr time interval)

#### 4.2.1.4 Model Results Summary

At the maximum flood depth of the 1% AEP (24-hour) storm event under the RCP 8.5 (2081–2100) climate change scenario, the model results indicate less than 5 mm difference in flood depth between the pre- and post-development scenarios. Refer to the pre and post-development maximum depth-difference map in **Appendix C: 078-SWC-103**.

This minimal variation occurs because floodwaters back up from the north-west of the site, creating a ponded (dam-like) condition across the wider floodplain. Under these conditions, the flood extent pushes southward, fully submerging the pre-development ground surface and forming an inundated basin around the elevated post-development platform. The post-

development platform remains above the peak flood level but produces similar maximum flood extents to the pre-development scenario.

However, before this full ponding condition is established, when surface runoff is still moving toward the north-western flood area, more noticeable differences in overland flow paths and shallow inundation occur between the two scenarios, particularly around 16 hours into the 30-hour model run. These localised variations result from changes to surface grading in the post-development layout.

In the pre-development scenario (**Figure 8**), the unlined eastern channel becomes inundated and is hydraulically governed by the 1.05 m diameter culvert with a flap gate through the diversion bank. When downstream water levels equal or exceed upstream levels, the flap gate closes, preventing outflow and causing the eastern channel to back up and overflow at its north-western end.

In the post-development scenario (**Figure 9**), where a 525 mm diameter negative-grade pipe is proposed, the same hydraulic control occurs; however, once backing-up begins, overflow from the channel is conveyed through the new pipe beneath the site and discharged to a scruffy dome west of Old Whangae Road. Refer to the pre and post-developments 16hr-interval depth-difference map in **Appendix C: 078-SWC-104**.

Overall, the post-development scenario has a negligible effect at peak flood depth during the 1% AEP event, as both surfaces are fully inundated within the same floodplain. Smaller, more frequent storm events are expected to exhibit more noticeable differences; however, these are appropriately managed through the inclusion of the proposed 525 mm negative-grade stormwater pipe.



Figure 8: Pre-Development Scenario Flood Depth @ 16hr into the Storm Duration

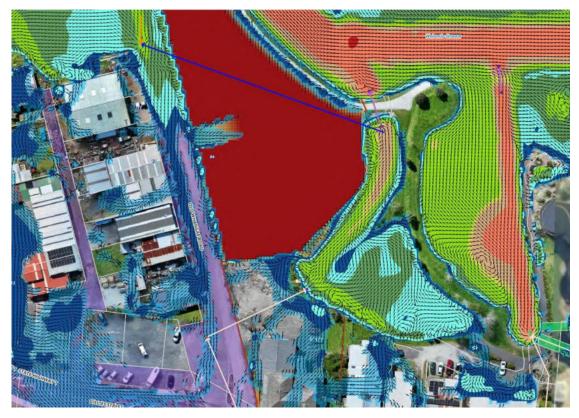


Figure 9: Figure 3: Post-Development Scenario Flood Depth @ 16hr into the Storm Duration

#### 4.2.1.5 Limitations and Assumptions

The model is based on survey, infrastructure, and hydrological data supplied by NRC, FNDC, NIWA, and FNHL. The reliability of the outputs depends on the accuracy and completeness of this information.

Flood modelling involves simplifying assumptions. Small changes in rainfall intensity, culvert blockages, or future land use could influence the results.

Results should be interpreted in the context of the information available at the time of modelling and may require revision if new or updated data becomes available.

This assessment is intended for comparative flood impact purposes and should not be used for detailed design of drainage structures without further validation.

#### 4.3 Flood Hazard

Flood hazards at the site were assessed using the NRC Priority River Model with the available regional flood information presented in Appendix D.

Finished floor levels and site design contours have been set to ensure that ground and building levels are raised at least 500 mm above the NRC priority model 1% AEP + CC flood level, in accordance with standard flood resilience requirements

## 4.4 Summary

The proposed development manages stormwater using a combination of new private reticulation and a 525 mm diameter pipe designed to replicate existing overflow behaviour from the eastern unlined channel. As the site is located at the lower end of the catchment and discharges north of the diversion bank, no attenuation is required, and only minor changes to overland flow paths are expected.

A refined 2D TUFLOW flood model was developed using the NRC Kawakawa Catchment Model (M15), incorporating updated topography, surveyed culverts, key FNDC stormwater assets, and the proposed development design. Model simulations for the 1% AEP (24-hour) RCP 8.5 (2081–2100) storm event indicate less than 5 mm difference in maximum flood depths between existing and proposed scenarios. This is due to a basin-like ponding condition that develops from the north-west, which inundates the pre-development ground surface and forms an island around the elevated post-development platform, resulting in comparable peak flood extents.

Localised changes in shallow flow and inundation occur before the full ponding condition is established, particularly around 16 hours into the storm event, these effects are mitigated through the inclusion of the proposed 525 mm negative-grade stormwater pipe conveying overflow beneath the site.

Overall, the modelling demonstrates that the development has a negligible effect on peak flood levels during the critical design storm, with no adverse impacts on upstream or downstream flood behaviour. Flood hazard requirements are met by setting finished floor

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levels and site contours at least 500 mm above the NRC Priority River Model 1% AEP + climate change flood level.

## 5. Recommendations

## **5.1 Water Supply**

- 1. **Hydrant pressure testing**: Undertake on-site hydrant flow and pressure tests to confirm the hydraulic model outputs and validate available firefighting performance.
- 2. **Flow meter data acquisition**: Request recent flow meter records from FNDC for the surrounding network to validate base demand assumptions and confirm model calibration.
- 3. **Detailed design modelling**: Incorporate the calculated development demands into the FNDC hydraulic model during detailed design and run updated scenarios to confirm operational and firefighting performance.

#### 5.2 Wastewater

- Confirm downstream capacity with FNDC: Engage with FNDC during the detailed design phase to obtain updated network modelling or capacity assessments confirming that the downstream system can accommodate the proposed development flows.
- 2. **Detailed design modelling**: Incorporate the calculated development flow contribution into the updated FNDC hydraulic model during detailed design and run updated scenarios to confirm operational performance.

#### **5.3 Stormwater**

- 1. **Detailed design modelling**: Refine the stormwater model during the detailed design phase, including updated design surfaces, final pipe alignments, and site levels, to confirm post-development flood behaviour and runoff pathways.
- 2. **Critical storm assessment**: Simulate a range of smaller and more frequent storm events to identify the critical storm for local overland flow and to validate the performance of the proposed stormwater network.
- 3. **Infrastructure sensitivity testing**: Assess the sensitivity of key stormwater structures (including culverts and the proposed 525 mm pipe) to partial or full blockage scenarios to understand their potential influence on upstream water levels.
- Incorporation of existing structures: Include relevant existing building footprints in the final model to ensure that overland flow paths and surface runoff behaviour are accurately represented.

# 6. Appendices

# 6.1 Appendix A:

Proposed site development layout from Eclipse Architecture (20251128 FNH0769.03 Kawakawa Housing RC).



LOCALITY MAP - LARGE SCALE
NTS@A1 HALF-SCALE@A3

DESTINATION	DISTANCE	TIME BY WALK
LOCAL TOWN CENTER	100M-500M	1-10 MIN
CULTURAL CENTER	300M	5 MIN
SPORTS / RECREATION	650M	10 MIN
CHURCH	400M	7 MIN
PRIMARY SCHOOL	450M	8 MIN
HIGH SCHOOL	1.4KM	20 MIN





SITE LOCATION

NTS@A1 HALF-SCALE@A3

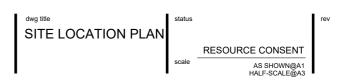










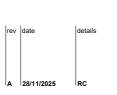












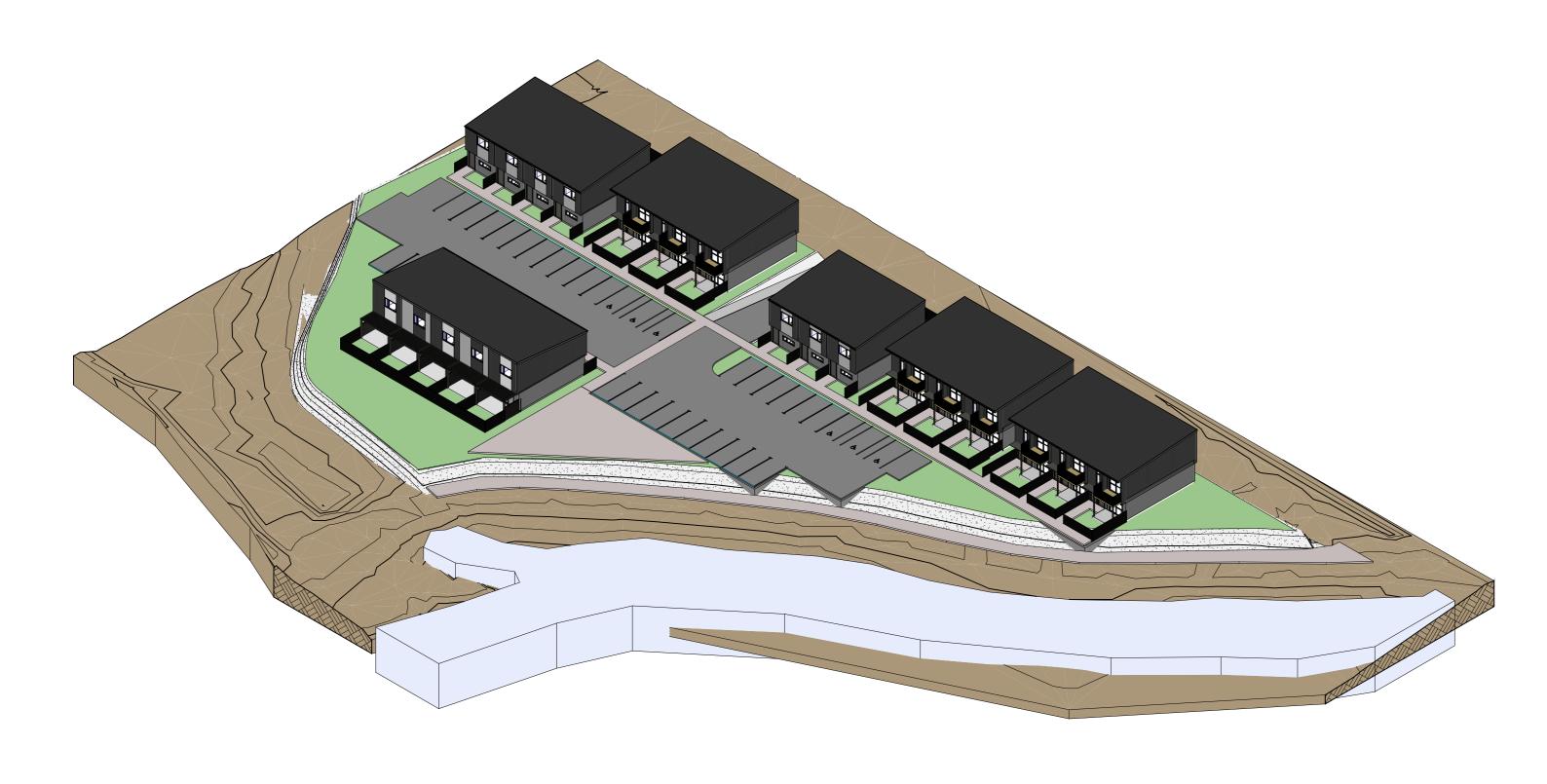


MEDIUM DENSITY HOUSING OLD WHANGAE RD, KAWAKAWA dwg title
VISUALS

RESOURCE CONSENT
scale

AS SHOWN@A1
HALF-SCALE@A3

A A002









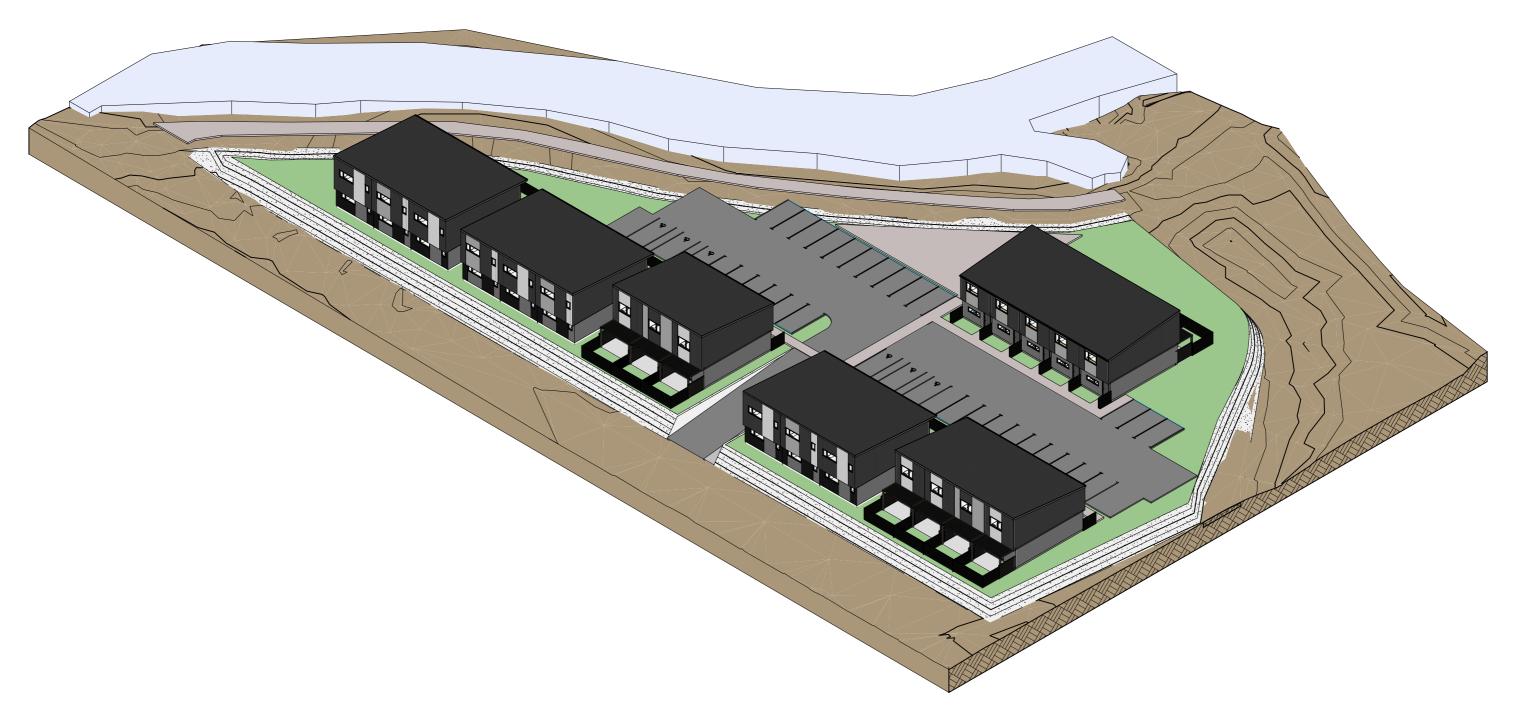






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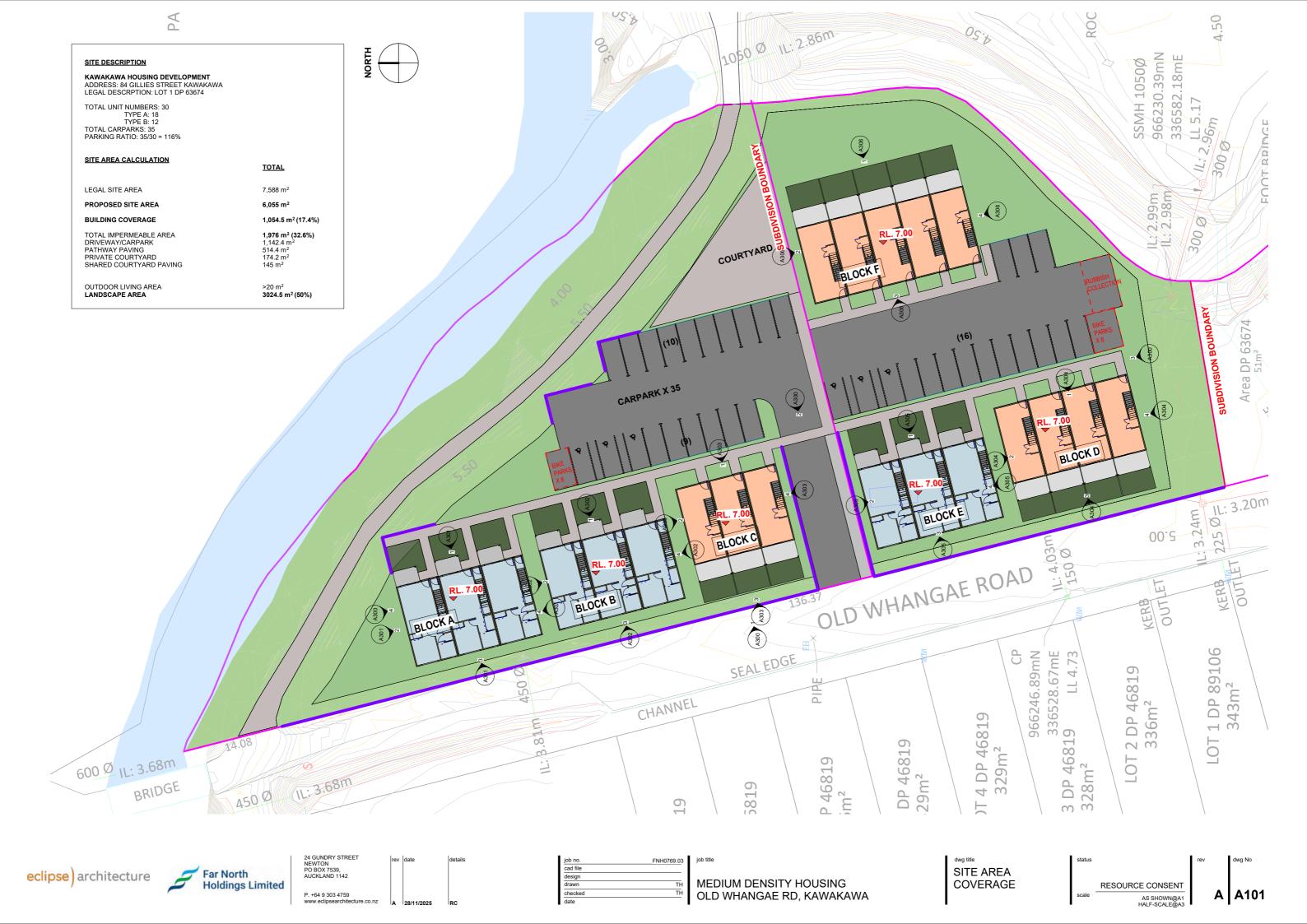


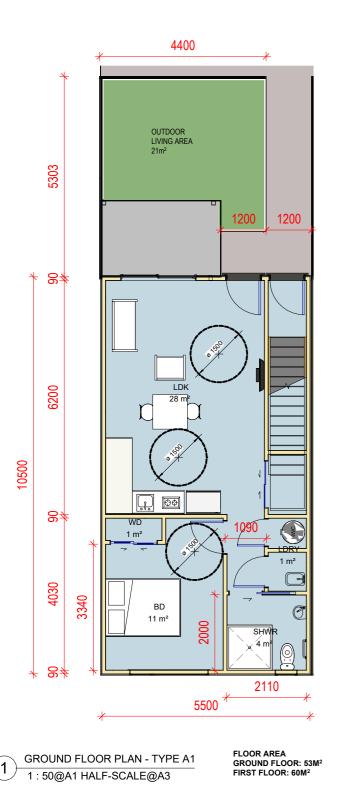
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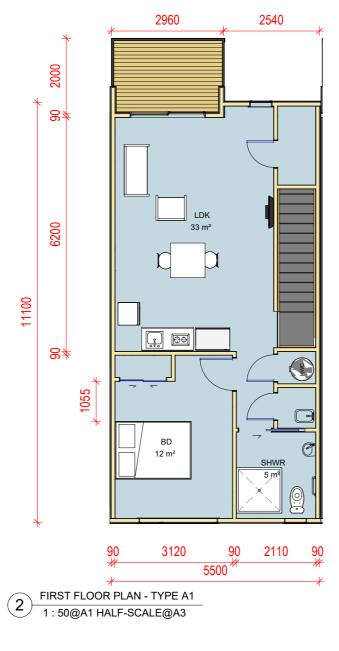


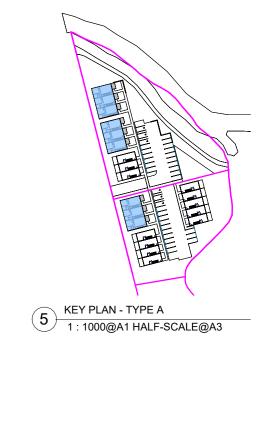








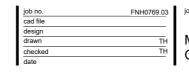




STANDARD UNIVERSAL DESIGN COMPLAINCE				
Parking	One carpark is provided per dwelling	YES		
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES		
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES		
	Apartment complexes and multi-unit developments: Drop-off zone for customers ' use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	YES		
	One path is at least 600mm wide between the dwelling and the clothesline	YES		
	Where Timber landings and decks are provided, they are level entry.	YES		
	All exterior doors have a clear opening width of at least 810mm.	YES		
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YES		
	There is step-free access from the main-entry to the main living-area.	YES		
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YES		
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YES		
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YES		
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YES		
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YES		
Fixtures and Fittings	To be compliant during BC Stage	YES		
Finishes	To be compliant during BC Stage	YES		

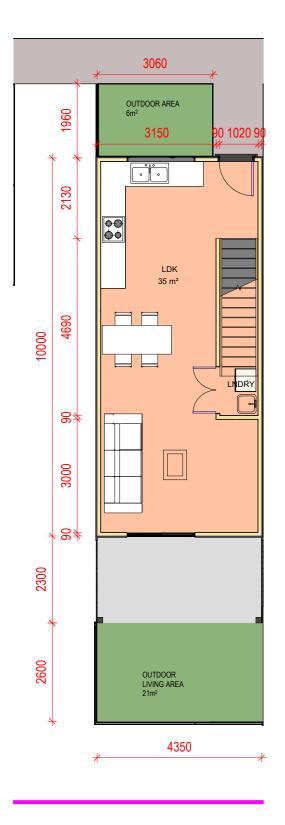


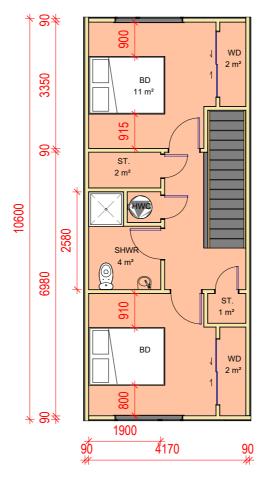












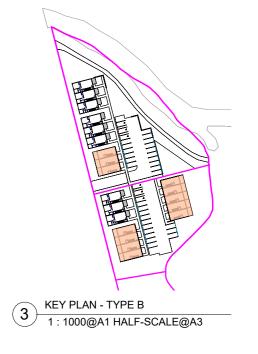
FLOOR AREA GROUND FLOOR:42M<sup>2</sup> FIRST FLOOR: 46M<sup>2</sup> TOTAL: 88M<sup>2</sup>

GROUND FLOOR PLAN - TYPE B

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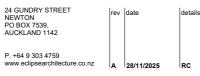
PIRST FLOOR PLAN - TYPE B

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STANDARD UNIVERSAL DES	SIGN COMPLAINCE	
Parking	One carpark is provided per dwelling	YES
Exterior Circulation	There is a 1.2 x 1.2m sheltered landing at the main entry.	YES
	The main entry pathway is at least 1m wide from the street and/or parking area.	YES
	Apartment complexes and multi-unit developments: Drop-off zone for customers 'use, (crossfall between 1:100 and 1:50) with direct access into building(s), supported by public transport within close proximityproximity.	YES
	One path is at least 600mm wide between the dwelling and the clothesline	YES
	Where Timber landings and decks are provided, they are level entry.	YES
	All exterior doors have a clear opening width of at least 810mm.	YES
Interior Circulation	Circulation routes on the main living level are at least 1.05m-wide (between framing) and include at least 800mm clearance between items of furniture and fixtures.	YES
	There is step-free access from the main-entry to the main living-area.	YES
	All ground floor interior doors (other than to cupboards and storage) have a clear opening width of at least 810mm.	YES
	Any internal stairs have: a maximum rise of 190mm; a minimum tread of 280mm; and include a handrail on at least one side, and do not use stair winders.	YES
Kitchens	Studio – 3 bedrooms: 1.2m clearance in front of kitchen benches and appliances	YES
Bathroom	All bathrooms on the main living level are at least 2120mm x 1920mm (measured between framing) with clearances of at 800mm between fixtures. Do not install a wet area-shower. No floor rebate required. Door swing inwards.	YES
Laundry	There is 1050mm clearance in front of all laundry fittings and appliances	YES
Fixtures and Fittings	To be compliant during BC Stage	YES
Finishes	To be compliant during BC Stage	YES

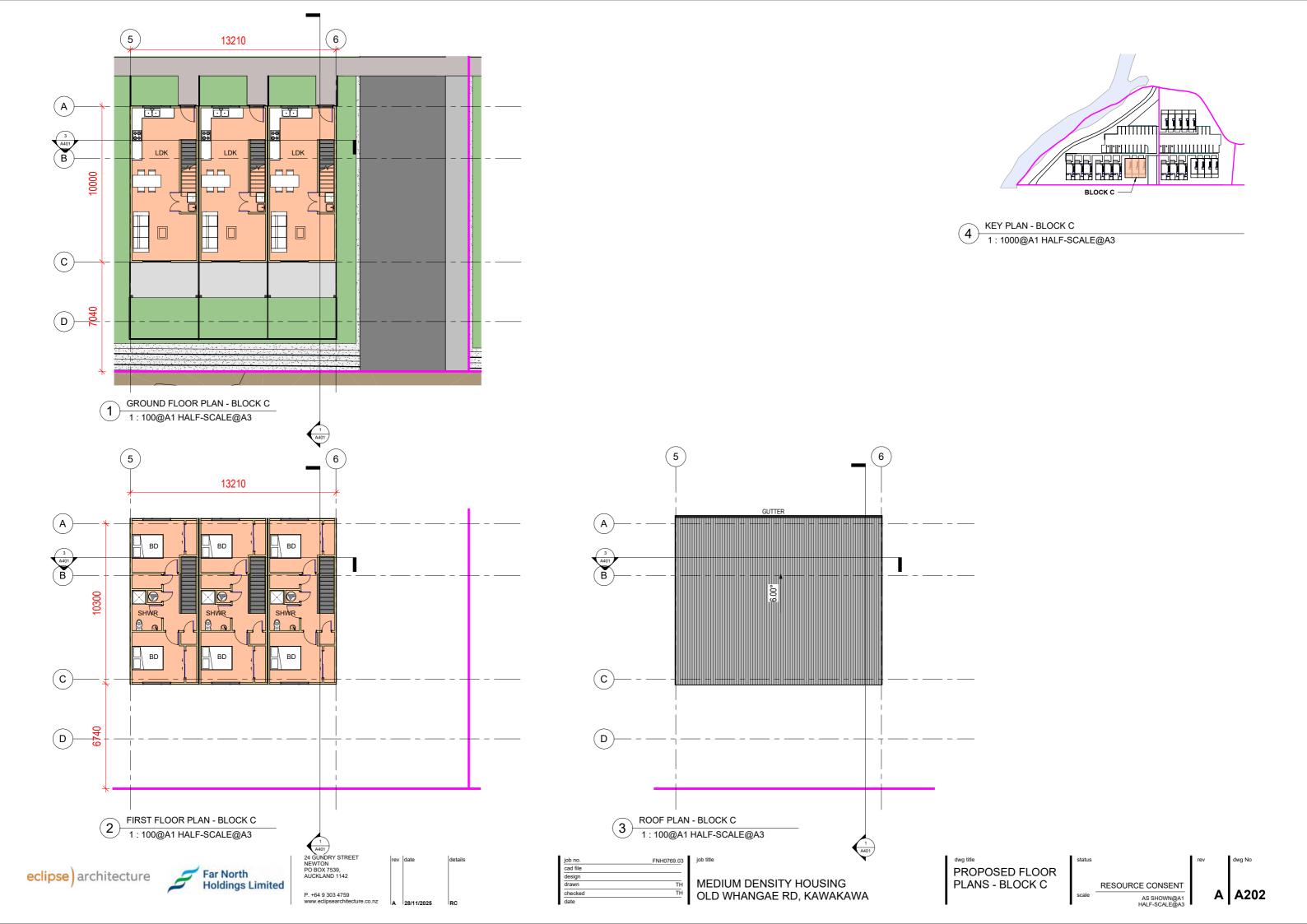


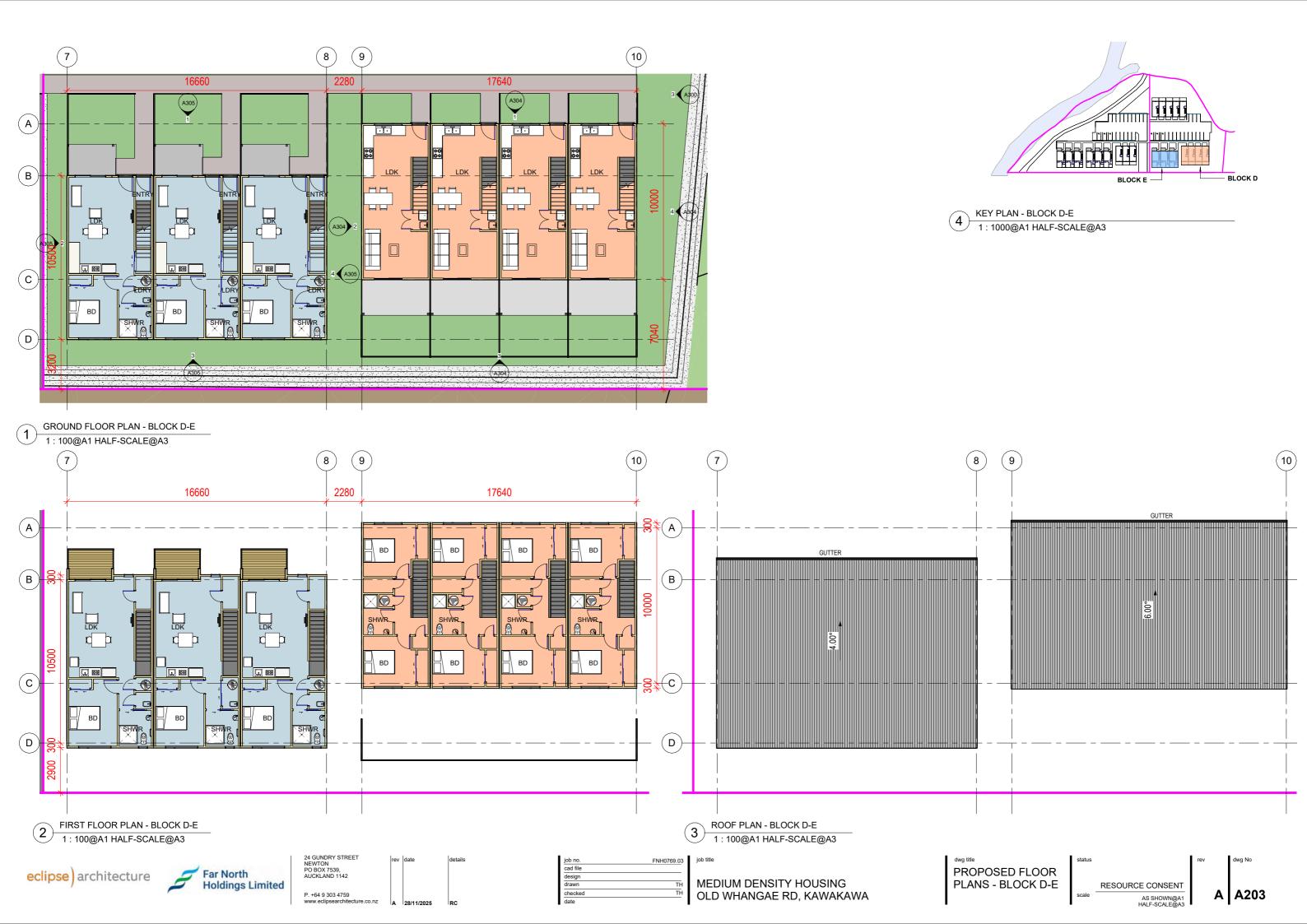


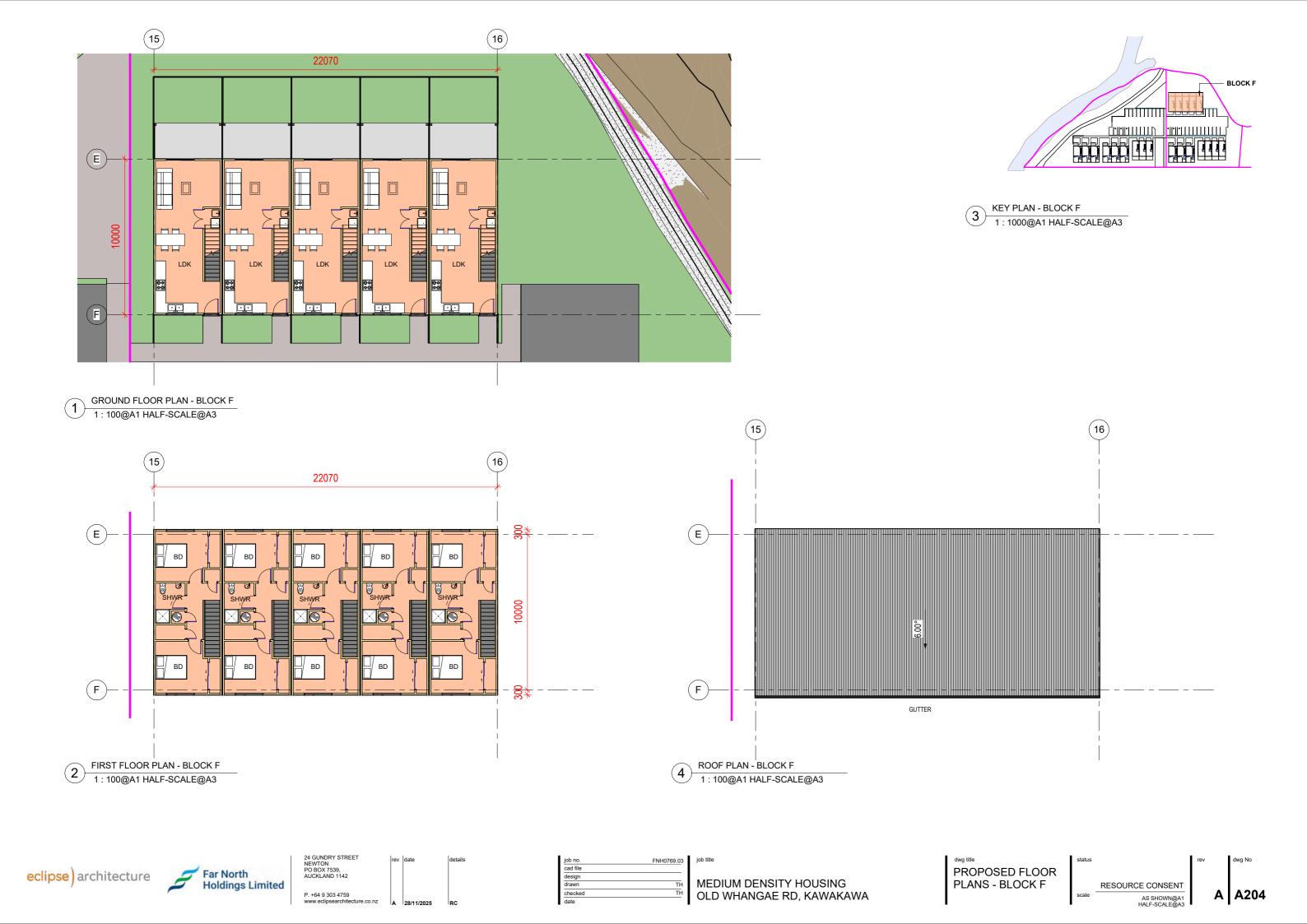


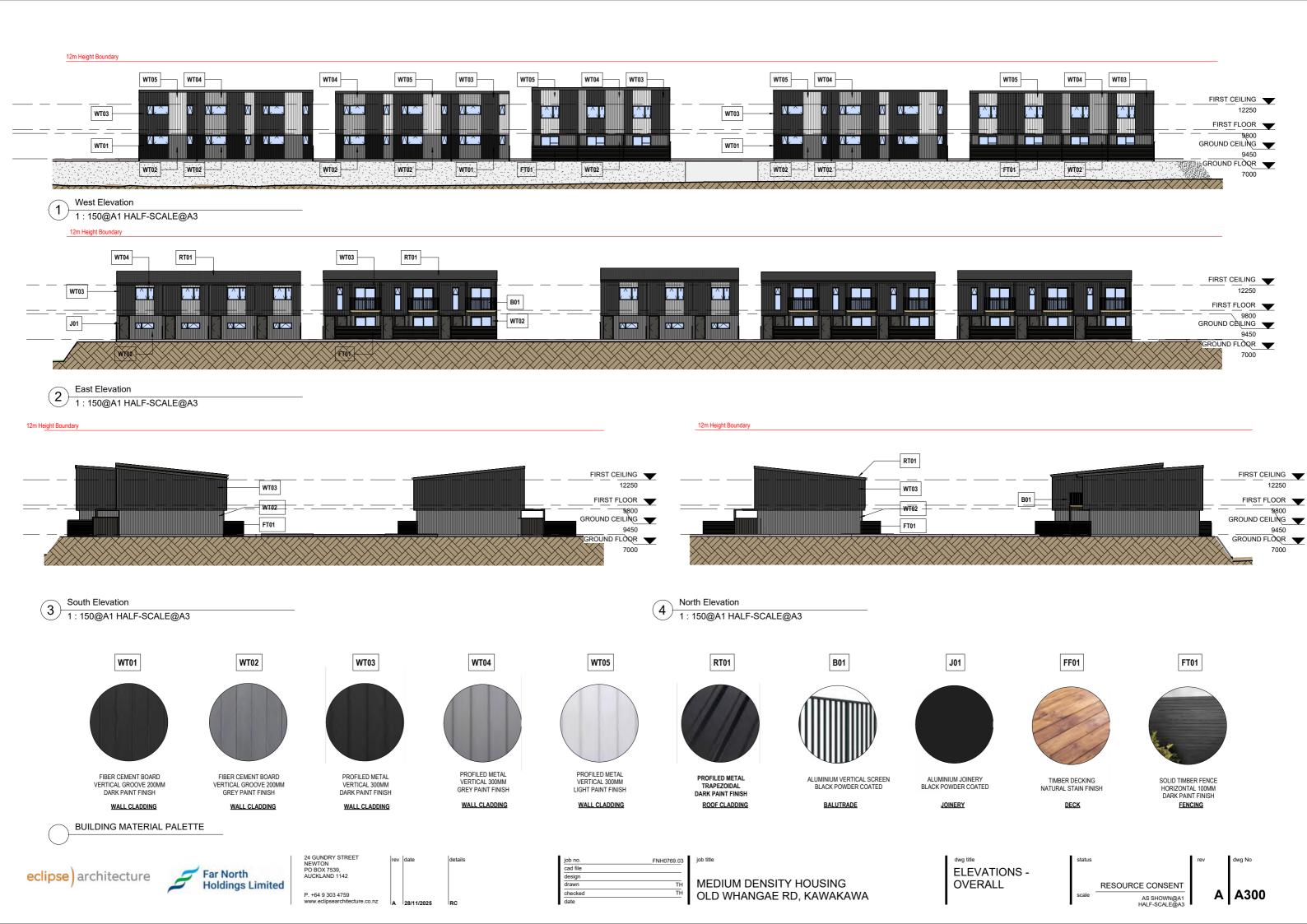


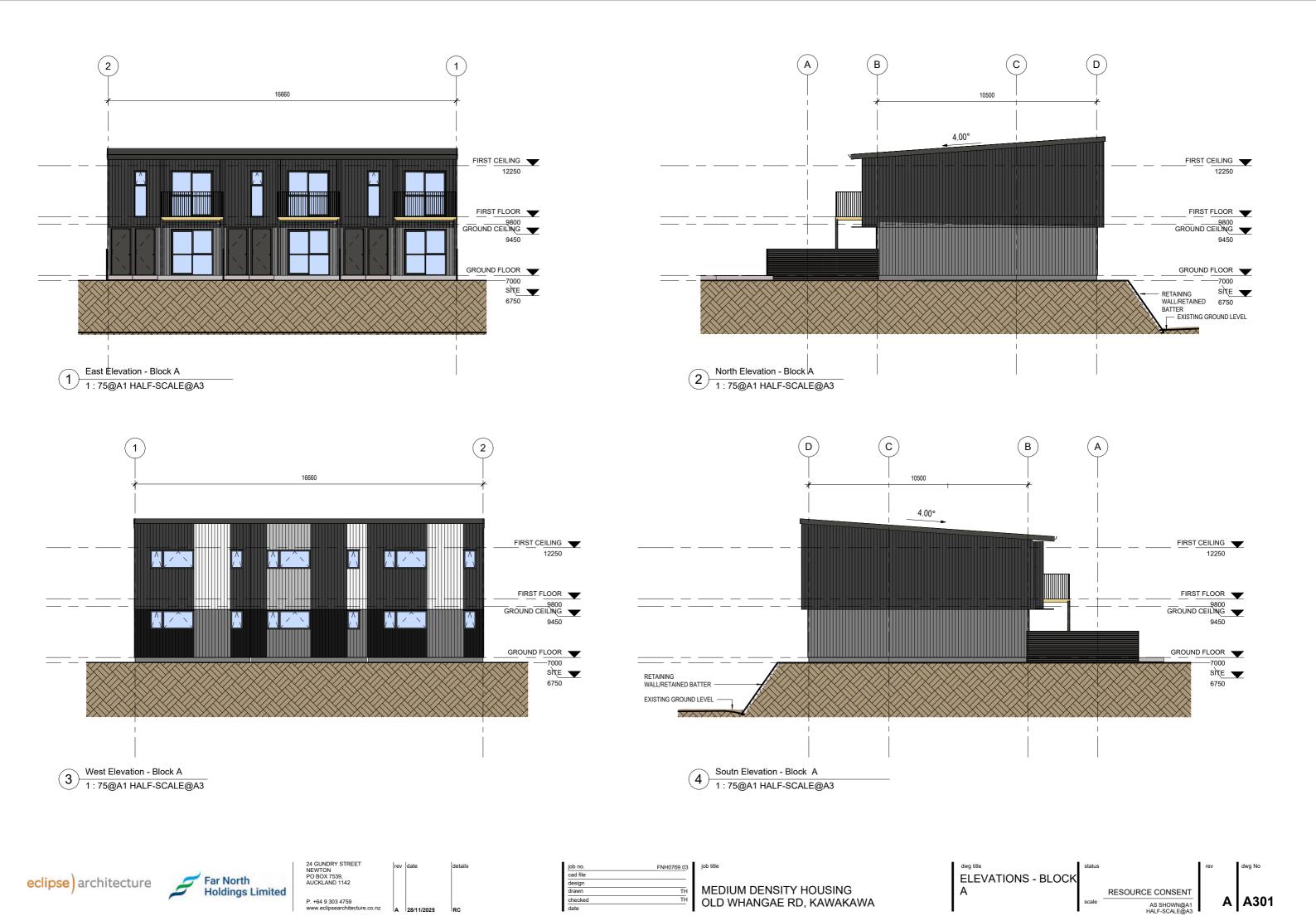


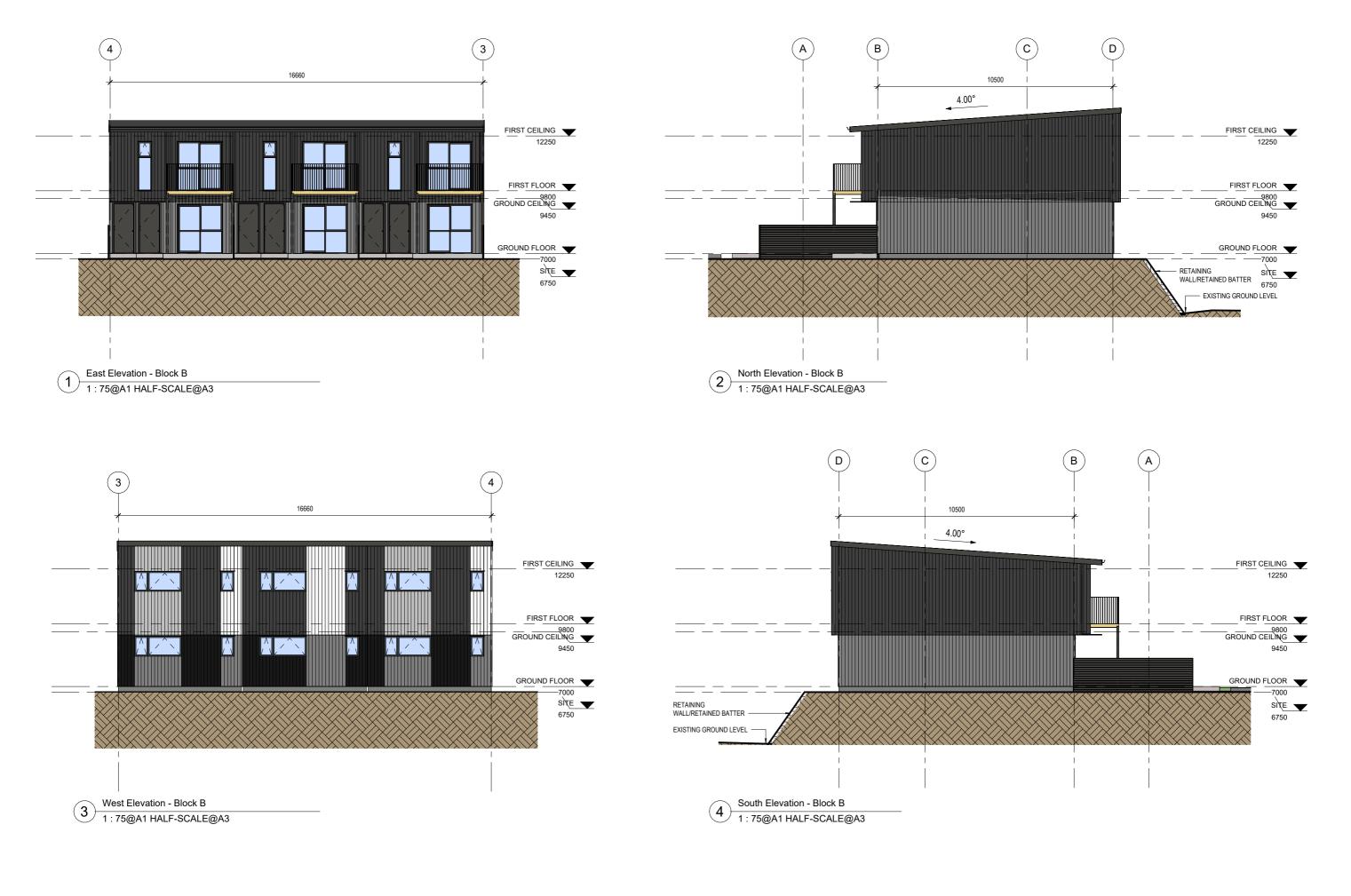












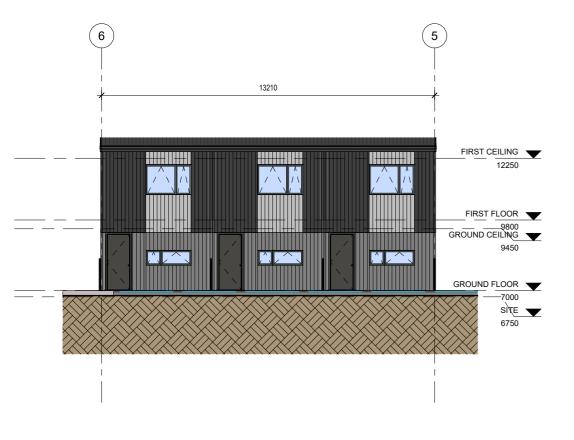






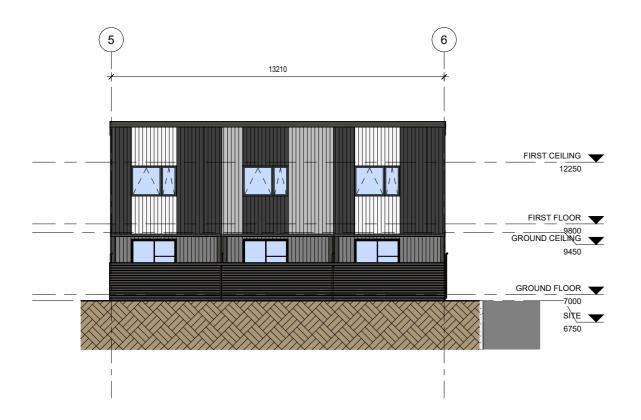






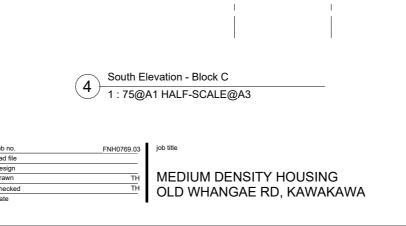
East Elevation - Block C

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West Elevation - Block C

1:75@A1 HALF-SCALE@A3



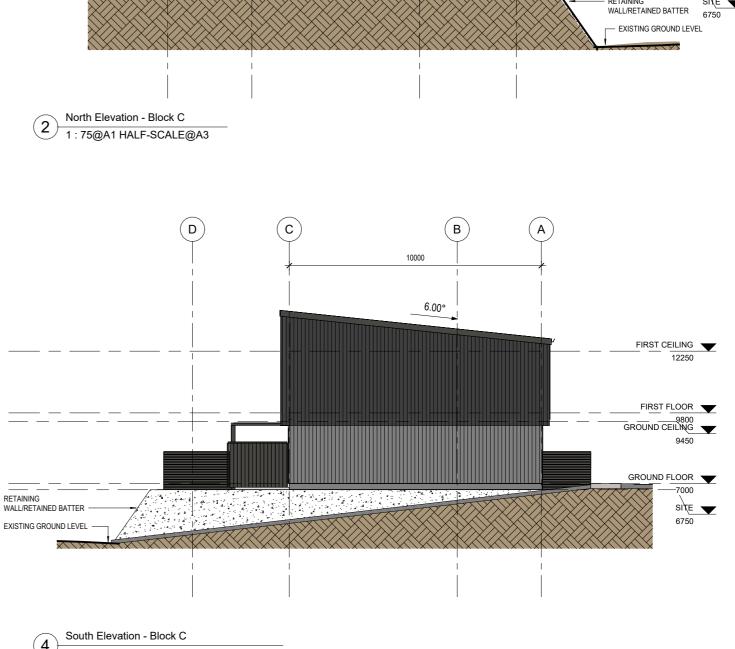
dwg title

ELEVATIONS - BLOCK
C

RESOURCE CONSENT

scale

AS SHOWN@A1
HALF-SCALE@A3



(c)

(D)

FIRST CEILING 12250

FIRST FLOOR

GROUND CEILING

GROUND FLOOR

RETAINING

SITE \_

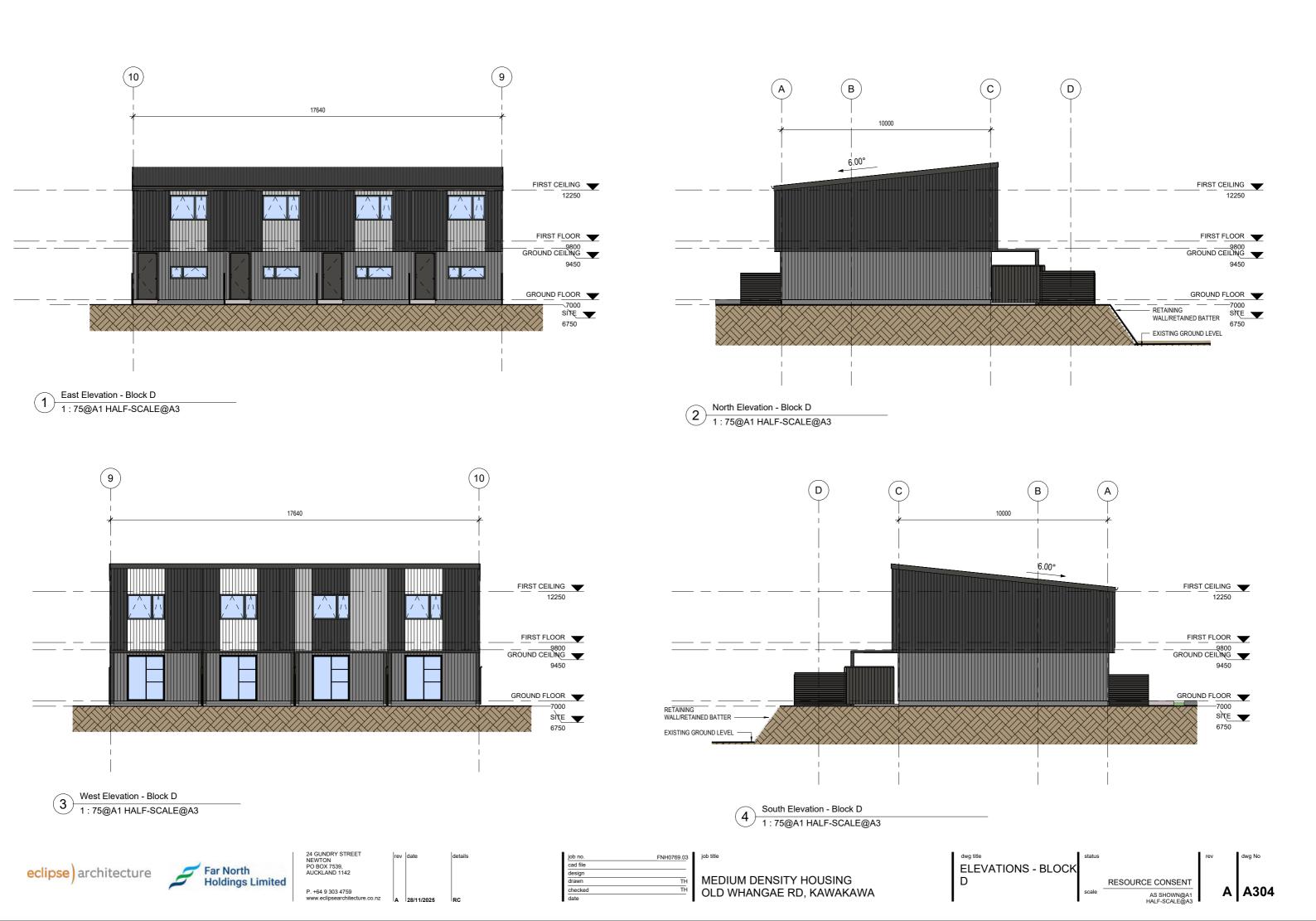
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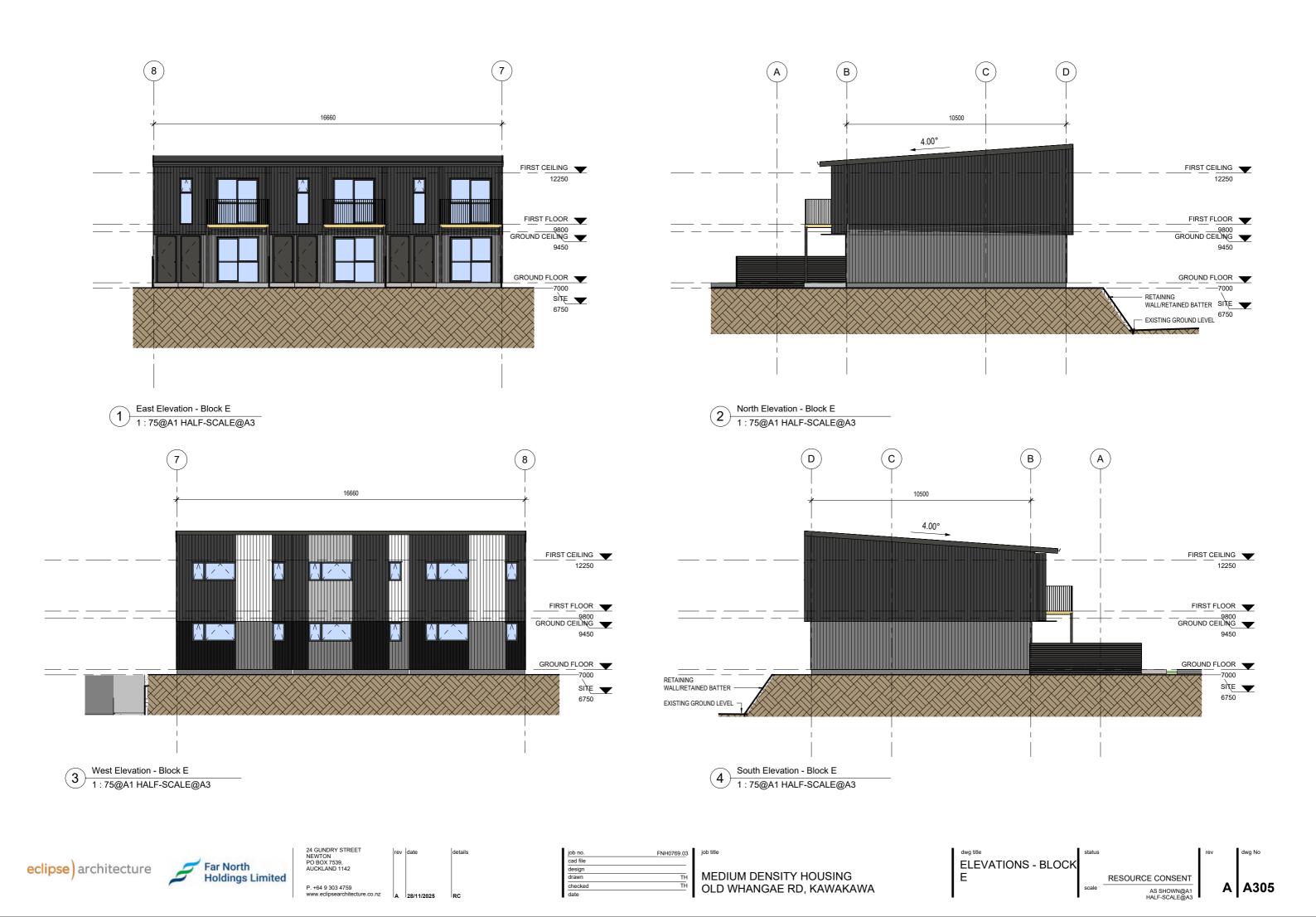
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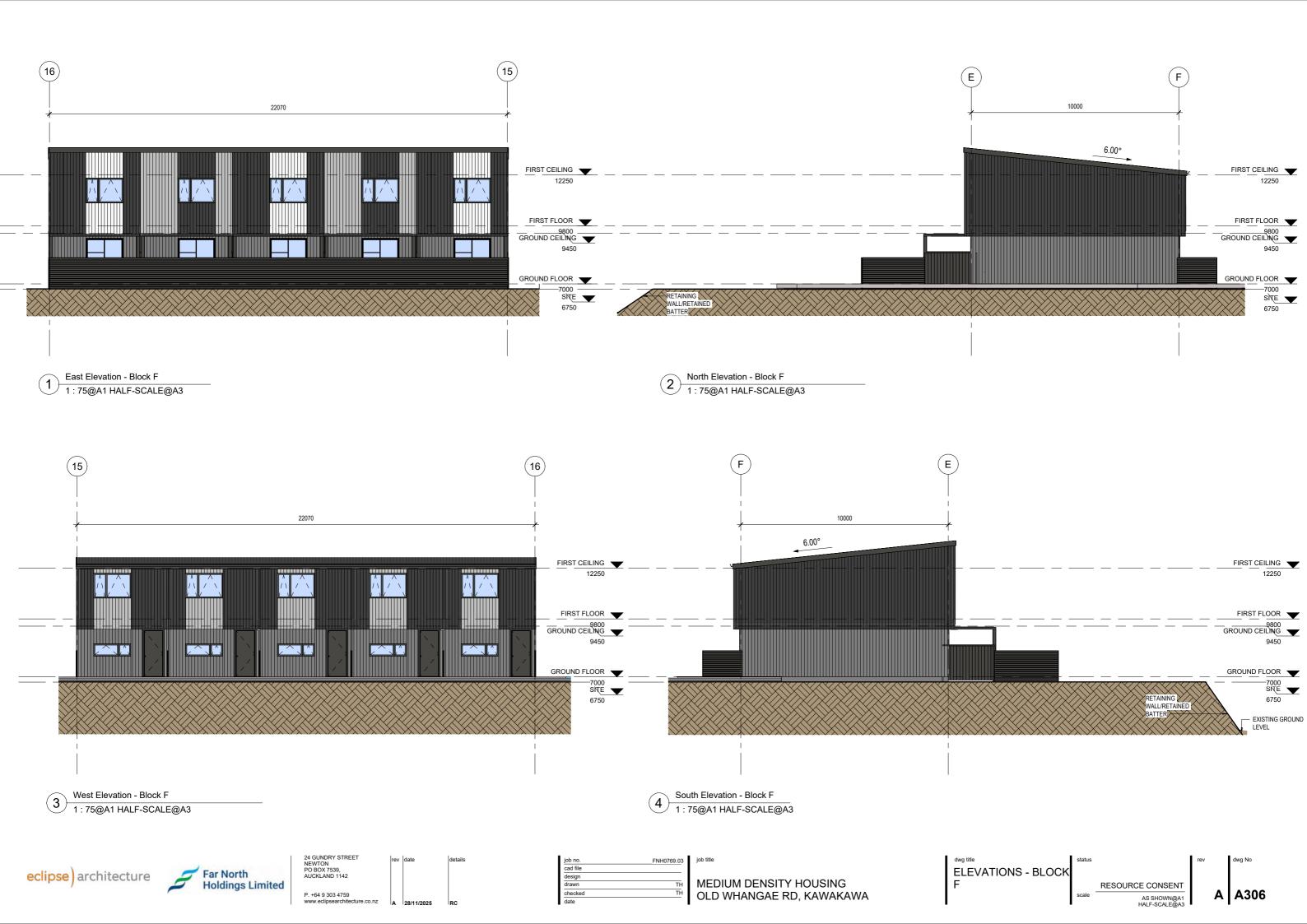
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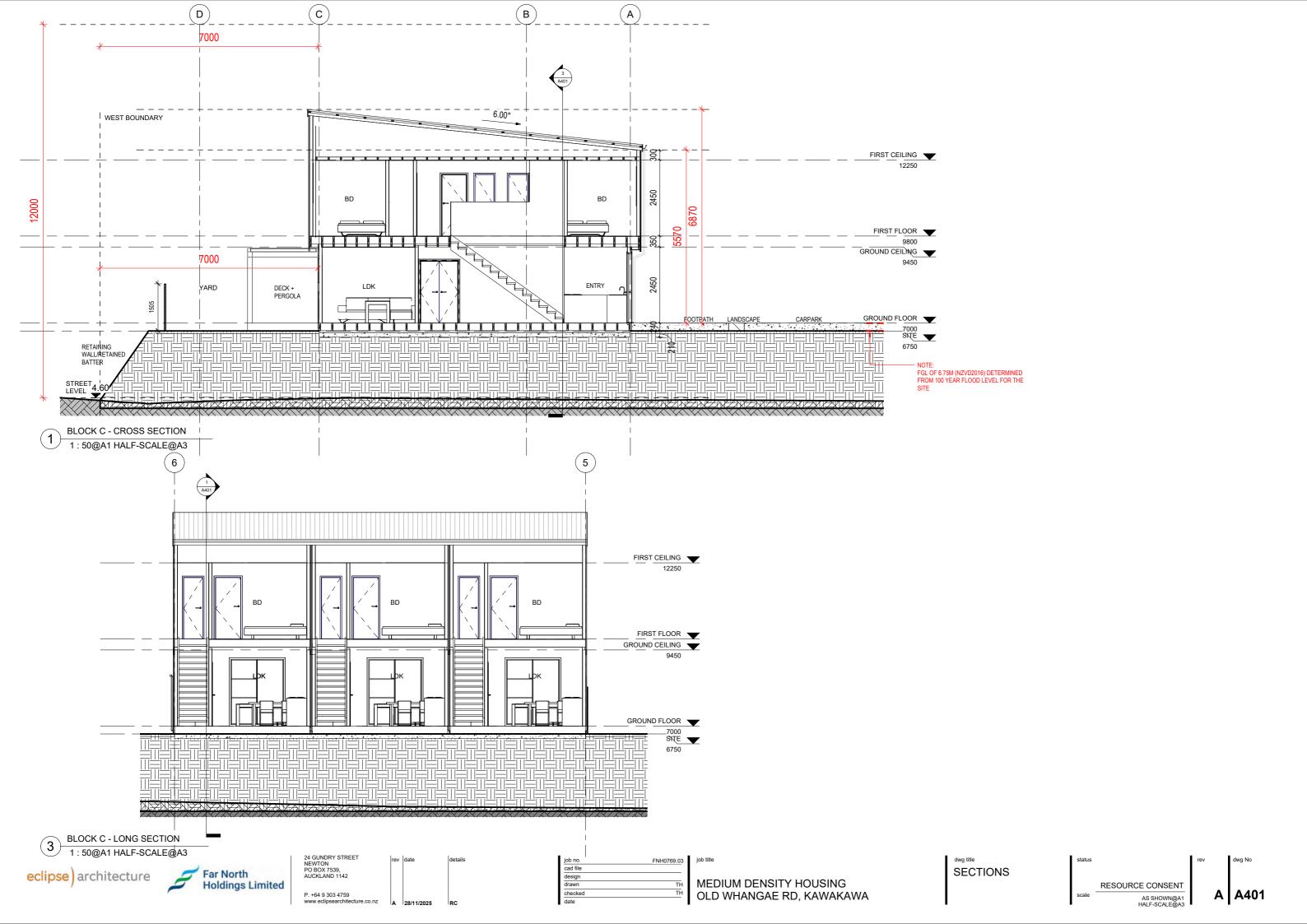
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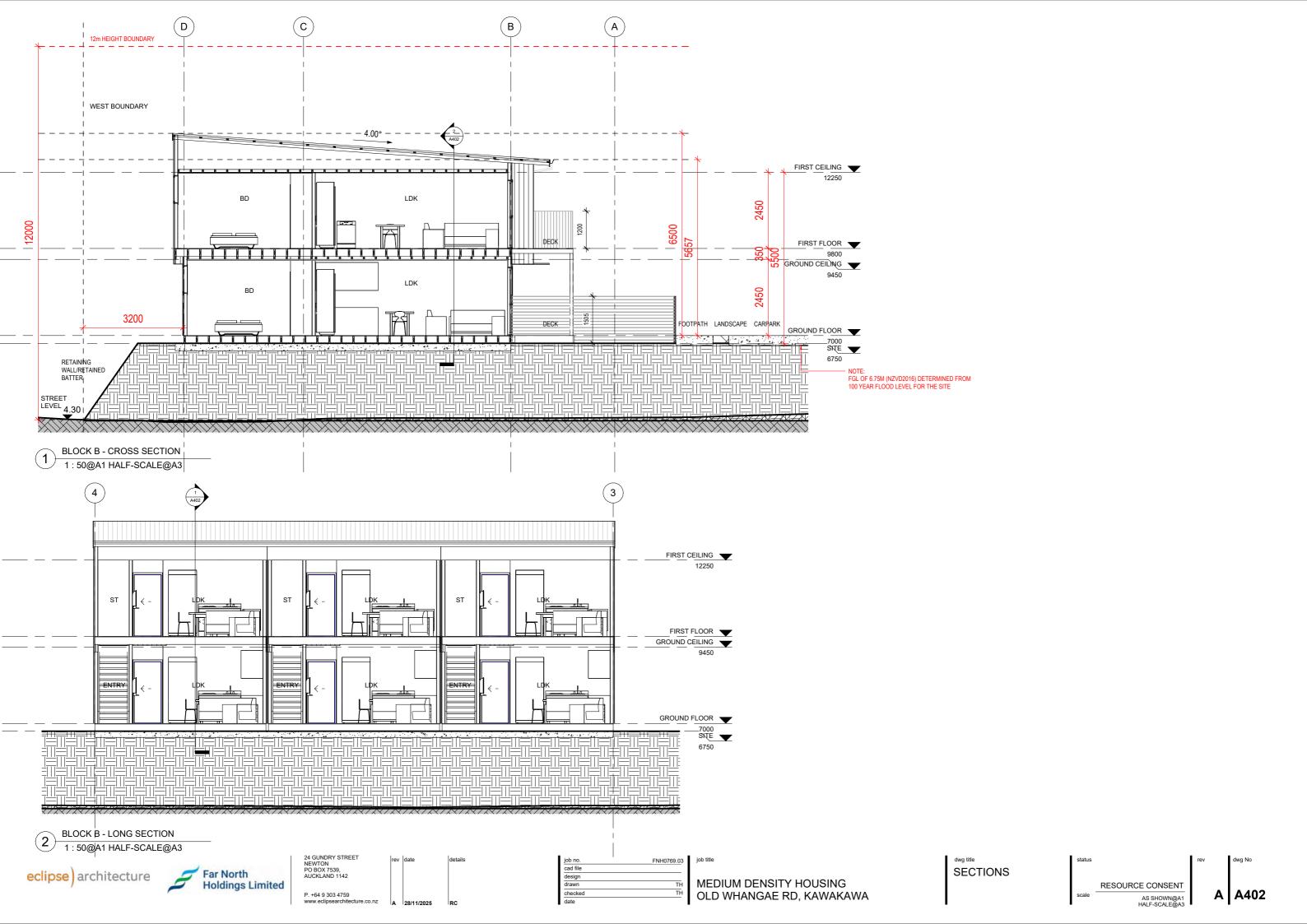












Old Whangae Road Development, Kawakawa – Far North Housing Limited

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## 6.2 Appendix B:

Resource consent engineering drawings prepared for the Old Whangae Road Development.

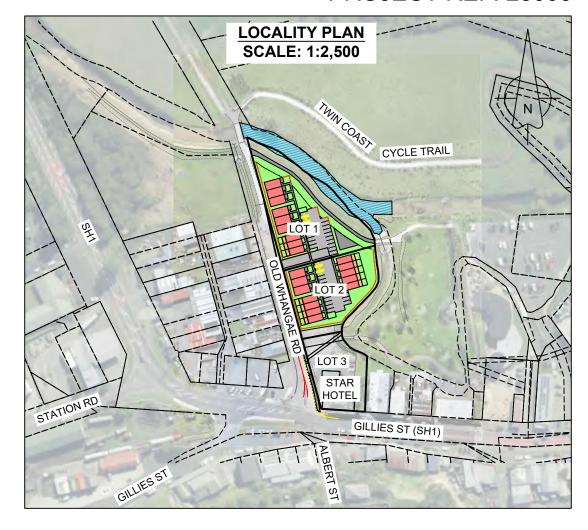


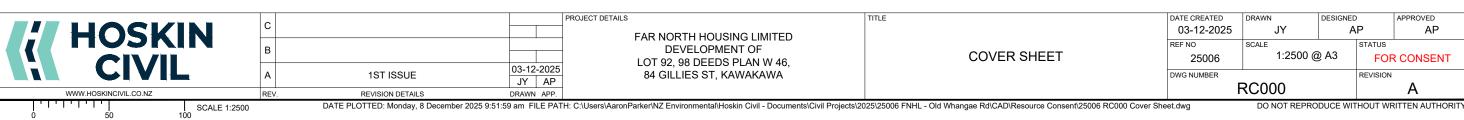
#### **SCHEDULE OF DRAWINGS** SHEET# **REV** TITLE RC000 **COVER SHEET** Α RC100 **EXISTING SITE PLAN - OVERVIEW** Α EXISTING SITE PLAN - SHEETS 1 - 2 RC101-102 Α RC200 **BULK EARTHWORKS PLAN** Α RC210 **EROSION & SEDIMENT CONTROL PLAN** Α EROSION & SEDIMENT CONTROL DETAILS - SHEETS 1 - 3 RC220-222 Α ROADING, RETAINING & FINISHED LEVELS PLAN - OVERVIEW Α RC300 RC301-303 ROADING, RETAINING & FINISHED LEVELS PLAN - SHEETS 1 - 3 Α RC400-401 DRAINAGE PLAN - SHEETS 1 - 2 Α RC410 EXISTING IMPERVIOUS AREAS CATCHMENT PLAN Α RC415 PROPOSED DEVELOPMENT IMPERVIOUS AREAS CATCHMENT PLAN Α RC420-422 STORMWATER LONGSECTIONS - SHEETS 1-3 Α RC430-431 SANITARY SEWER LONGSECTIONS - SHEETS 1-2 Α RC500 POTABLE WATER PLAN - OVERVIEW Α RC501 POTABLE WATER PLAN - SHEET 1 Α POTABLE WATER FIRE HYDRANT PLAN RC510 Α

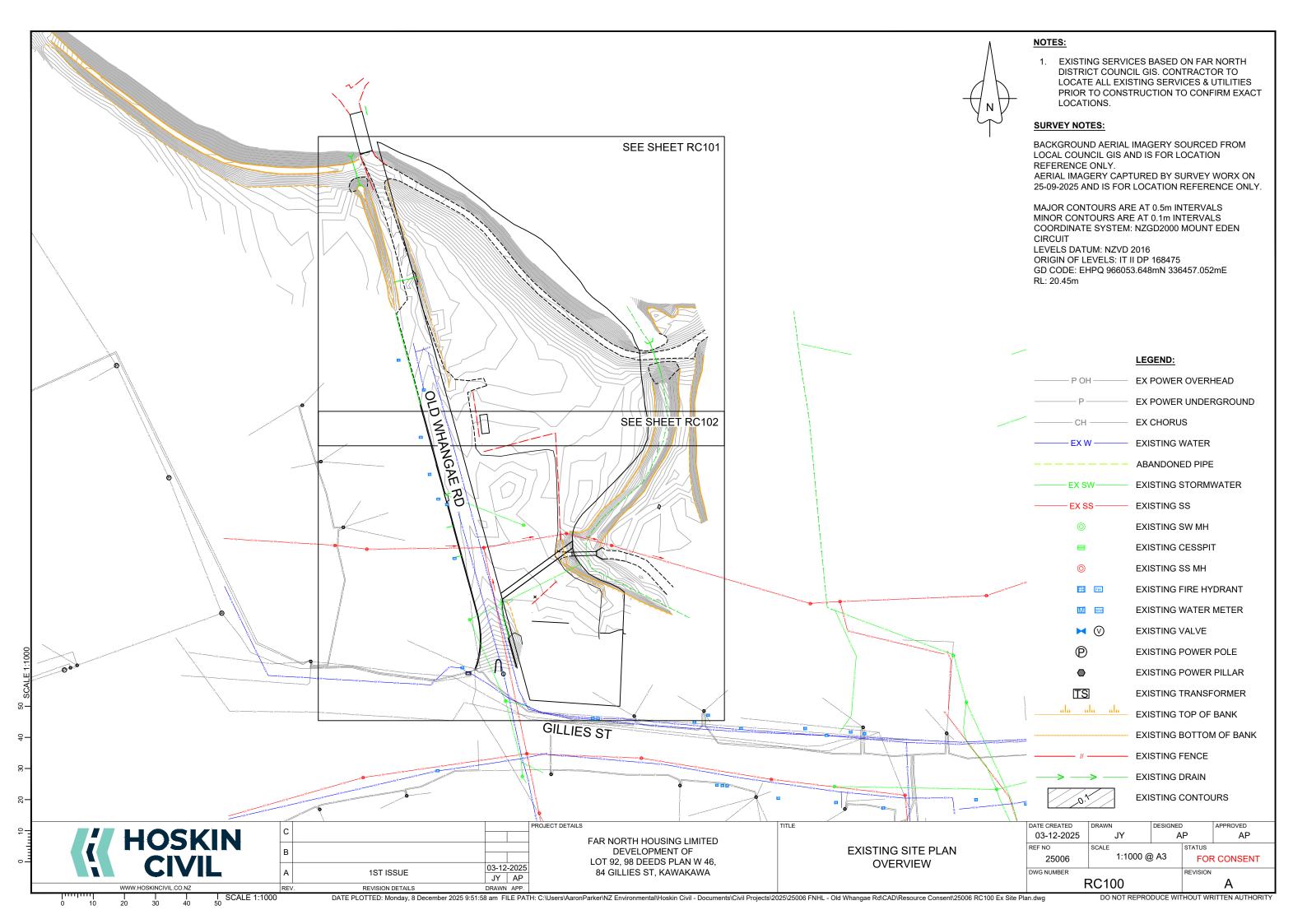
# **CIVIL ENGINEERING DESIGN** FOR RESOURCE CONSENT

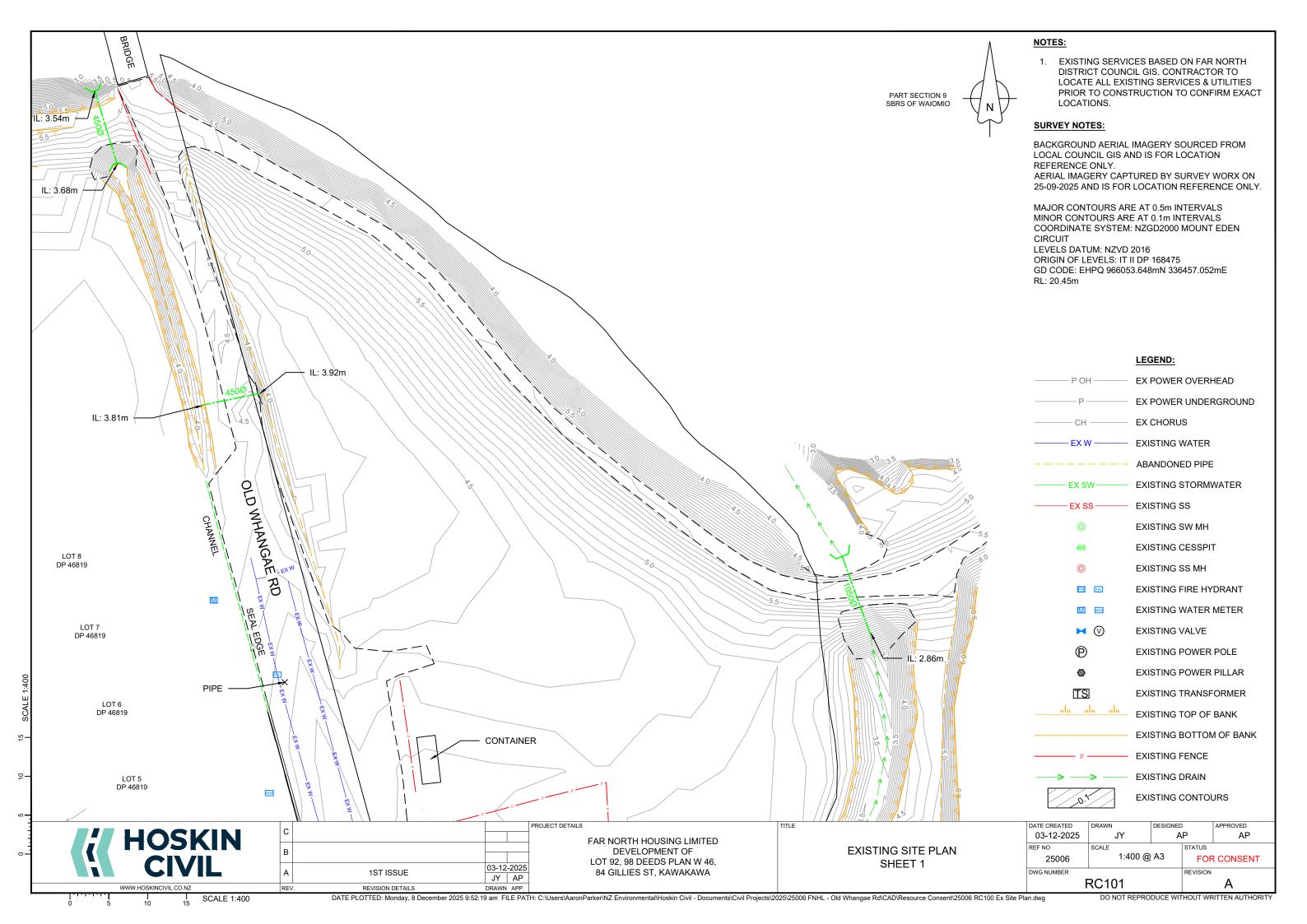
FAR NORTH HOUSING LTD LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

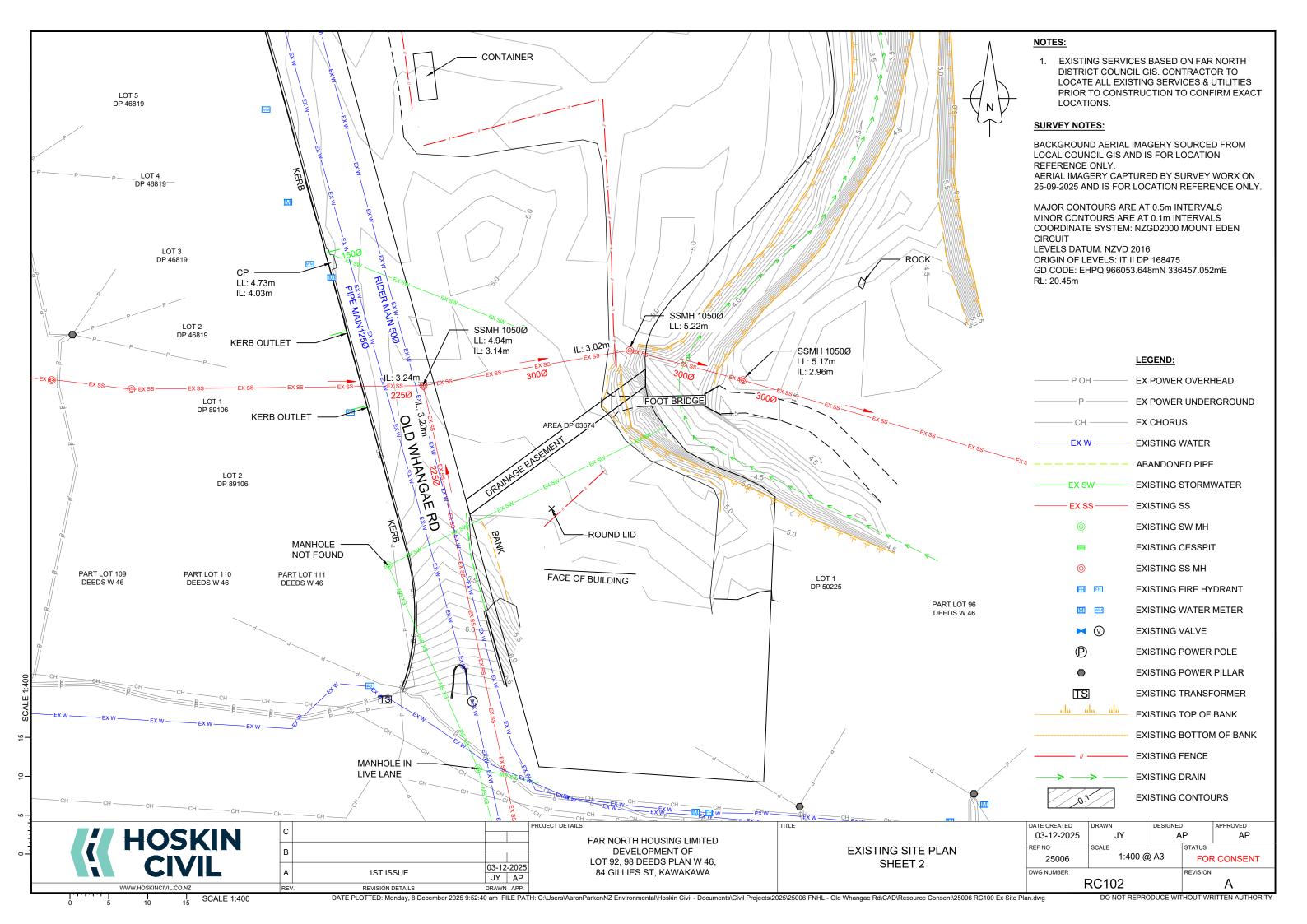
PROJECT REF: 25006

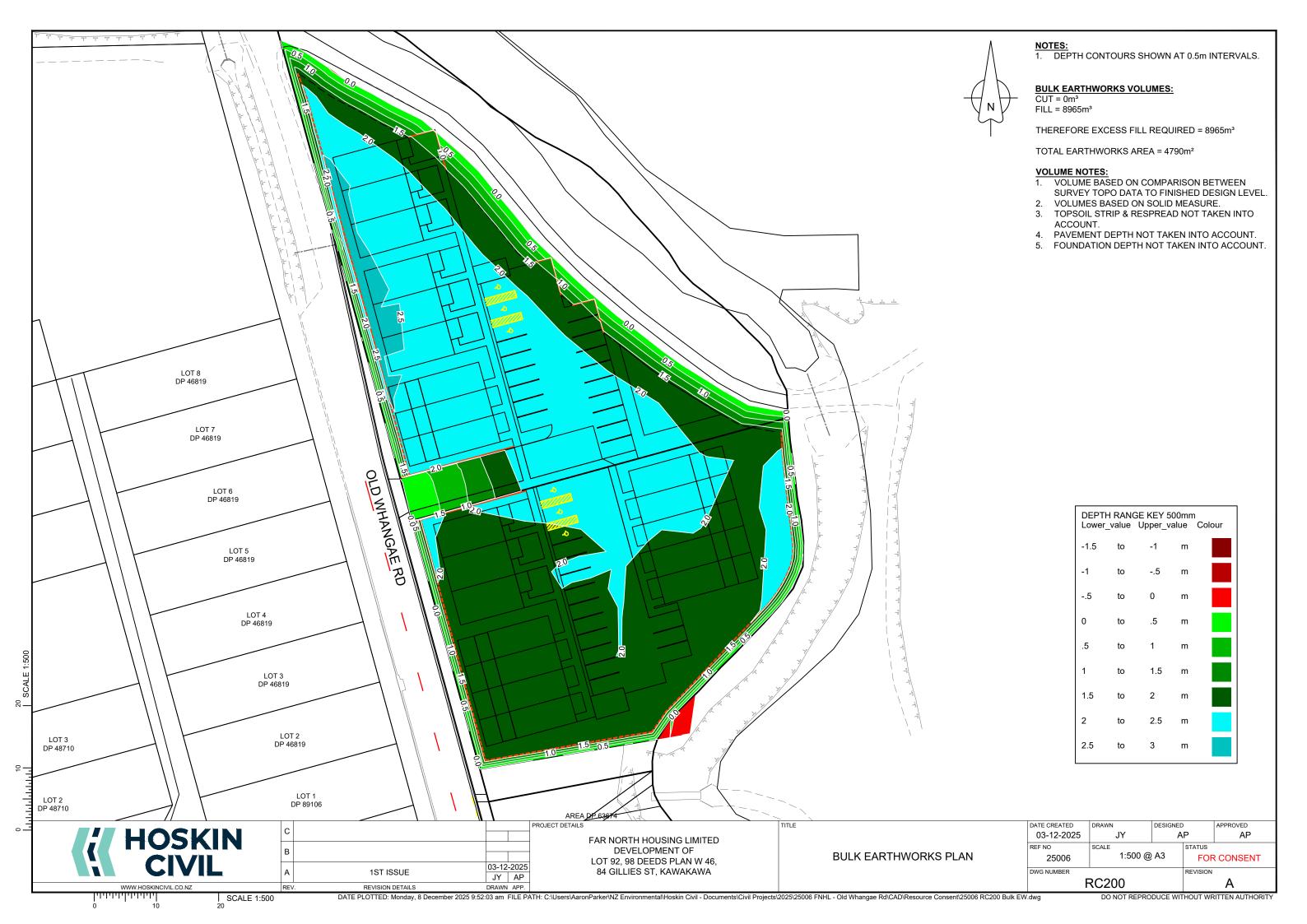












## NOTES: DESIGN CONTOURS AT 200mm INTERVALS. EXISTING CONTOURS AT 200mm INTERVALS. EROSION CONTROL - ALL SILT CONTROL MEASURES SHALL BE INSTALLED IN ACCORDANCE WITH GD05 AND PLACED PRIOR TO COMMENCEMENT OF EARTHWORKS. SUCH MEASURES SHALL BE SUBJECT TO FURTHER ADDITIONS AND ALTERATIONS, WHERE CONSIDERED NECESSARY, AS DIRECTED BY THE PROJECT MANAGER OR NRC, DURING THE PROGRESSION OF WORKS. IT IS ADVISED TO CONTACT NRC PRIOR TO COMMENCEMENT OF EARTHWORKS, AFTER INSTALLATION OF EROSION AND SEDIMENT CONTROL DEVICES TO ENSURE THEY HAVE BEEN INSTALLED TO THE SATISFACTION OF NRC. LEGEND: ANY LOCATIONS EARTH BUND IS NOT SUITABLE (DUE TO SPACE **EXISTING CONTOURS** LIMITATIONS), SILT FENCE TO BE INSTALLED PROPOSED CONTOURS — EXTENT OF EARTHWORKS (4790m²) SILT FENCE EARTH BUND DECANT OVERLAND FLOWPATH WITH CATCHMENT AREA OF 2260m<sup>2</sup> SITE TO BE SPLIT INTO EARTH BUND TWO CATCHMENTS OF (DISCHARGE INTO LESS THAN 3000m<sup>2</sup> EXISTING CULVERT) EARTH BUND DECANT EARTH BUND DECANT WITH CATCHMENT STABILISED AREA OF 2440m<sup>2</sup> CONSTRUCTION ENTRANCE OLD WHANGAEF 召 HOSKIN CIVIL 03-12-2025 FAR NORTH HOUSING LIMITED DEVELOPMENT OF **EROSION & SEDIMENT CONTROL PLAN** 1:750 @ A3 25006 FOR CONSENT LOT 92, 98 DEEDS PLAN W 46, 03-12-2025 1ST ISSUE 84 GILLIES ST, KAWAKAWA JY AP RC210 REVISION DETAILS DRAWN APP. DO NOT REPRODUCE WITHOUT WRITTEN AUTHORITY DATE PLOTTED: Monday, 8 December 2025 9:52:36 am FILE PATH: C:\Users\AaronParker\NZ Environmental\Hoskin Civil - Documents\Civil Projects\2025\25006 FNHL - Old Whangae Rd\CAD\Resource Consent\25006 RC210 ESCP.dwg

# STABILISED CONSTRUCTION ENTRANCE SPECIFICATIONS:

#### **APPLICATION**

USE A STABILISED CONSTRUCTION ENTRANCE AT ALL POINTS OF CONSTRUCTION SITE INGRESS AND EGRESS WITH A CONSTRUCTION PLAN LIMITING TRAFFIC TO THESE ENTRANCES ONLY. THEY ARE PARTICULARLY USEFUL ON SMALL CONSTRUCTION SITES BUT CAN BE UTILISED FOR ALL PROJECTS.

#### DESIGN:

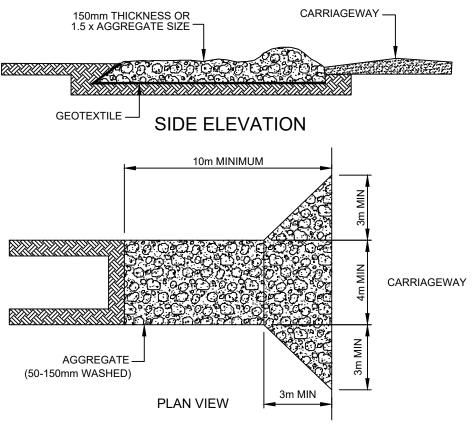
CLEAR THE ENTRANCE AND EXIT AREA OF ALL VEGETATION, ROOTS AND OTHER UNSUITABLE MATERIAL AND PROPERLY GRADE IT.

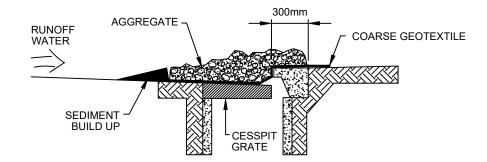
- 1. LAY WOVEN GEOTEXTILE; PIN DOWN EDGES AND OVERLAP JOINTS.
- 2. PROVIDE DRAINAGE TO CARRY RUNOFF FROM THE STABILISED CONSTRUCTION ENTRANCE TO A SEDIMENT CONTROL MEASURE.
- 3. PLACE AGGREGATE TO THE SPECIFICATIONS BELOW AND SMOOTH IT.
- 4. STABILISED CONSTRUCTION ENTRANCE AGGREGATE SPECIFICATIONS:

AGGREGATE SIZE	5-150mm WASHED AGGREGATE
THICKNESS	150mm MINIMUM OR 1.5 X AGGREGATE SIZE
LENGTH	10m MINIMUM LENGTH RECOMMENDED
WIDTH	4m MINIMUM

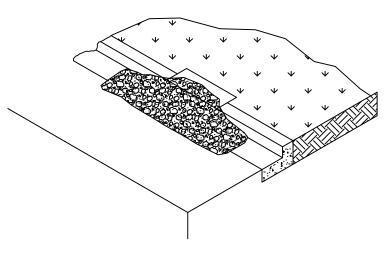
#### MAINTENANCE

- MAINTAIN THE STABILISED CONSTRUCTION ENTRANCE IN A CONDITION TO PREVENT SEDIMENT FROM LEAVING THE CONSTRUCTION SITE. AFTER EACH RAINFALL INSPECT ANY STRUCTURE USED TO TRAP SEDIMENT FROM THE STABILISED CONSTRUCTION ENTRANCE AND CLEAN OUT AS NECESSARY.
- 2. WHEN WHEEL WASHING IS ALSO REQUIRED, ENSURE THIS IS DONE ON AN AREA STABILISED WITH AGGREGATE WHICH DRAINS TO AN APPROVED SEDIMENT RETENTION FACILITY.





## **CROSS SECTION**



STORMWATER INLET PROTECTION
- FILTER MEDIA DESIGN

## STABILISED CONSTRUCTION ENTRANCE

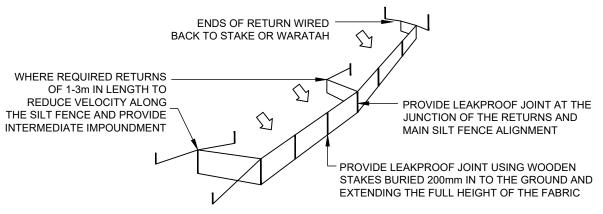


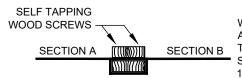
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FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

EROSION & SEDIMENT CONTROL DETAILS SHEET 1

	DATE CREATED	DRAWN	DESIGNED	)	APPROVED	
	03-12-2025	JY	AP		AP	
:	REF NO	NTS @ A3		STATUS		
,	25006			FOR CONSENT		
	DWG NUMBER			REVISION		
	F	RC220			Α	
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WRAP BOTH ENDS OF THE FABRIC AROUND ONE STAKE AND CLAMP THE OTHER STAKE TO IT USING SELF TAPPING WOOD SCREWS AT 150mm SPACINGS

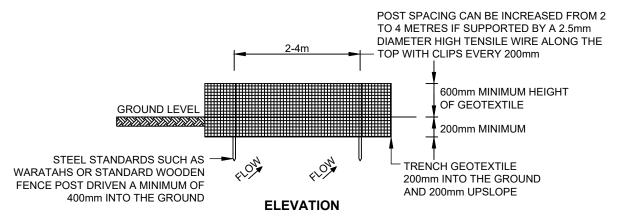
#### STANDARD FABRIC JOINT

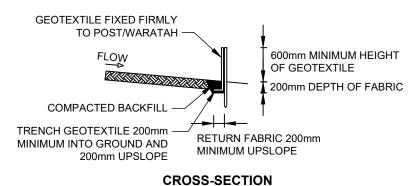
#### SILT FENCE DESIGN CRITERIA:

SLOPE STEEPNESS %	SLOPE LENGTH (m) (MAX)	SPACING OF RETURNS (m)
< 2%	N/A	UNLIMITED
2-10%	40	60
10-20%	30	50
20-33%	20	40
33-50%	15	30
>50%	6	20

GRAB TENSILE STRENGTH: TENSILE MODULUS: APPARENT OPENING SIZE: >440N (ASTM D4632) 0.140 pa (MINIMUM) 0.1-0.5mm (ASTM D4751)

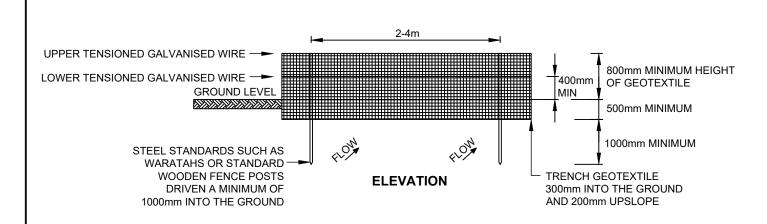
#### SILT FENCE WITH RETURNS AND SUPPORT WIRE

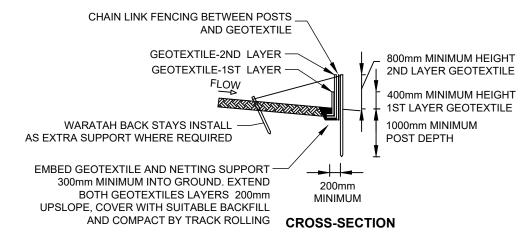




#### OK000-0E

### SILT FENCE CONSTRUCTION





### SUPER SILT FENCE DESIGN CRITERIA:

SLOPE LENGTH (m) (MAX)	SPACING OF RETURNS (m)
UNLIMITED	60
60	50
30	40
30	30
15	20
	UNLIMITED 60 30 30

## SUPER SILT FENCE CONSTRUCTION

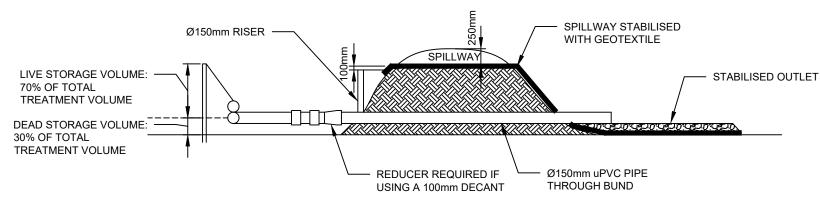


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FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

EROSION & SEDIMENT CONTROL DETAILS SHEET 2

	DATE CREATED	DRAWN	DESIGNED	,	APPROVED	
	03-12-2025	JY	AP		AP	
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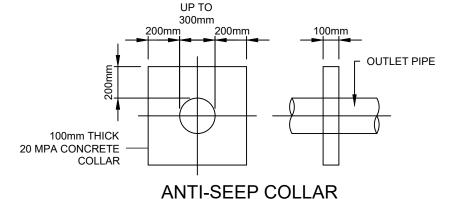
### **DECANTING EARTH BUND**

NOTE: THE 100mm DIAMETER PVC PIPE UPSTAND IS ONLY REQUIRED WHERE THE 2m WIDE EMERGENCY SPILLWAY DISCHARGES TO VULNERABLE AREA OR WHERE THE DISCHARGE IS REQUIRED TO BE PIPED TO A SAFE OUTFALL SUCH AS A STORMWATER MANHOLE. IF THE UPSTAND IS NOT REQUIRED THE DECANT CAN BE CONNECTED DIRECT TO A 40mm DIAMETER OUTFALL PIPE AND THE TREATMENT VOLUME IS MEASURED TO THE INVERT OF THE EMERGENCY SPILLWAY.

NOTE: THE DECANT HAS A 40mm DIAMETER PVC PIPE WITH A 1.3m LONG ARM (INCLUDING FLEXIBLE JOINT), A 0.5m LONG DECANT AND 20 x 10mm DIAMETER EQUALLY SPACED HOLES POSITIONED HORIZONTALLY AT 10 AND 2 OCLOCK

0.5m LONG 100mm DIAMETER PVC PIPE FLOAT WITH STANDARD 100mm END CAPS. THE FLOAT IS STRAPPED TO THE 40mm DIAMETER PVC DECANT PIPE WITH STAINLESS STEEL STRAPS OR ZIP TIES. NYLON CORD TIES TO SUSPEND DECANT FROM WARATAHS AT DECANT AND FLOAT CORRECT HEIGHT STANDARD 40mm **END CAPS (GLUED)** 100mm DIAMETER PVC PIPE UPSTAND WITH THE TOP POSITIONED 100mm BELOW STANDARD 40mm THE LEVEL OF THE EMERGENCY SPILLWAY. TEE JOINT (GLUED) THE TREATMENT VOLUME IS TO BE MEASURED TO THE TOP OF THE UPSTAND. FLEXIBLE RUBBER/NEOPRENE JOINT (SUCH AS PLUMBQWIK) HOSE CLAMPED FOR EASE OF REUSE JOIN SHOULD 100mm TO 40mm REDUCER BE MADE USING PK SCREWS AND FITTING TO BE GLUED CONSTRUCTION TAPE -STANDARD 100mm TEE JOINT (GLUED)

## 40mm DECANT WITH UPSTAND FOR DECANTING EARTH BUND



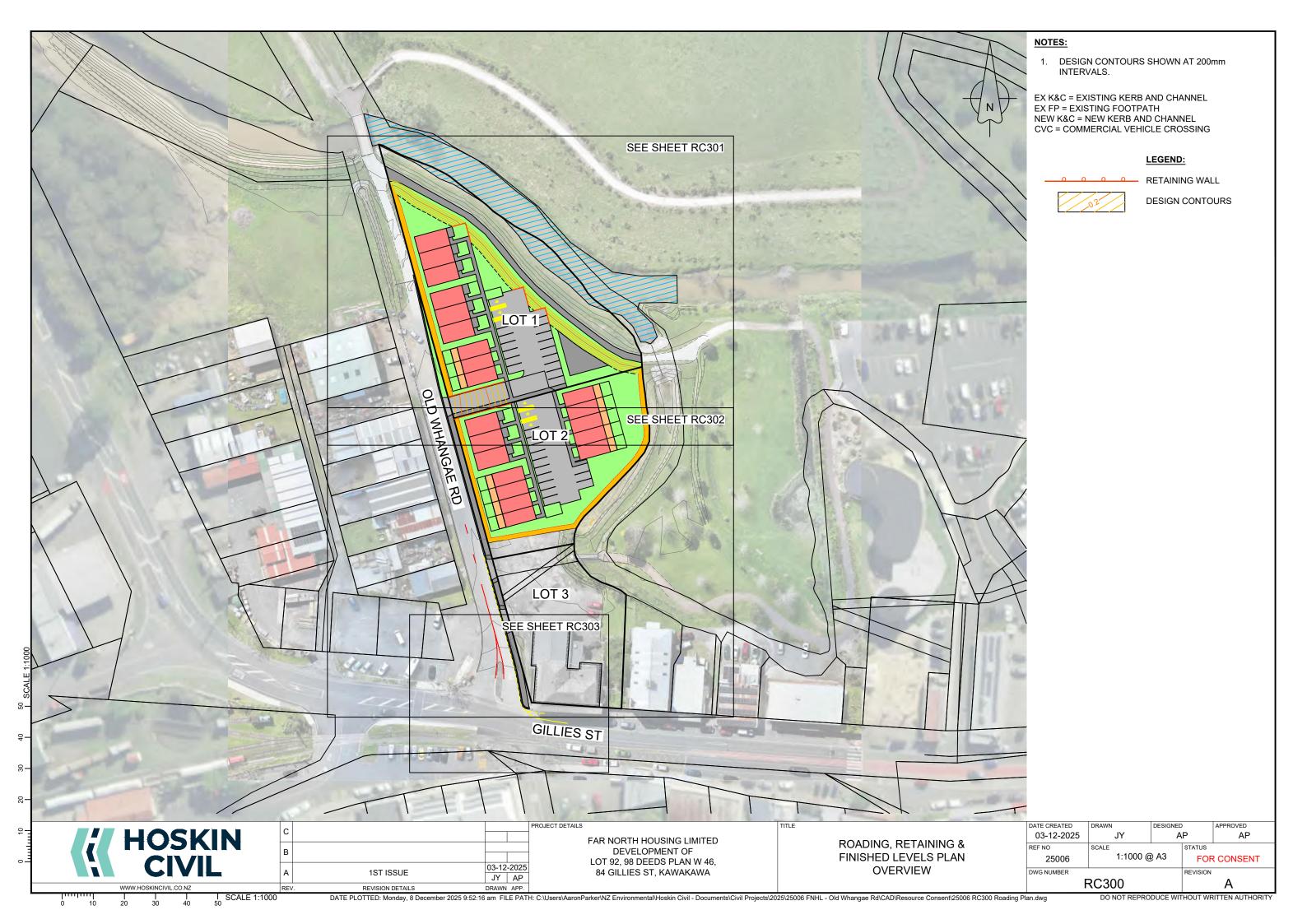


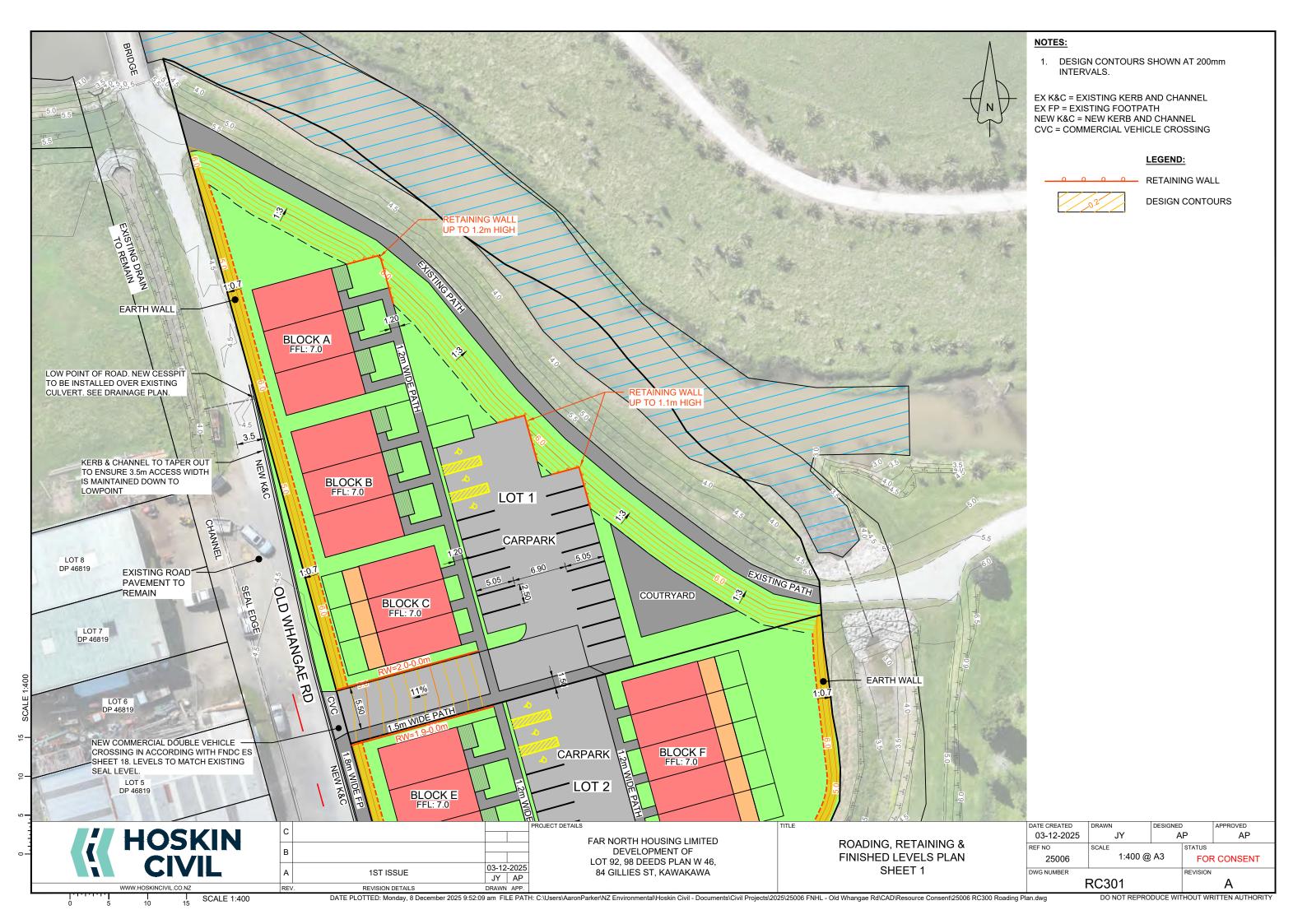
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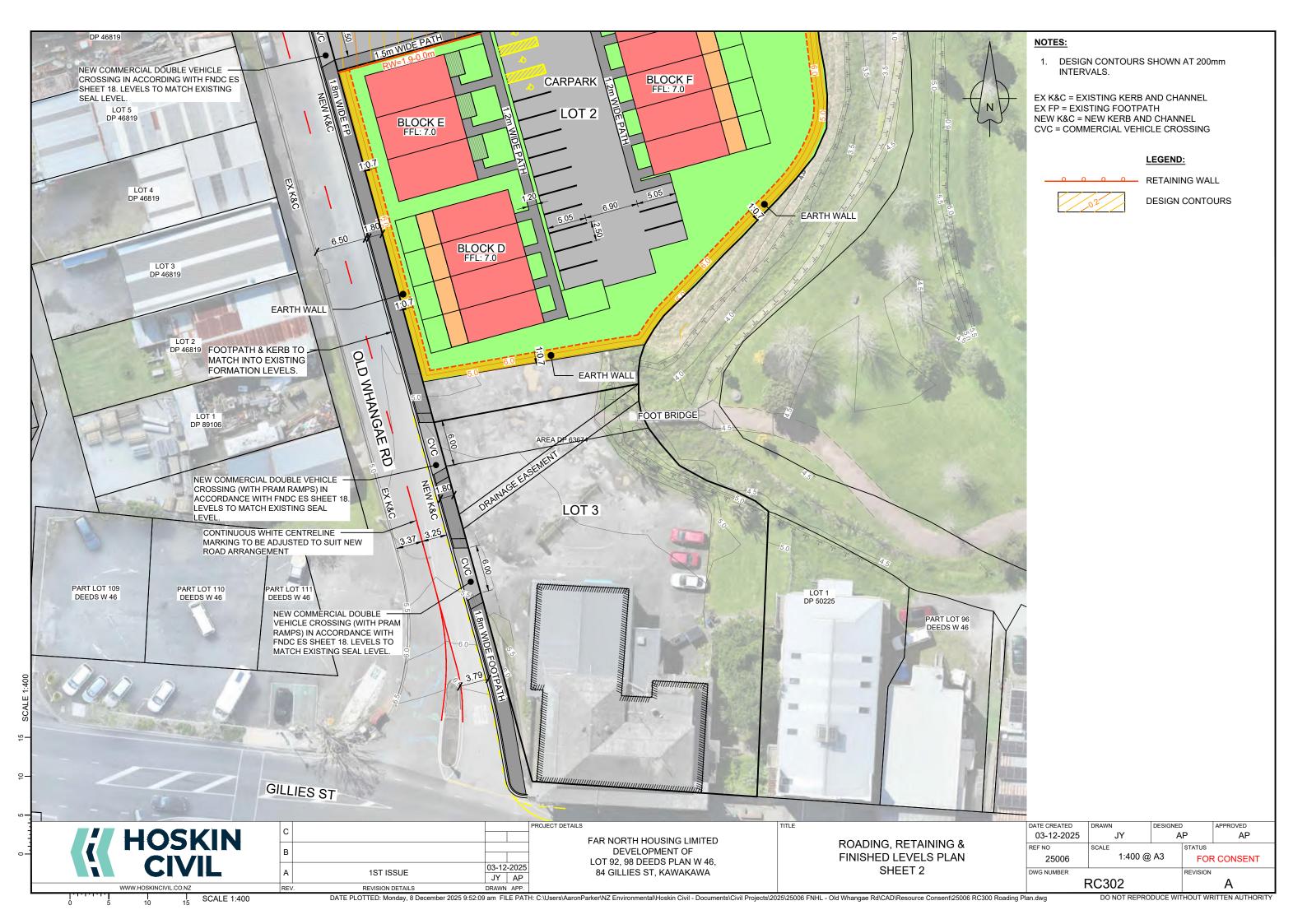
R NORTH HOUSING LIMITED DEVELOPMENT OF T 92, 98 DEEDS PLAN W 46, 34 GILLIES ST, KAWAKAWA

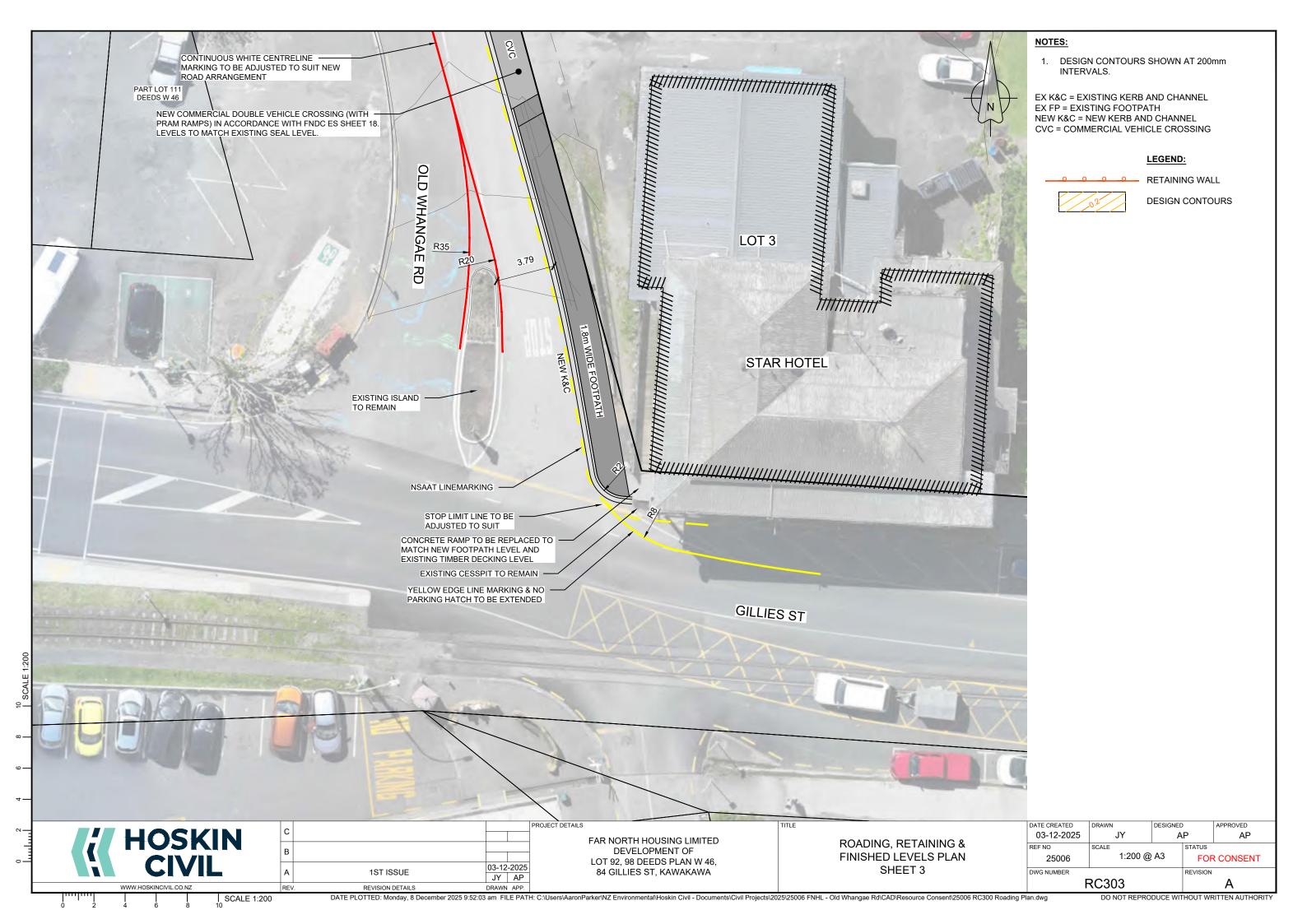
**EROSION & SEDIMENT CONTROL DETAILS** SHEET 3

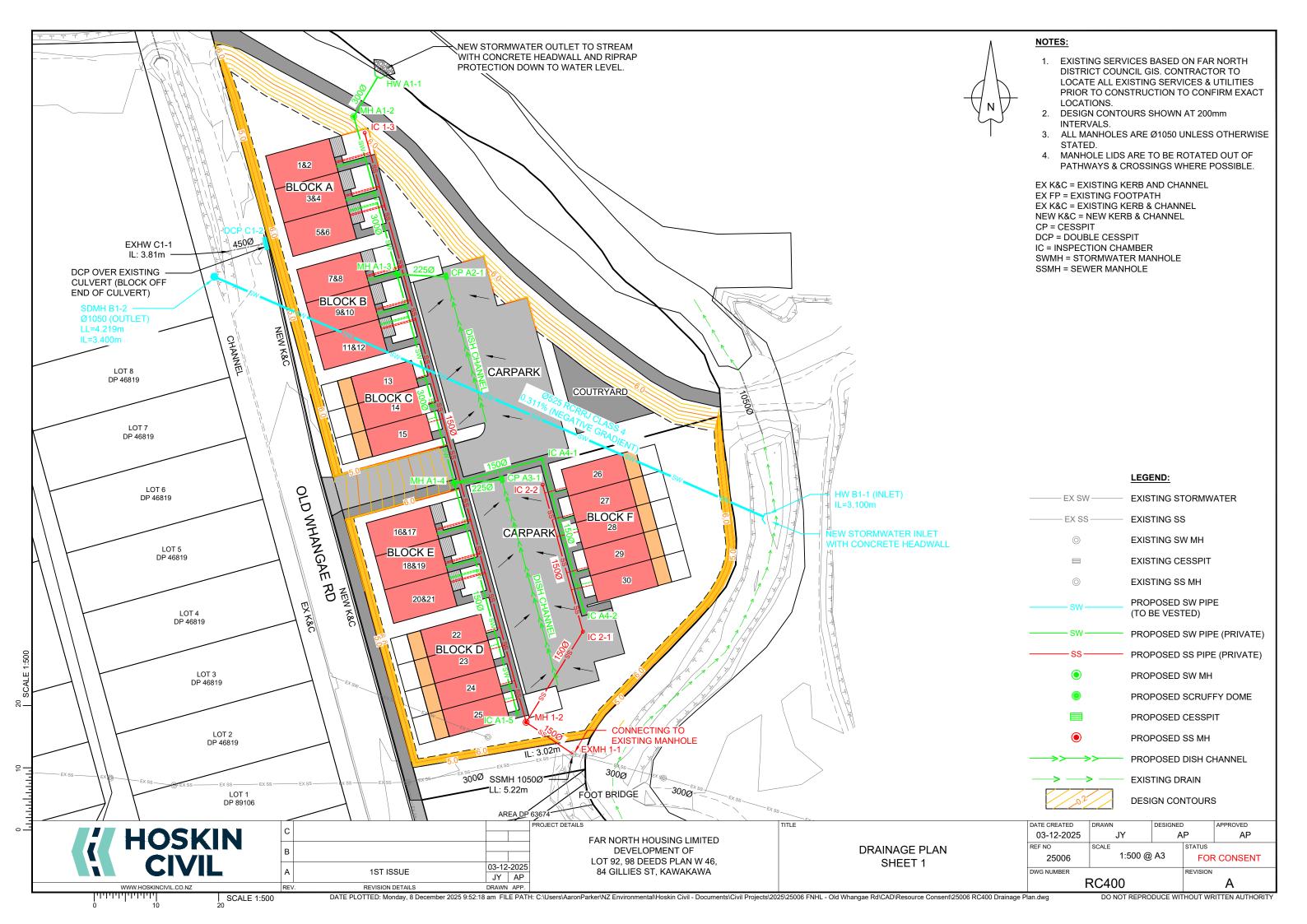
03-12-2025 JΥ ΑP NTS @ A3 25006 FOR CONSENT RC222

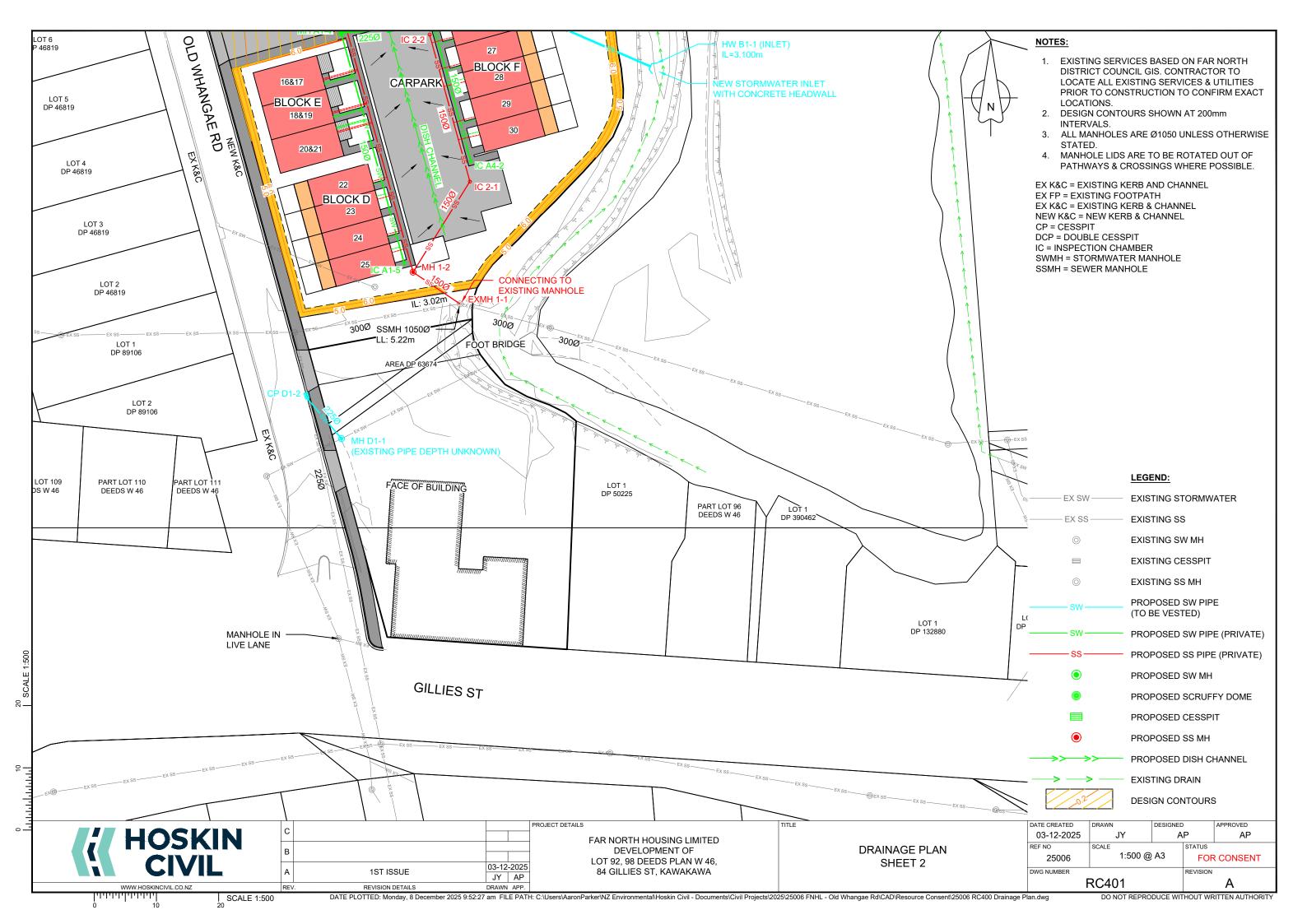




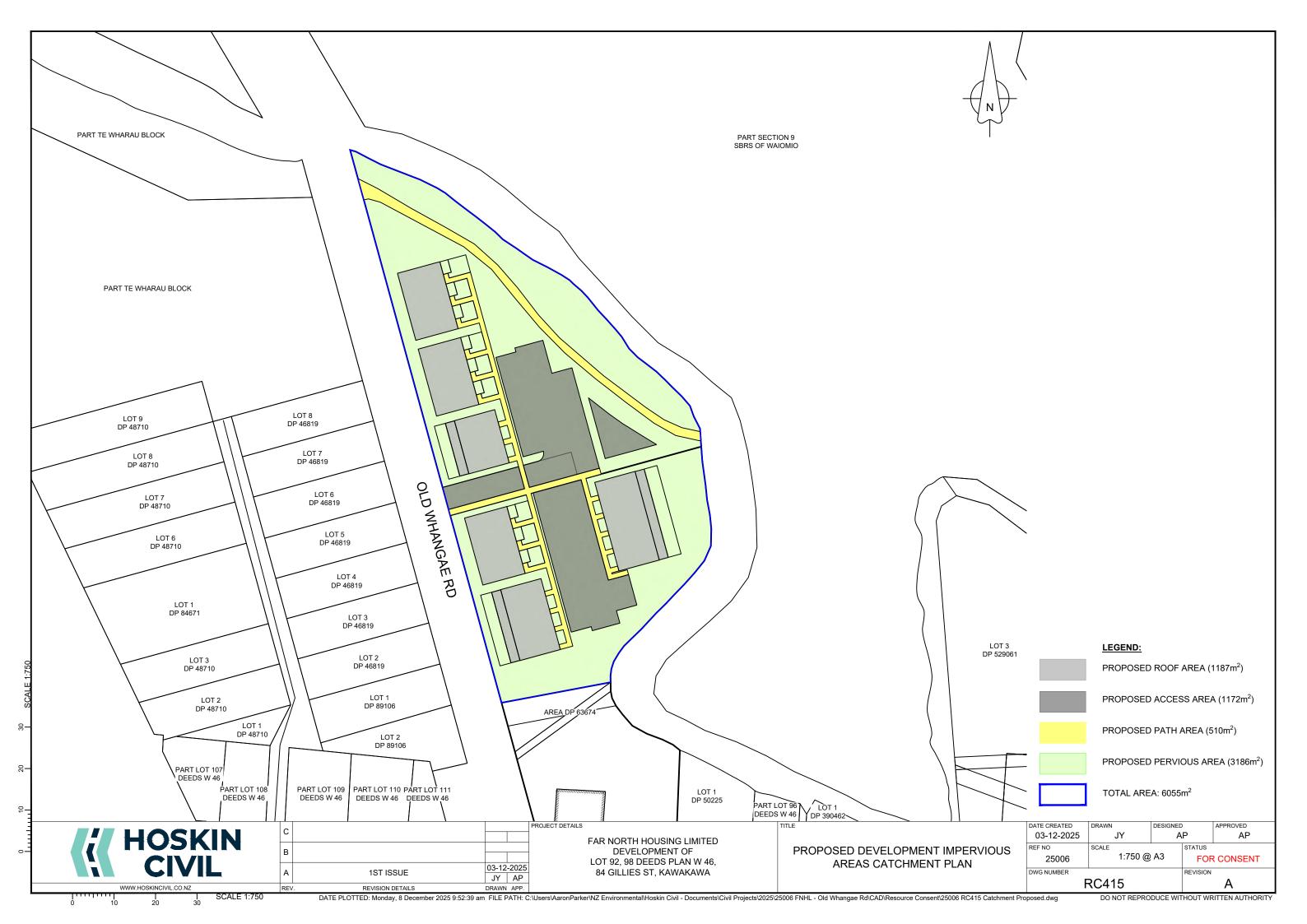


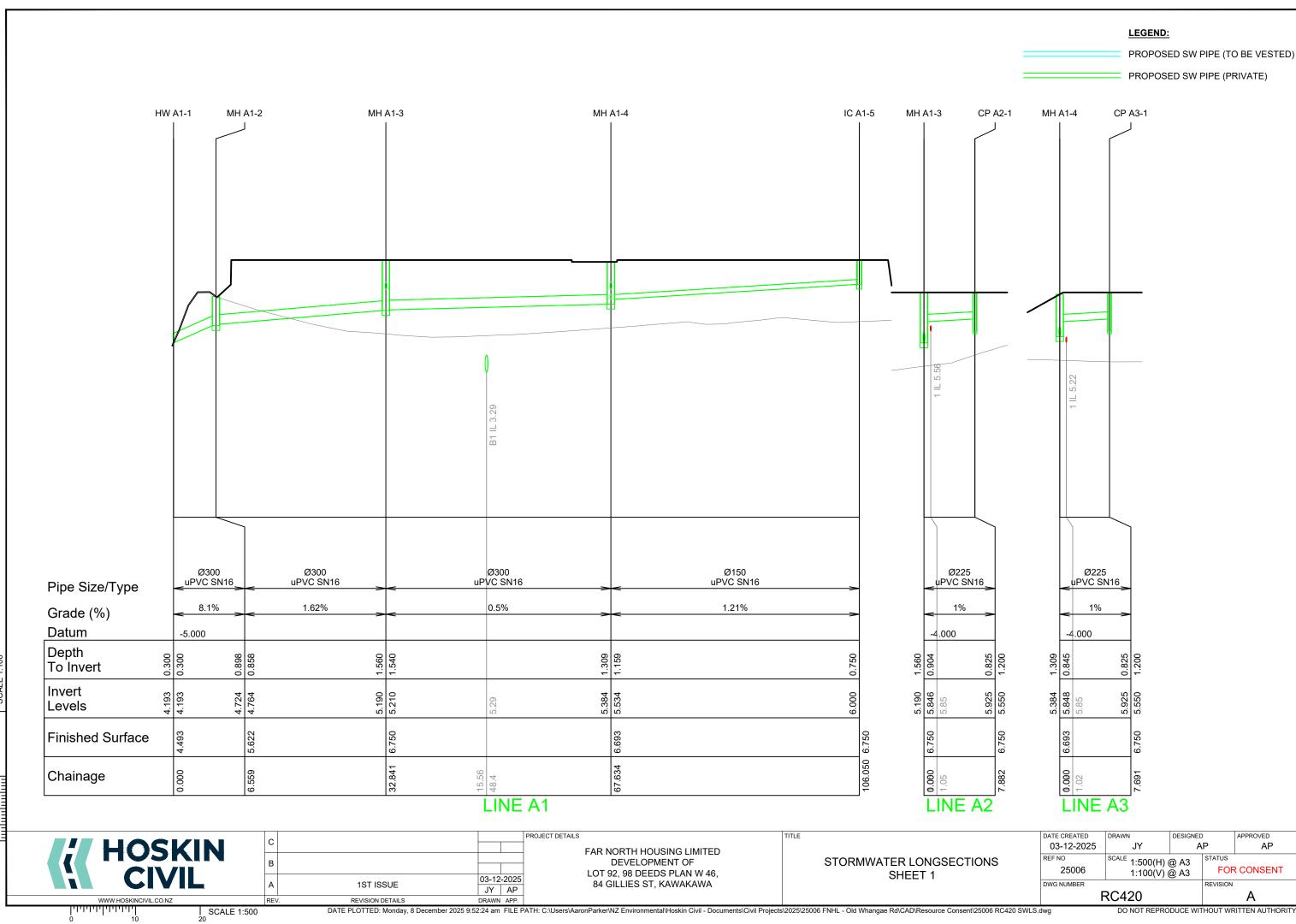


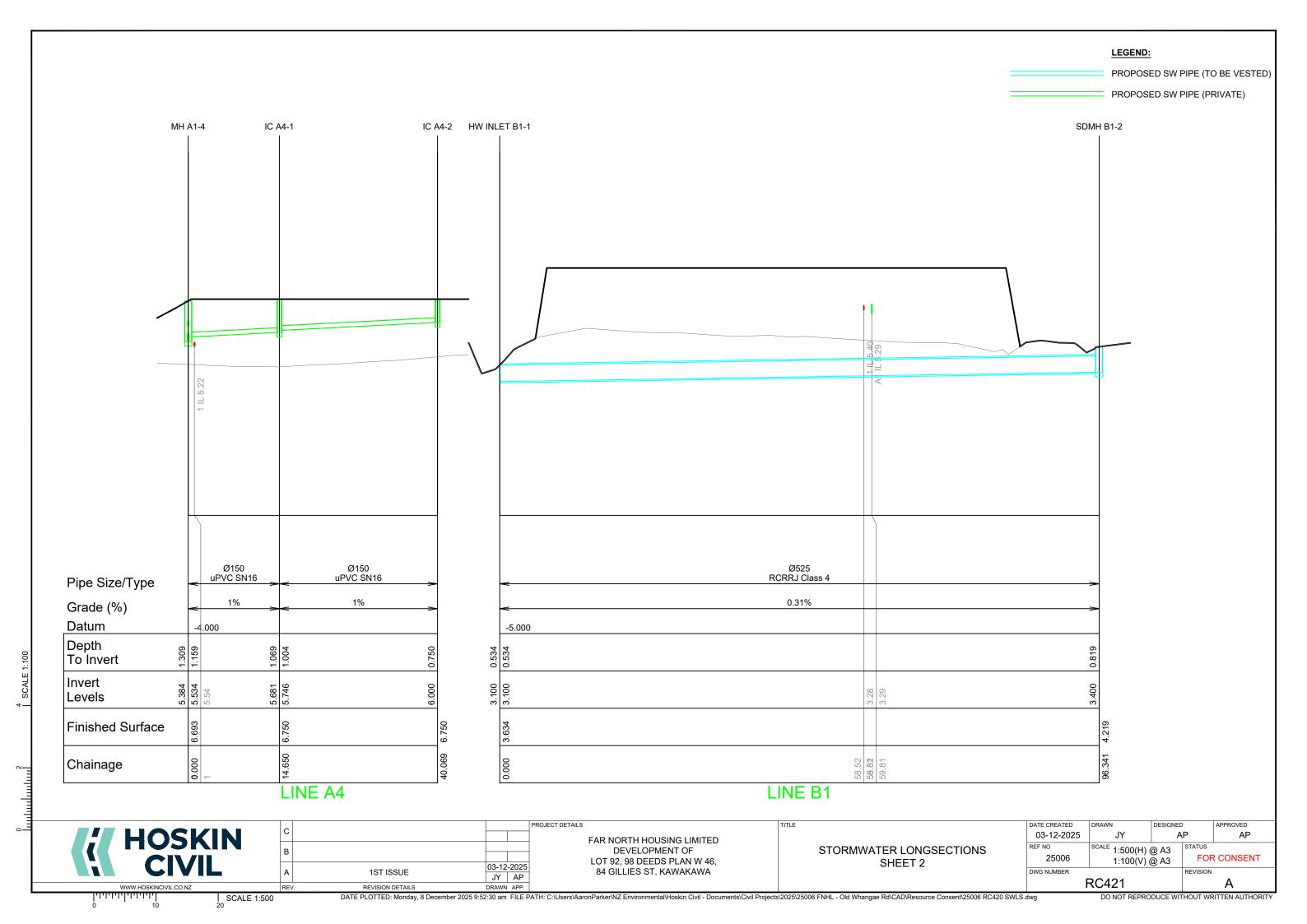




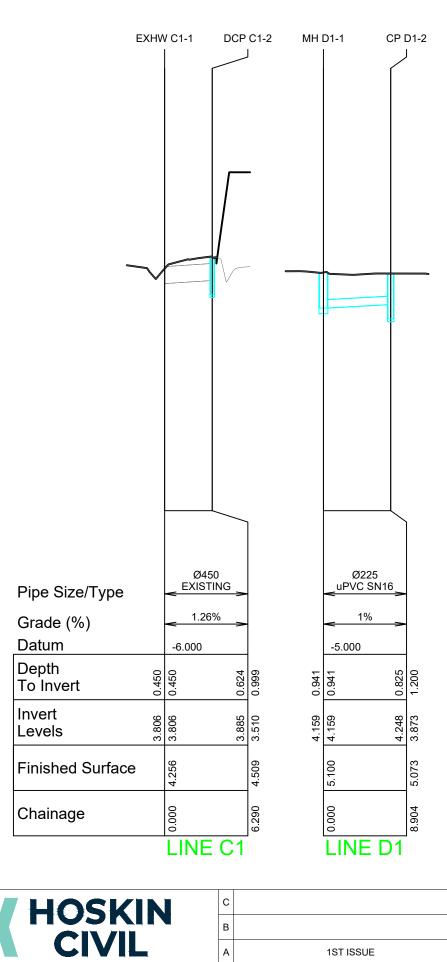








LEGEND: PROPOSED SW PIPE (TO BE VESTED) PROPOSED SW PIPE (PRIVATE)



FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

03-12-2025

JY AP

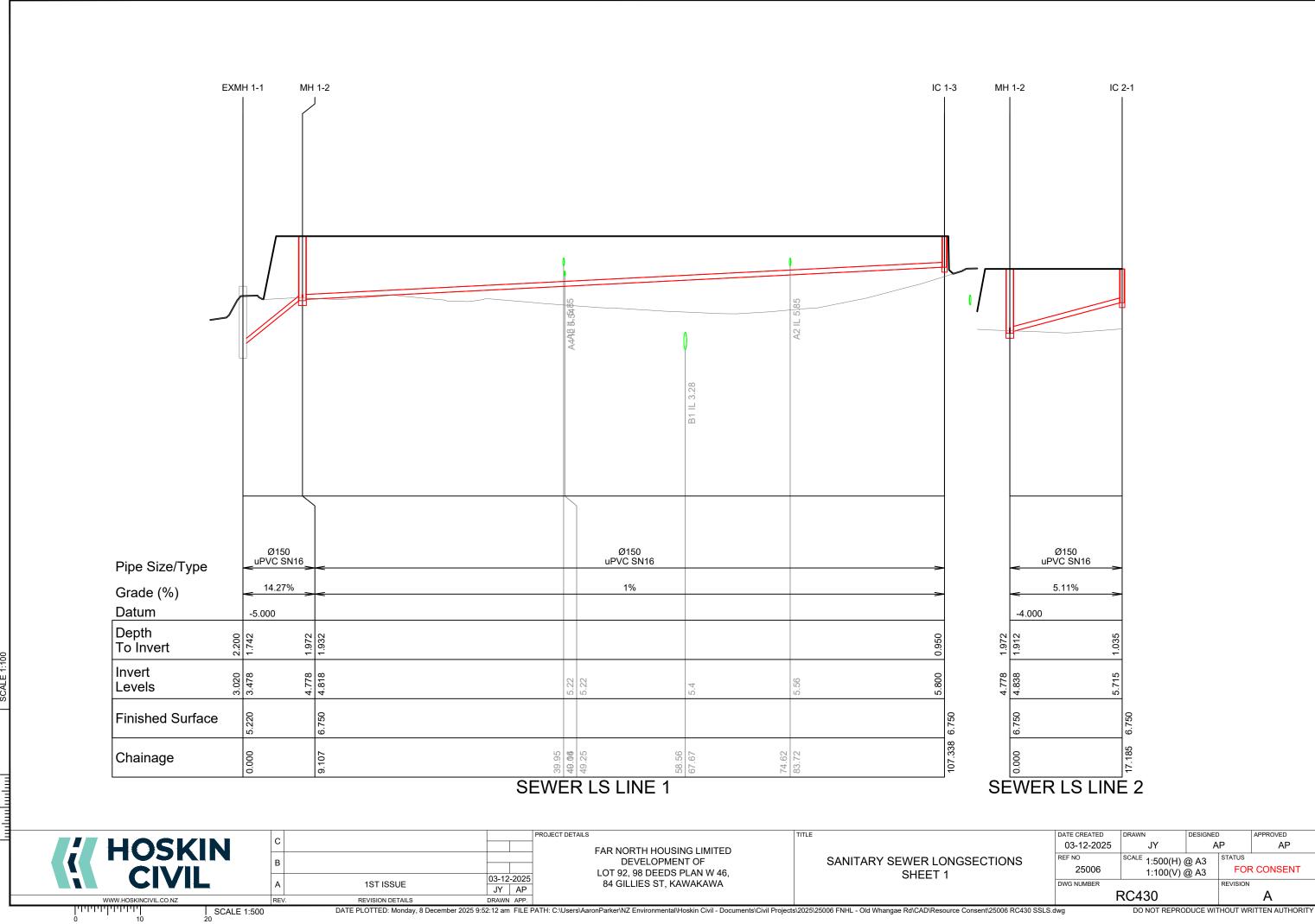
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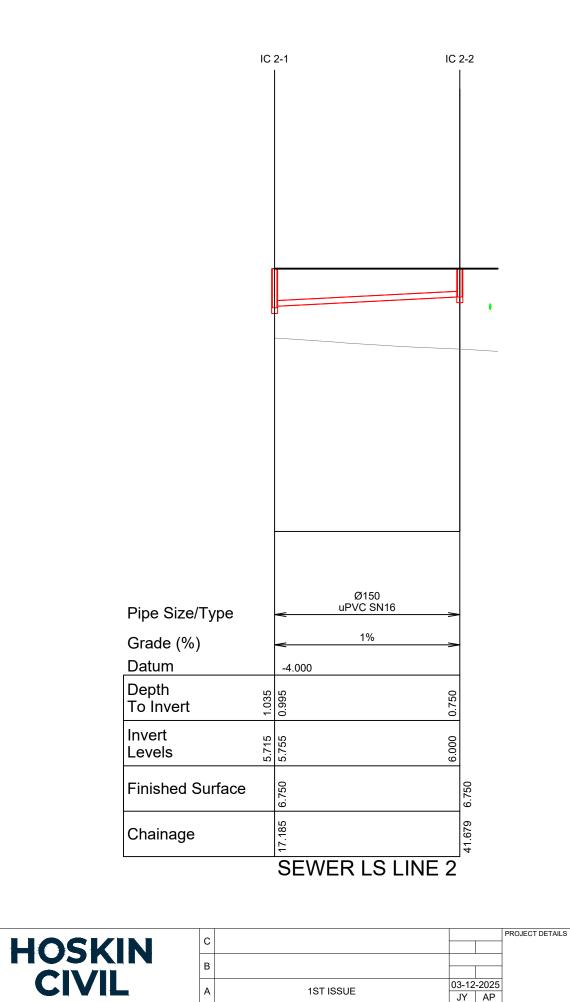
STORMWATER LONGSECTIONS SHEET 3

DATE CREATED 03-12-2025 SCALE 1:500(H) @ A3 1:100(V) @ A3 FOR CONSENT 25006

SCALE 1:500

REVISION DETAILS DATE PLOTTED: Monday, 8 December 2025 9:52:27 am FILE PATH: C:\Users\AaronParker\NZ Environmental\Hoskin Civil - Documents\Civil Projects\2025\25006 FNHL - Old Whangae Rd\CAD\Resource Consent\25006 RC420 SWLS.dwg





DATE CREATED 03-12-2025 SCALE 1:500(H) @ A3 1:100(V) @ A3 SANITARY SEWER LONGSECTIONS FOR CONSENT 25006 SHEET 2 RC431

SCALE 1:500

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03-12-2025

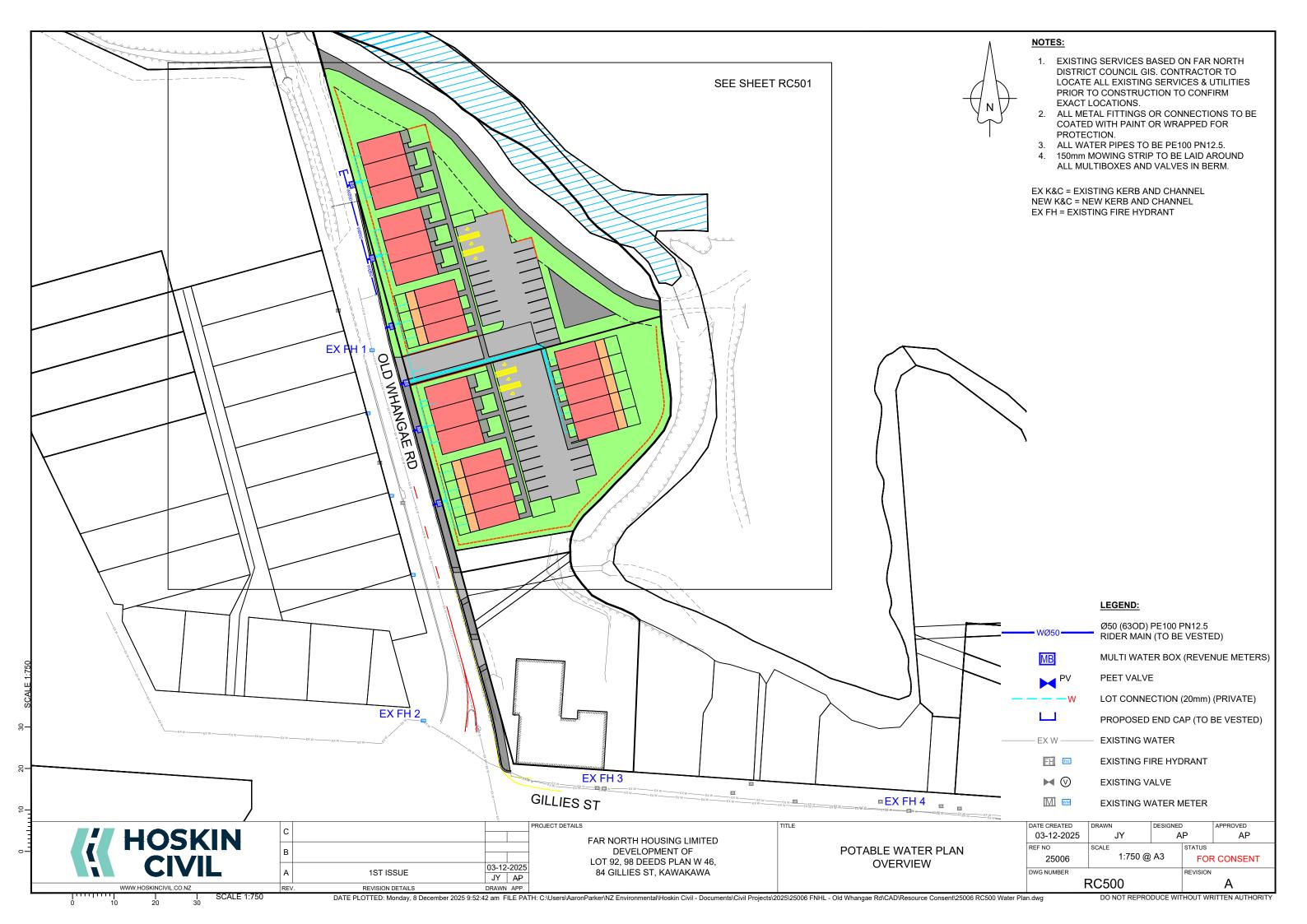
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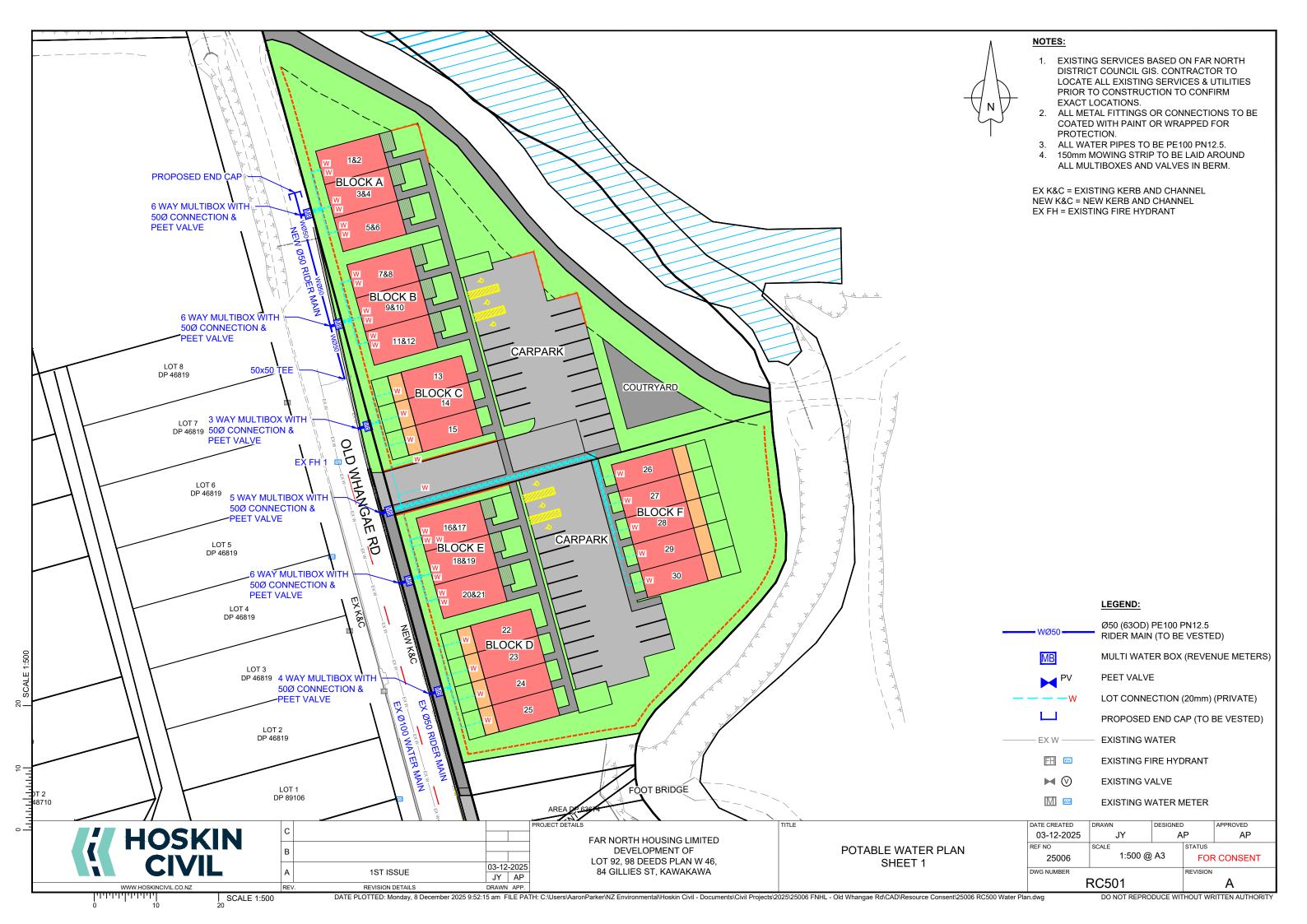
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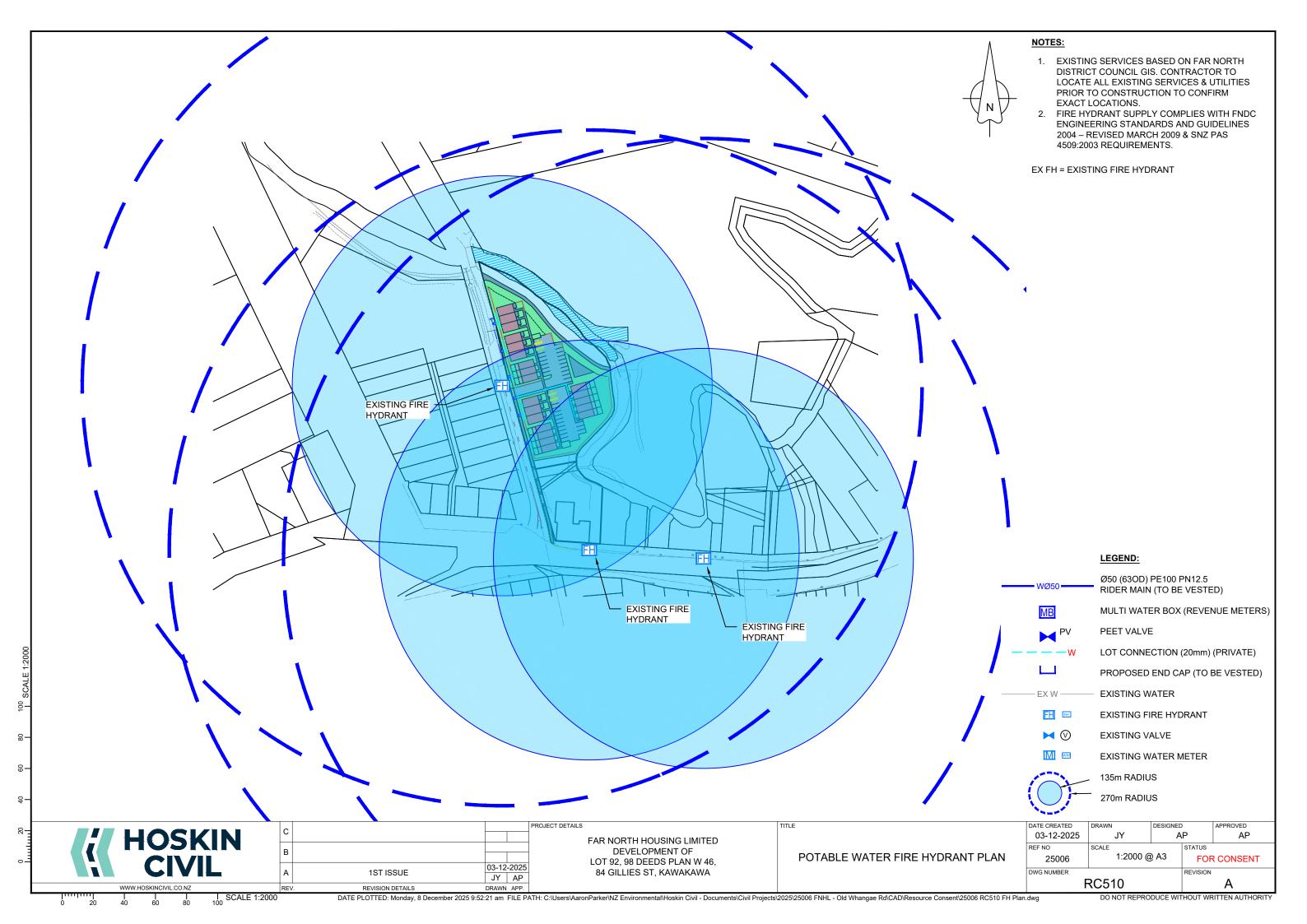
FAR NORTH HOUSING LIMITED

DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46,

84 GILLIES ST, KAWAKAWA







Old Whangae Road Development, Kawakawa – Far North Housing Limited

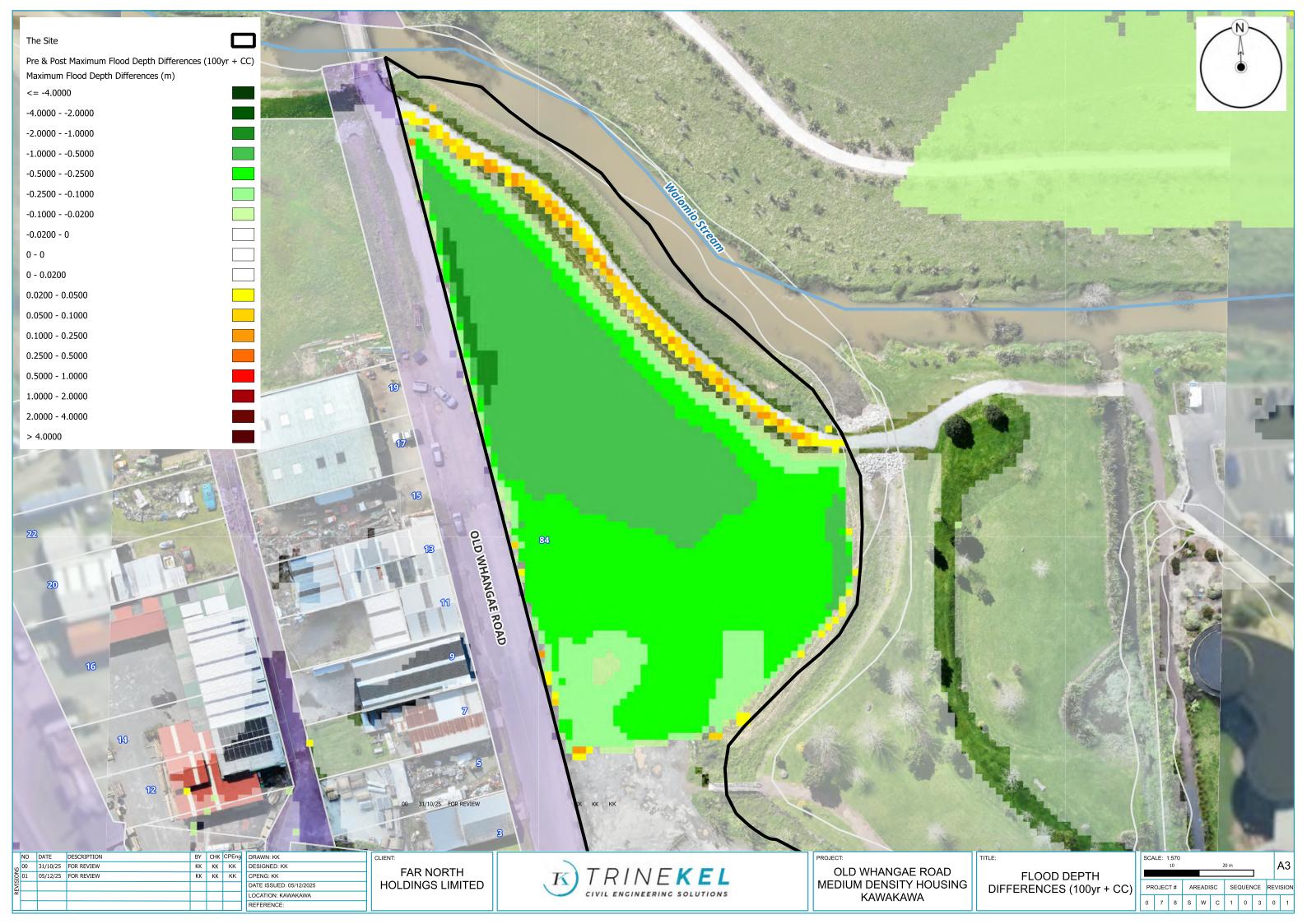
Three Waters Report

## 6.3 Appendix C:

Flood Modelling Maps Outputs









Old Whangae Road Development, Kawakawa – Far North Housing Limited

Three Waters Report

## 6.4 Appendix C:

NRC Flood Level Report (Parcel ID 4991387), providing modelled flood information for the site.

# Flood Level Report



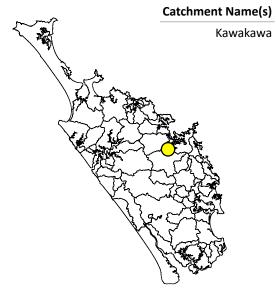


Parcel ID: 4991387

Title: NA523/225

Appellation: Lot 1 DP 63674

Survey Area: 7,588 m<sup>2</sup>



Date Exported: 24/11/2025 Report Reference: 20251118\_135228



#### <u>Useful Flood Information Definitions</u>

**Annual Exceedance Probability (AEP)** - The probability of a flood event of a given size occurring in any one year, usually expressed as a percentage annual chance.

1% AEP - A flood of this size or larger has a 1 in 100 chance or a 1% probability of occurring in any year.

2% AEP - A flood of this size or larger has a 1 in 50 chance or a 2% probability of occurring in any year.

5% AEP - A flood of this size or larger has a 1 in 20 chance or a 5% probability of occurring in any year.

10% AEP - A flood of this size or larger has a 1 in 10 chance or a 10% probability of occurring in any year.

**NZVD2016 - New Zealand Vertical Datum -** The reference level used in our flood models to define ground level. **Flood Levels -** Flood levels are used from our modelled flood level rasters. The flood levels are calculated above NZVD 2016 Datum.

**Climate Change (CC)** - NZCPS (2010) requires that the identification of coastal hazards includes consideration of sea level rise over at least a 100-year planning period. Climate change impacts, such as increased rain intensity, have been included in the flood scenarios. You can read more about the Climate Change forecasts included in each flood model in the technical reports on the NRC website.

Mean high water spring (MHWS) - describes the highest level that spring tides reach, on average.

#### Coastal Flood Hazard Zones (CFHZ)

Coastal flood hazard zones are derived using a range of data including tide gauge analysis, wind and wave data and models, and use empirical calculations to estimate extreme water levels around the coastline. The calculations include projected sea level rise scenarios based on the latest Ministry for the Environment guidance.

**CFHZ 0** Coastal Flood Hazard Zone 0 - area currently susceptible to coastal inundation (flooding by the sea) in a 1-in-100 year storm event

**CFHZ 1** Coastal Flood Hazard Zone 1 - an area susceptible to coastal inundation (flooding by the sea) in a 1-in-50 year storm event, taking into account a projected sea-level rise of 0.6m over the next 50 years **CFHZ 2** Coastal Flood Hazard Zone 2 - an area susceptible to coastal inundation (flooding by the sea) in a 1-in-100 year storm event, taking into account a projected sea-level rise of 1.2m over the next 100 years **CFHZ 3** Coastal Flood Hazard Zone 3 - an area susceptible to coastal inundation (flooding by the sea) in a 1-in-100 year storm event, taking into account a projected sea-level rise of 1.5m over the next 100 years (rapid sea level rise scenario)

### **REGIONWIDE and PRIORITY - RIVER FLOOD HAZARD ZONES (RFHZ)**

River flood hazard zones are created to raise awareness of where flood hazard areas are identified, inform decision-making and to support the minimisation of the impacts of flooding in our region. The river flood hazard zones have been created using an assessment of best current available information, engaging national and international experts in the field, using national standards and guidelines and has been peer reviewed. This will provide a good indication of the areas at potential risk of flooding from a regional perspective. However, flood mapping is a complex process which involves some approximation of the natural features and processes associated with flooding.

River Flood Hazard Zone 1 – 10% AEP flood extent: an area with a 10% chance of flooding annually River Flood Hazard Zone 2 – 2% AEP flood extent: an area with a 2% chance of flooding annually River Flood Hazard Zone 3 – 1% AEP flood extent: an area with a 1% chance of flooding annually with the inclusion of potential Climate Change (CC) impact











Maximum Minimum

Max Min flood levels are for raster extent shown on the map

100 Year + CC

m NZVD

6.28 - 6.48

Parcel







# **Disclaimers**

Our modelling disclaimers are linked below:

https://www.nrc.govt.nz/media/ko2dkgxn/coastal-hazard-maps-disclaimer-june-2017.pdf https://www.nrc.govt.nz/media/cqnnw12y/flood-map-disclaimer-2021.pdf

### Our regionwide modelling reports are linked below:

https://www.nrc.govt.nz/environment/river-flooding-and-coastal-hazards/river-flooding/river-flood-hazard-maps/regionwide-river-catchments-analysis-technical-reports

# **ARE YOU FLOOD READY? Know your risk** Check what potential flood risks and other hazards that may impact your property. The Natural Hazards Portal is a great place to start. It's a 'one-stop-shop' of information related to natural hazards within our region: www.nrc.govt.nz/environment/natural-hazards-portal The Environmental Data Hub provides river level and flow data, as well as warning levels, rainfall data, water quality, and more: www.nrc.govt.nz/environment/environmental-data/environmental-datahub Have a plan Make sure you have an evacuation plan, emergency kit and important phone numbers ready. Check out: https://getready.govt.nz/en/prepared/ for tips on how to get ready. Stay up to date In a civil defence emergency situation, follow the updates on the Northland CDEM Group's Facebook page: www.facebook.com/civildefencenorthland Or follow updates from the embedded feed on the regional council website: www.nrc.govt.nz/civildefence In an emergency





Remember, if life is threatened dial 111 to contact emergency services.





**KAPP, K** CPEng | CMEngNZ | IntPE(NZ) **Senior Civil Engineer** 

8 December 2025

Old Whangae Road Development, Kawakawa - Three Waters Report

Prepared for Far North Housing Limited Hoskin Civil Report: 078-3WR-01\_Rev00

LOCATION 113 Bank Street Whangarei 0110



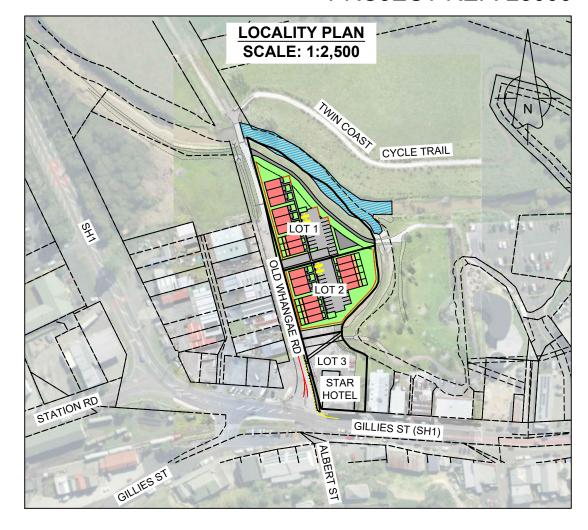


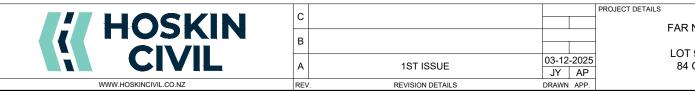
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# CIVIL ENGINEERING DESIGN FOR RESOURCE CONSENT

FAR NORTH HOUSING LTD LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

PROJECT REF: 25006

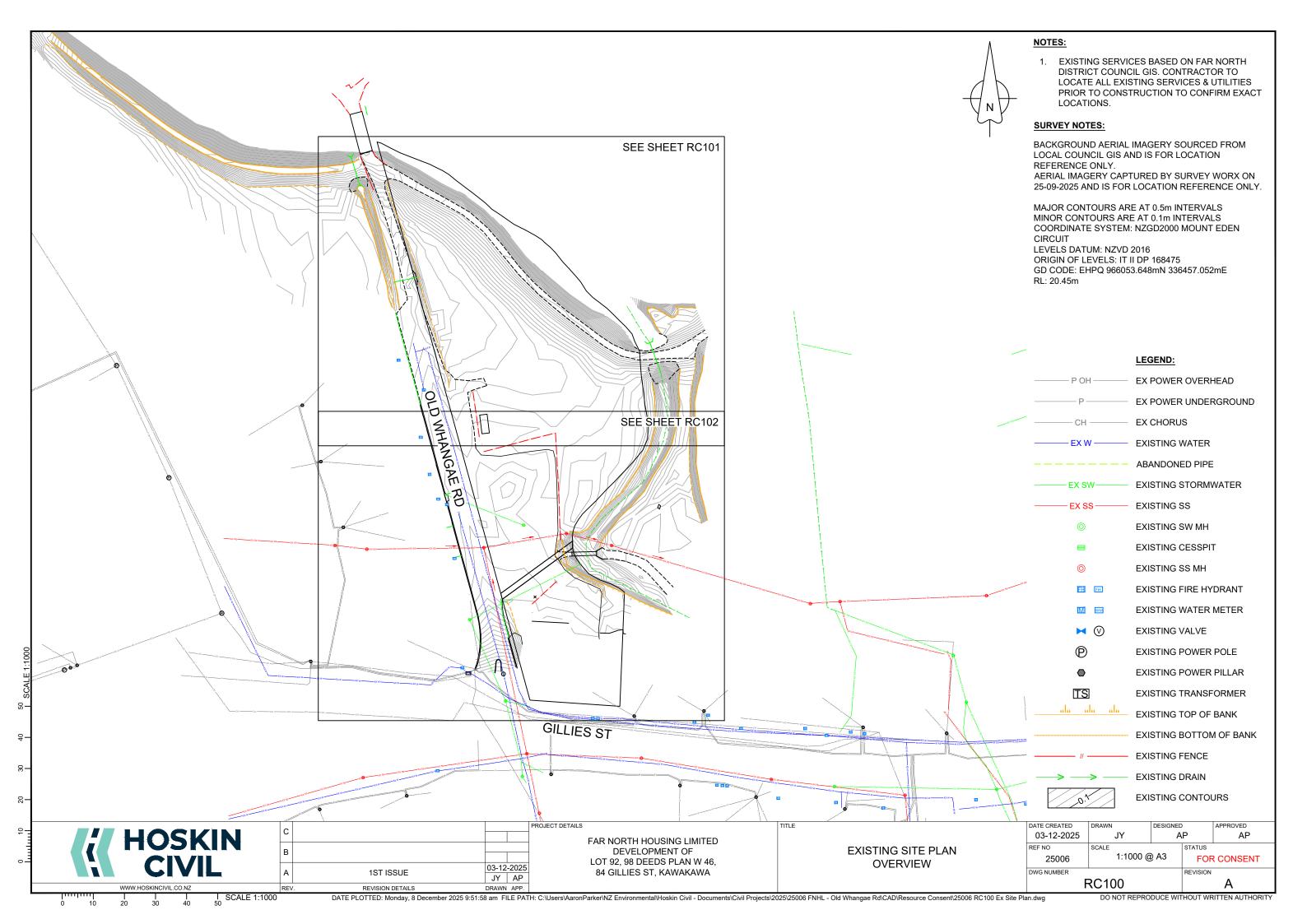


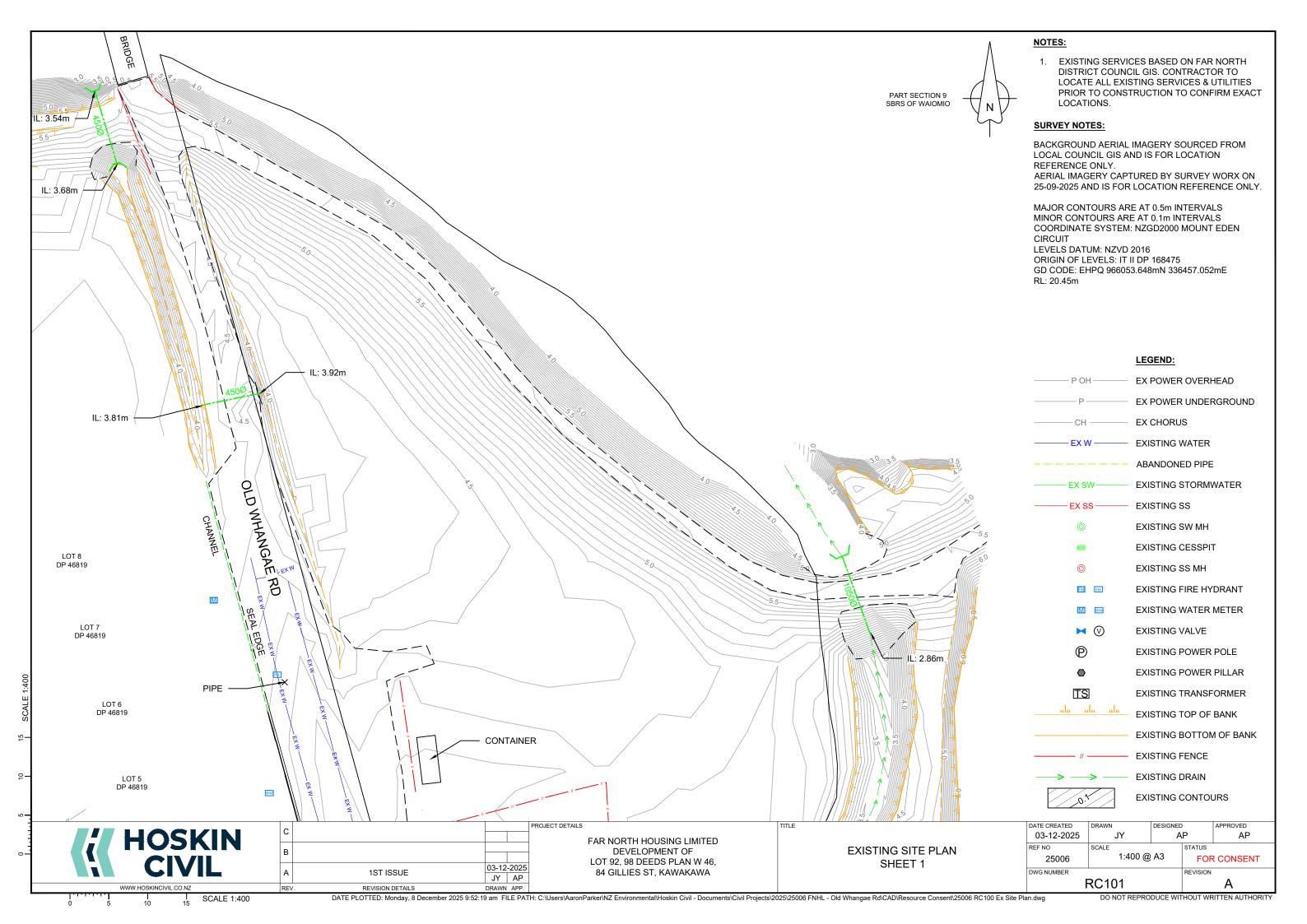


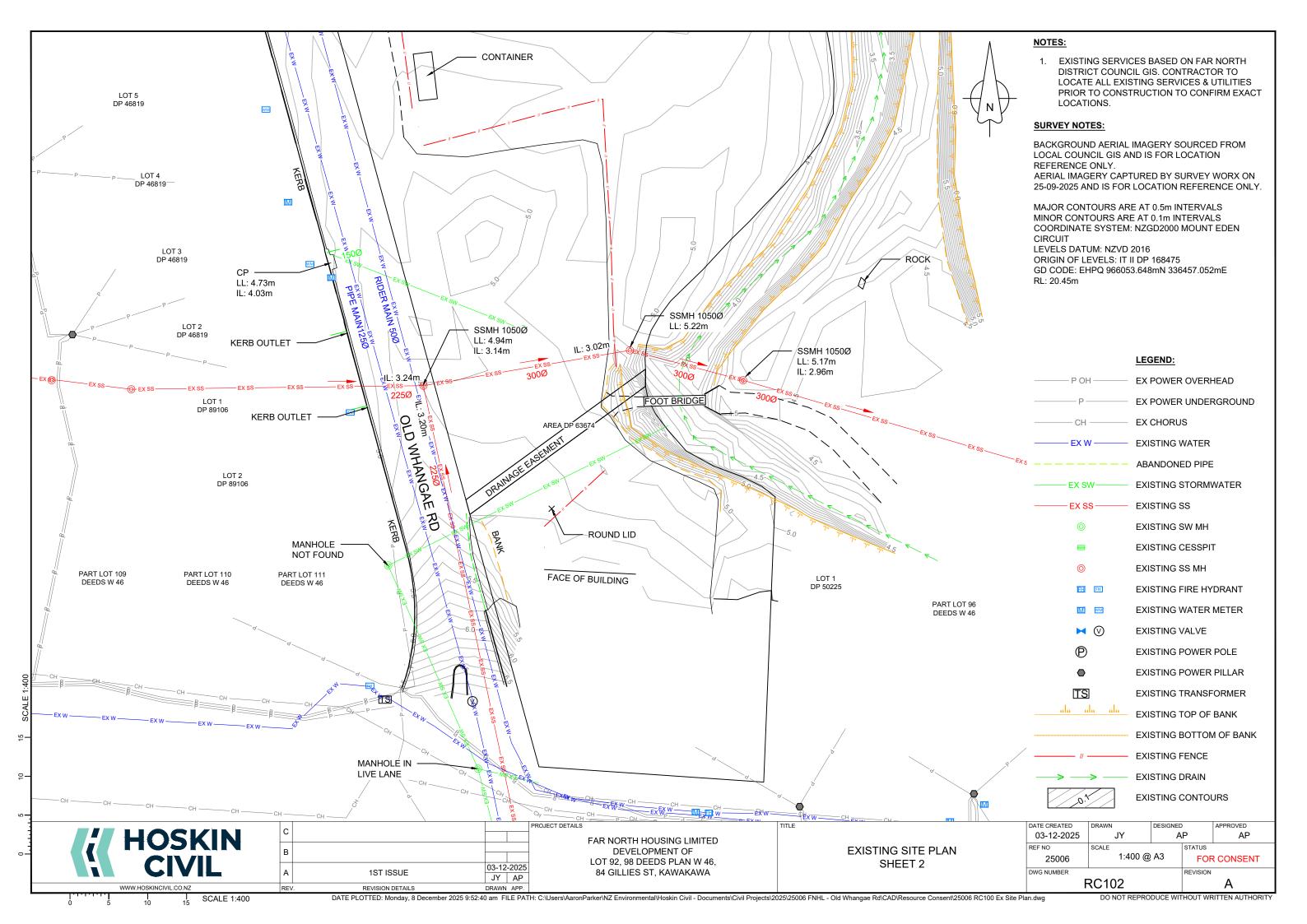
FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

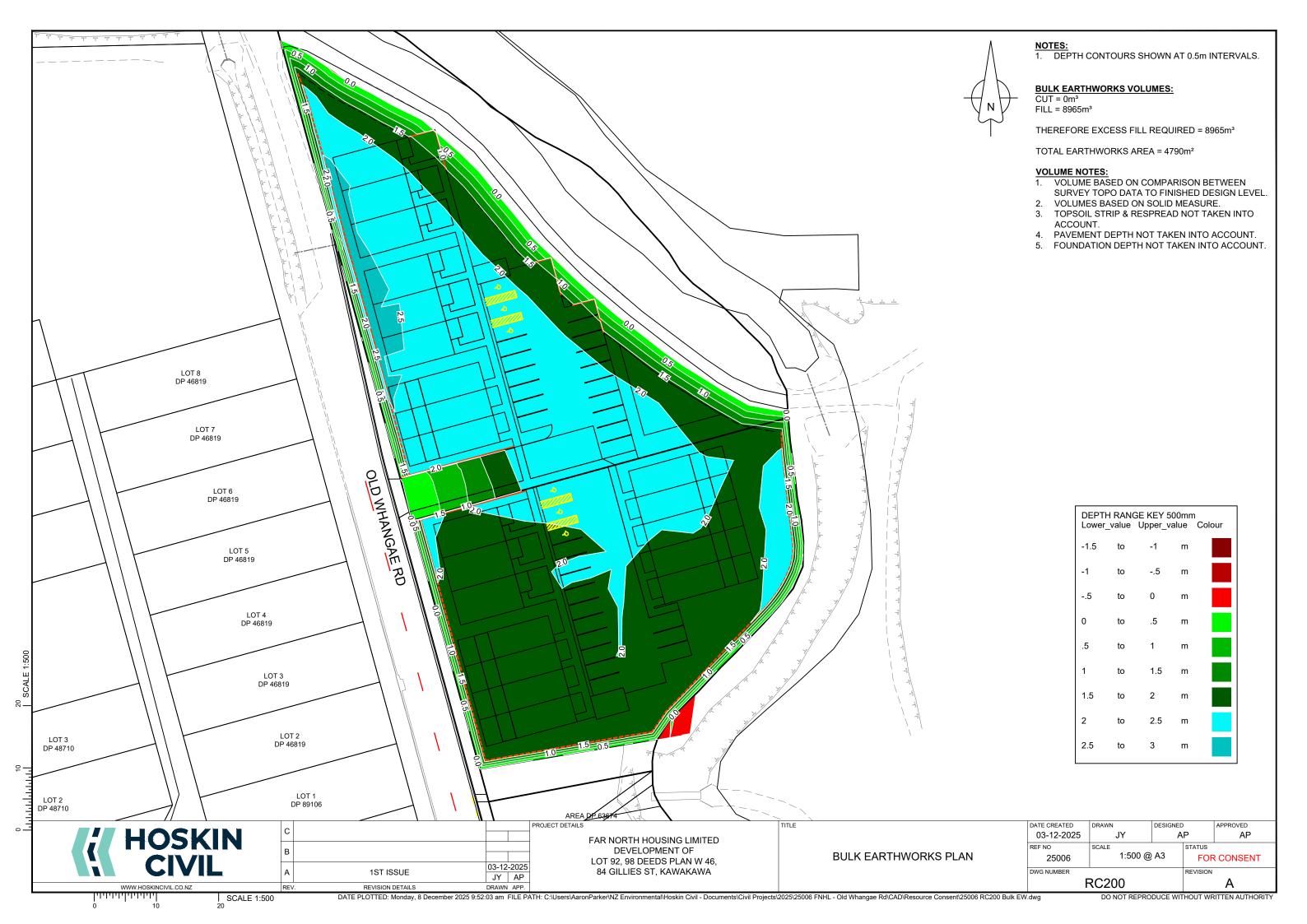
COVER SHEET

50 SCALE 1:2500









# NOTES: DESIGN CONTOURS AT 200mm INTERVALS. EXISTING CONTOURS AT 200mm INTERVALS. EROSION CONTROL - ALL SILT CONTROL MEASURES SHALL BE INSTALLED IN ACCORDANCE WITH GD05 AND PLACED PRIOR TO COMMENCEMENT OF EARTHWORKS. SUCH MEASURES SHALL BE SUBJECT TO FURTHER ADDITIONS AND ALTERATIONS, WHERE CONSIDERED NECESSARY, AS DIRECTED BY THE PROJECT MANAGER OR NRC, DURING THE PROGRESSION OF WORKS. IT IS ADVISED TO CONTACT NRC PRIOR TO COMMENCEMENT OF EARTHWORKS, AFTER INSTALLATION OF EROSION AND SEDIMENT CONTROL DEVICES TO ENSURE THEY HAVE BEEN INSTALLED TO THE SATISFACTION OF NRC. LEGEND: ANY LOCATIONS EARTH BUND IS NOT SUITABLE (DUE TO SPACE **EXISTING CONTOURS** LIMITATIONS), SILT FENCE TO BE INSTALLED PROPOSED CONTOURS — EXTENT OF EARTHWORKS (4790m²) SILT FENCE EARTH BUND DECANT OVERLAND FLOWPATH WITH CATCHMENT AREA OF 2260m<sup>2</sup> SITE TO BE SPLIT INTO EARTH BUND TWO CATCHMENTS OF (DISCHARGE INTO LESS THAN 3000m<sup>2</sup> EXISTING CULVERT) EARTH BUND DECANT EARTH BUND DECANT WITH CATCHMENT STABILISED AREA OF 2440m<sup>2</sup> CONSTRUCTION ENTRANCE OLD WHANGAEF 召 HOSKIN CIVIL 03-12-2025 FAR NORTH HOUSING LIMITED DEVELOPMENT OF **EROSION & SEDIMENT CONTROL PLAN** 1:750 @ A3 25006 FOR CONSENT LOT 92, 98 DEEDS PLAN W 46, 03-12-2025 1ST ISSUE 84 GILLIES ST, KAWAKAWA JY AP RC210 REVISION DETAILS DRAWN APP. DO NOT REPRODUCE WITHOUT WRITTEN AUTHORITY DATE PLOTTED: Monday, 8 December 2025 9:52:36 am FILE PATH: C:\Users\AaronParker\NZ Environmental\Hoskin Civil - Documents\Civil Projects\2025\25006 FNHL - Old Whangae Rd\CAD\Resource Consent\25006 RC210 ESCP.dwg

# STABILISED CONSTRUCTION ENTRANCE SPECIFICATIONS:

#### **APPLICATION**

USE A STABILISED CONSTRUCTION ENTRANCE AT ALL POINTS OF CONSTRUCTION SITE INGRESS AND EGRESS WITH A CONSTRUCTION PLAN LIMITING TRAFFIC TO THESE ENTRANCES ONLY. THEY ARE PARTICULARLY USEFUL ON SMALL CONSTRUCTION SITES BUT CAN BE UTILISED FOR ALL PROJECTS.

#### DESIGN:

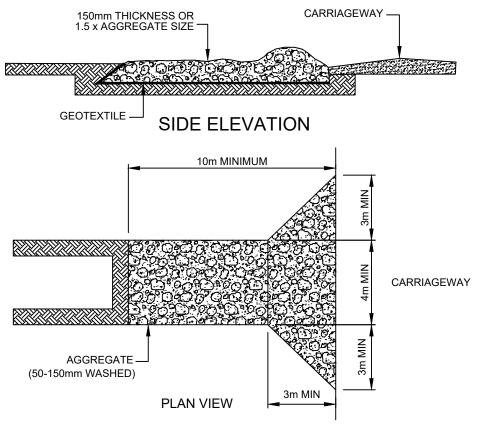
CLEAR THE ENTRANCE AND EXIT AREA OF ALL VEGETATION, ROOTS AND OTHER UNSUITABLE MATERIAL AND PROPERLY GRADE IT.

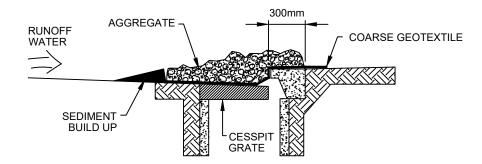
- 1. LAY WOVEN GEOTEXTILE; PIN DOWN EDGES AND OVERLAP JOINTS.
- 2. PROVIDE DRAINAGE TO CARRY RUNOFF FROM THE STABILISED CONSTRUCTION ENTRANCE TO A SEDIMENT CONTROL MEASURE.
- 3. PLACE AGGREGATE TO THE SPECIFICATIONS BELOW AND SMOOTH IT.
- 4. STABILISED CONSTRUCTION ENTRANCE AGGREGATE SPECIFICATIONS:

AGGREGATE SIZE	5-150mm WASHED AGGREGATE
THICKNESS	150mm MINIMUM OR 1.5 X AGGREGATE SIZE
LENGTH	10m MINIMUM LENGTH RECOMMENDED
WIDTH	4m MINIMUM

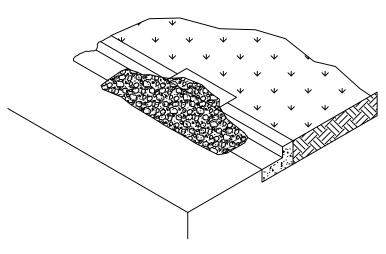
#### MAINTENANCE

- MAINTAIN THE STABILISED CONSTRUCTION ENTRANCE IN A CONDITION TO PREVENT SEDIMENT FROM LEAVING THE CONSTRUCTION SITE. AFTER EACH RAINFALL INSPECT ANY STRUCTURE USED TO TRAP SEDIMENT FROM THE STABILISED CONSTRUCTION ENTRANCE AND CLEAN OUT AS NECESSARY.
- 2. WHEN WHEEL WASHING IS ALSO REQUIRED, ENSURE THIS IS DONE ON AN AREA STABILISED WITH AGGREGATE WHICH DRAINS TO AN APPROVED SEDIMENT RETENTION FACILITY.





# **CROSS SECTION**



STORMWATER INLET PROTECTION
- FILTER MEDIA DESIGN

# STABILISED CONSTRUCTION ENTRANCE

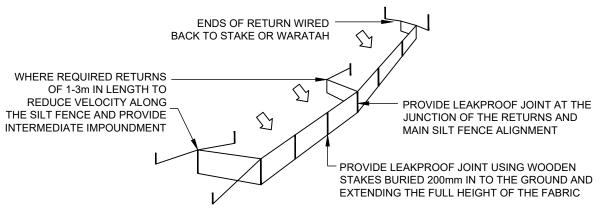


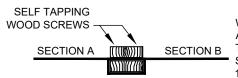
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FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

EROSION & SEDIMENT CONTROL DETAILS SHEET 1

| DATE CREATED | DRAWN | DESIGNED | APPROVED | APPROVED





WRAP BOTH ENDS OF THE FABRIC AROUND ONE STAKE AND CLAMP THE OTHER STAKE TO IT USING SELF TAPPING WOOD SCREWS AT 150mm SPACINGS

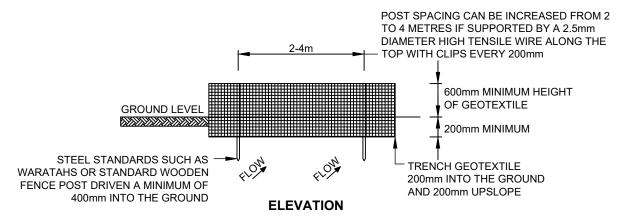
### STANDARD FABRIC JOINT

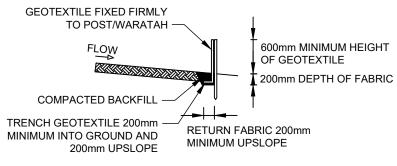
#### SILT FENCE DESIGN CRITERIA:

SLOPE STEEPNESS %	SLOPE LENGTH (m) (MAX)	SPACING OF RETURNS (m)		
< 2%	N/A	UNLIMITED		
2-10%	40	60		
10-20%	30	50		
20-33%	20	40		
33-50%	15	30		
>50%	6	20		

GRAB TENSILE STRENGTH: TENSILE MODULUS: APPARENT OPENING SIZE: >440N (ASTM D4632) 0.140 pa (MINIMUM) 0.1-0.5mm (ASTM D4751)

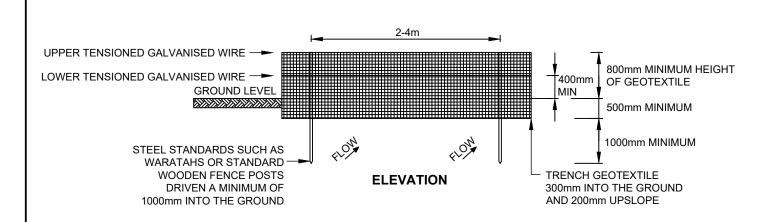
### SILT FENCE WITH RETURNS AND SUPPORT WIRE

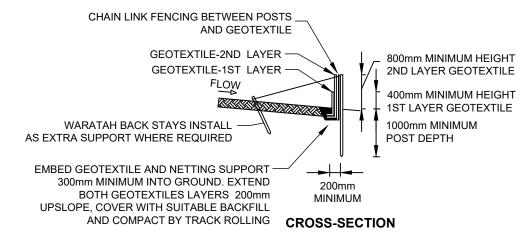




#### **CROSS-SECTION**

# SILT FENCE CONSTRUCTION





# SUPER SILT FENCE DESIGN CRITERIA:

SLOPE LENGTH (m) (MAX)	SPACING OF RETURNS (m)
UNLIMITED	60
60	50
30	40
30	30
15	20
	UNLIMITED 60 30 30

# SUPER SILT FENCE CONSTRUCTION



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FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

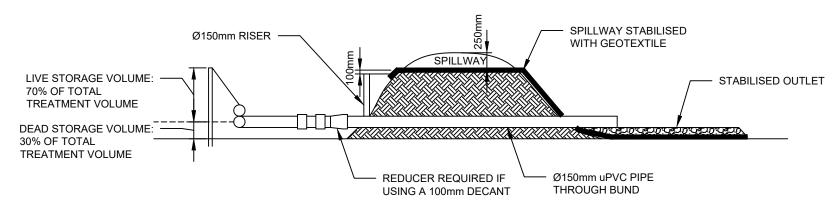
EROSION & SEDIMENT CONTROL DETAILS SHEET 2

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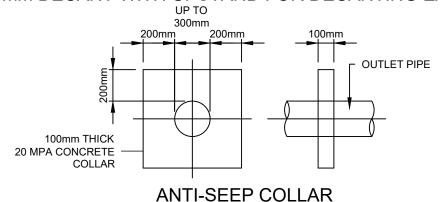
# **DECANTING EARTH BUND**

NOTE: THE 100mm DIAMETER PVC PIPE UPSTAND IS ONLY REQUIRED WHERE THE 2m WIDE EMERGENCY SPILLWAY DISCHARGES TO VULNERABLE AREA OR WHERE THE DISCHARGE IS REQUIRED TO BE PIPED TO A SAFE OUTFALL SUCH AS A STORMWATER MANHOLE. IF THE UPSTAND IS NOT REQUIRED THE DECANT CAN BE CONNECTED DIRECT TO A 40mm DIAMETER OUTFALL PIPE AND THE TREATMENT VOLUME IS MEASURED TO THE INVERT OF THE EMERGENCY SPILLWAY.

NOTE: THE DECANT HAS A 40mm DIAMETER PVC PIPE WITH A 1.3m LONG ARM (INCLUDING FLEXIBLE JOINT), A 0.5m LONG DECANT AND 20 x 10mm DIAMETER EQUALLY SPACED HOLES POSITIONED HORIZONTALLY AT 10 AND 2 OCLOCK

0.5m LONG 100mm DIAMETER PVC PIPE FLOAT WITH STANDARD 100mm END CAPS. THE FLOAT IS STRAPPED TO THE 40mm DIAMETER PVC DECANT PIPE WITH STAINLESS STEEL STRAPS OR ZIP TIES. NYLON CORD TIES TO SUSPEND DECANT FROM WARATAHS AT DECANT AND FLOAT CORRECT HEIGHT STANDARD 40mm **END CAPS (GLUED)** 100mm DIAMETER PVC PIPE UPSTAND WITH THE TOP POSITIONED 100mm BELOW STANDARD 40mm THE LEVEL OF THE EMERGENCY SPILLWAY. TEE JOINT (GLUED) THE TREATMENT VOLUME IS TO BE MEASURED TO THE TOP OF THE UPSTAND. FLEXIBLE RUBBER/NEOPRENE JOINT (SUCH AS PLUMBQWIK) HOSE CLAMPED FOR EASE OF REUSE JOIN SHOULD - 100mm TO 40mm REDUCER FITTING TO BE GLUED BE MADE USING PK SCREWS AND CONSTRUCTION TAPE -STANDARD 100mm TEE JOINT (GLUED)

# 40mm DECANT WITH UPSTAND FOR DECANTING EARTH BUND





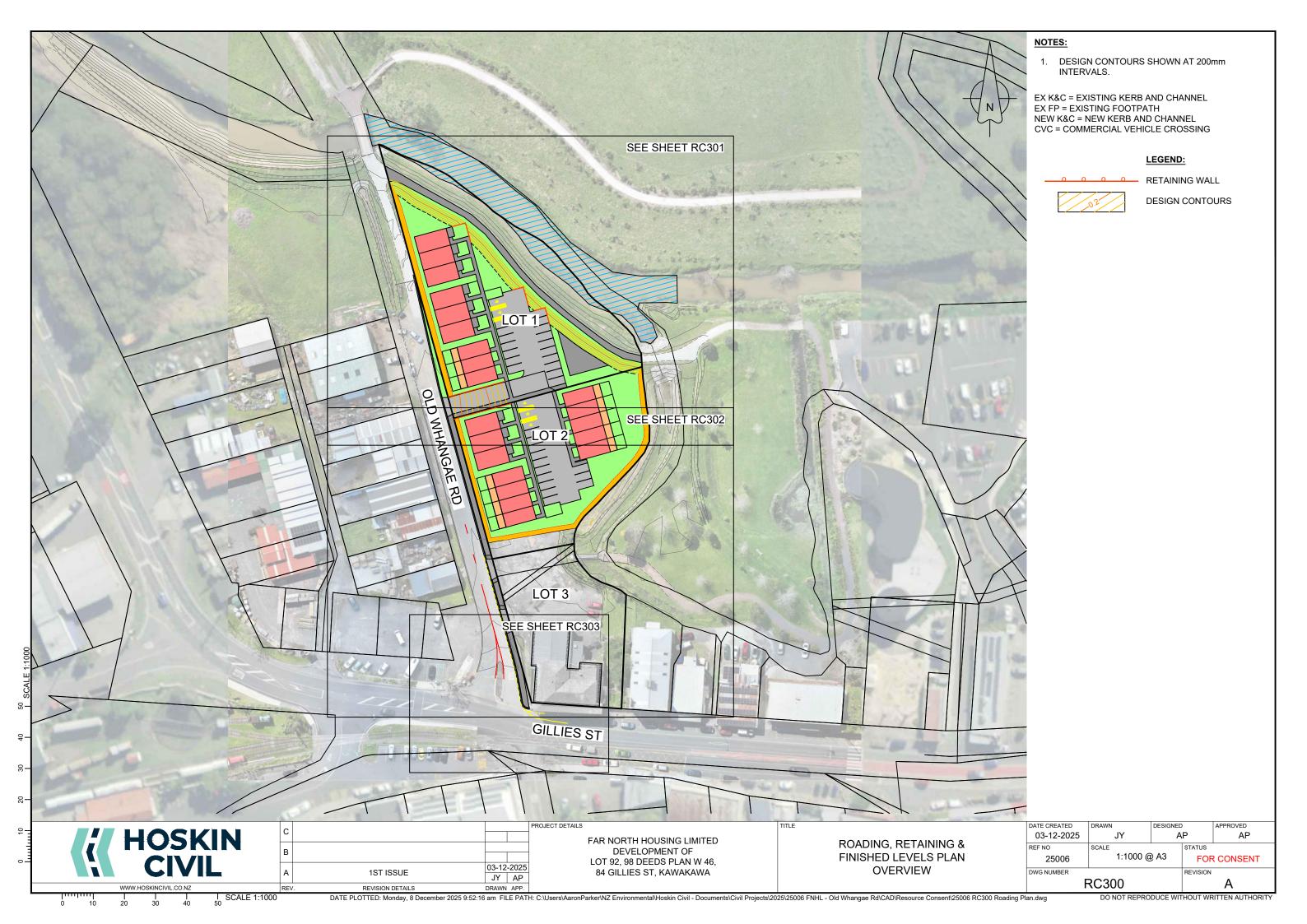
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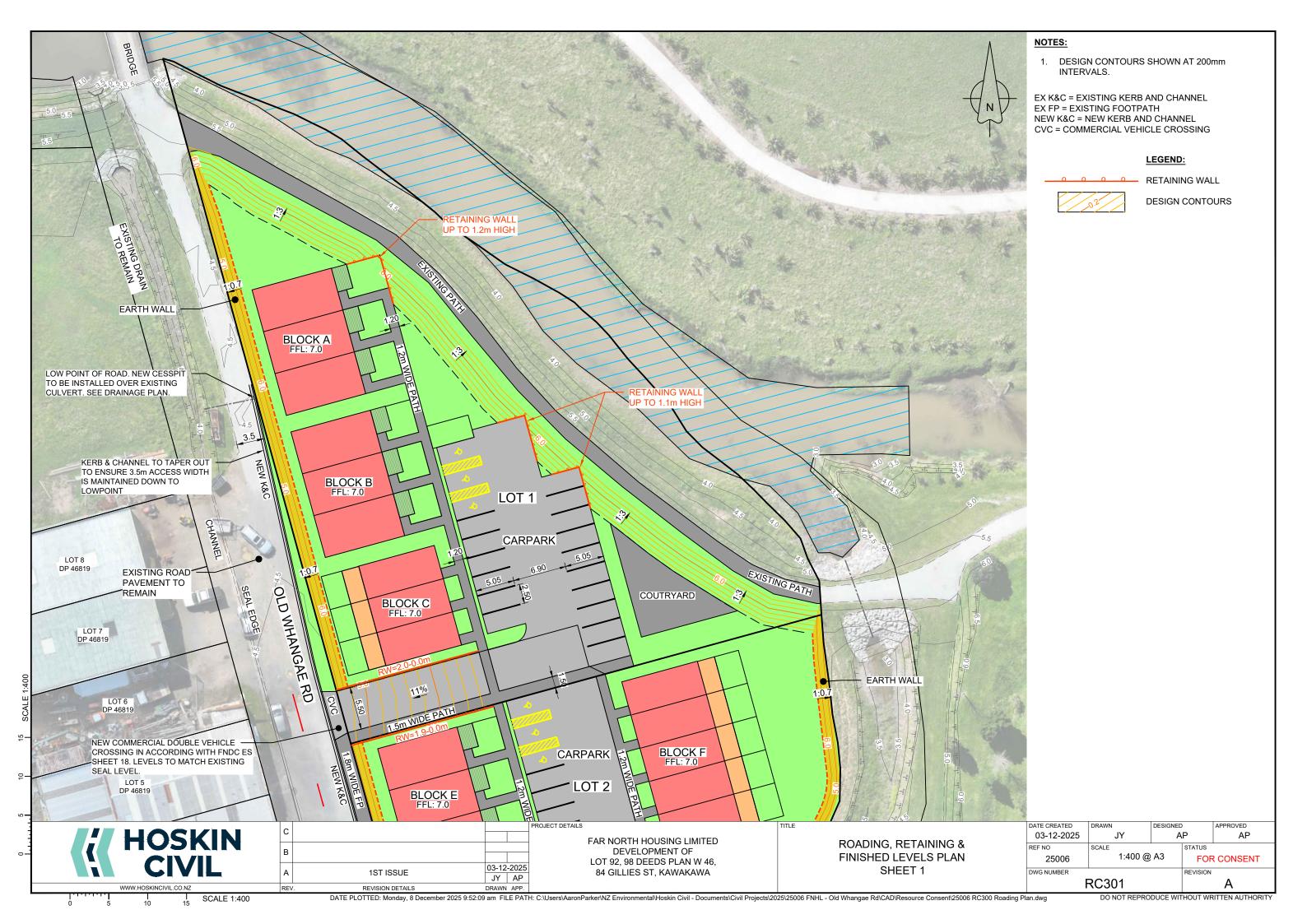
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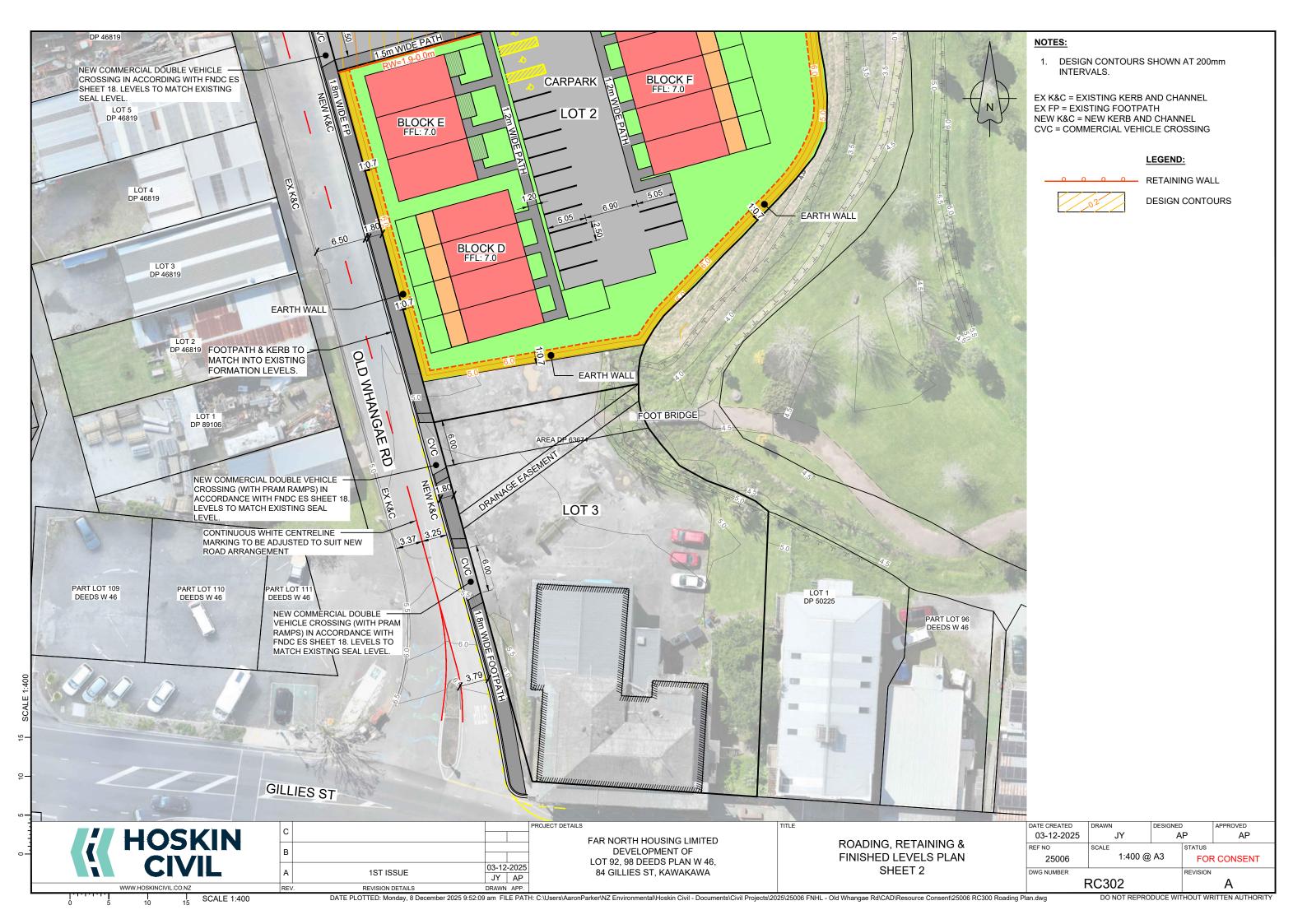
FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

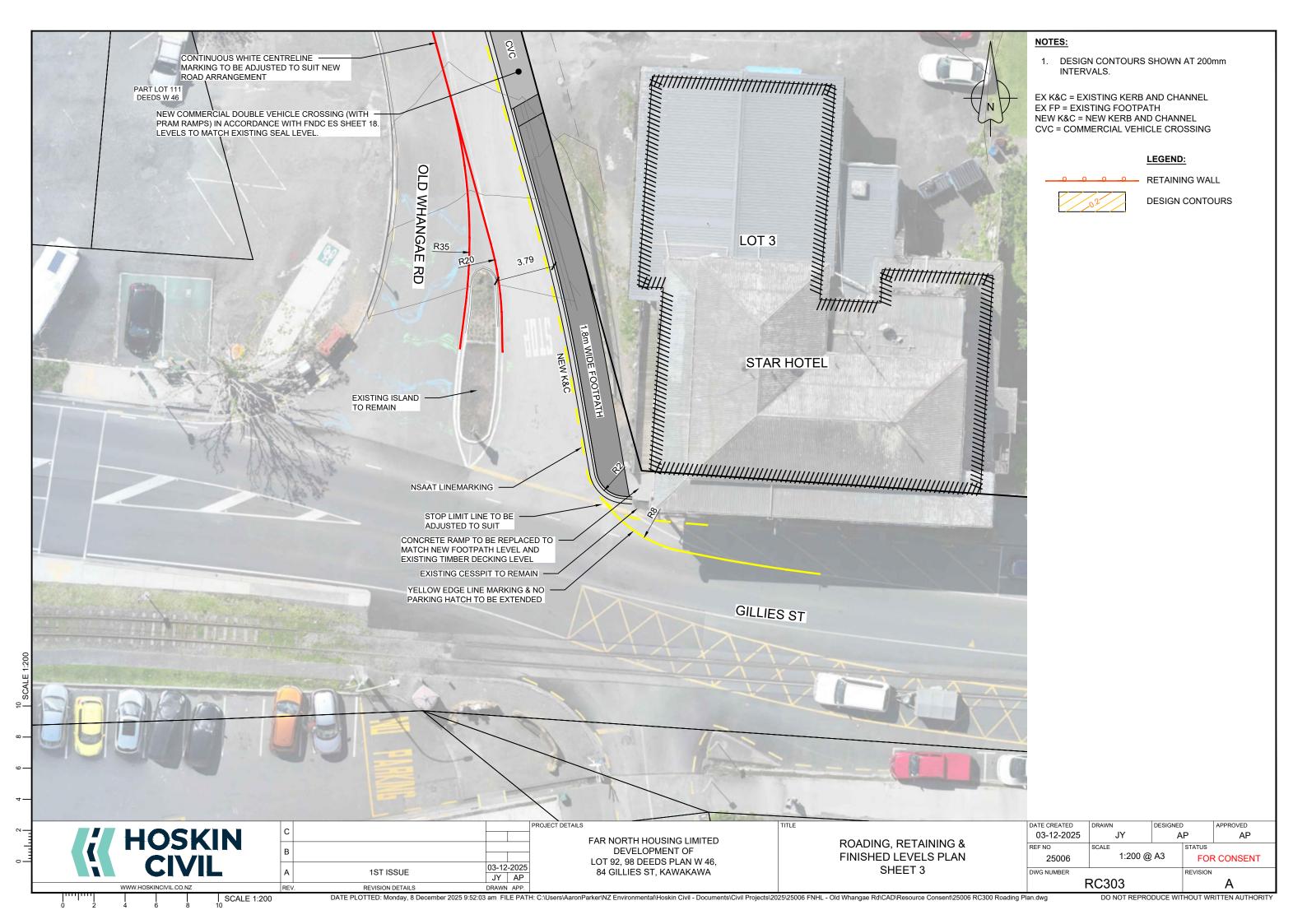
**EROSION & SEDIMENT CONTROL DETAILS** SHEET 3

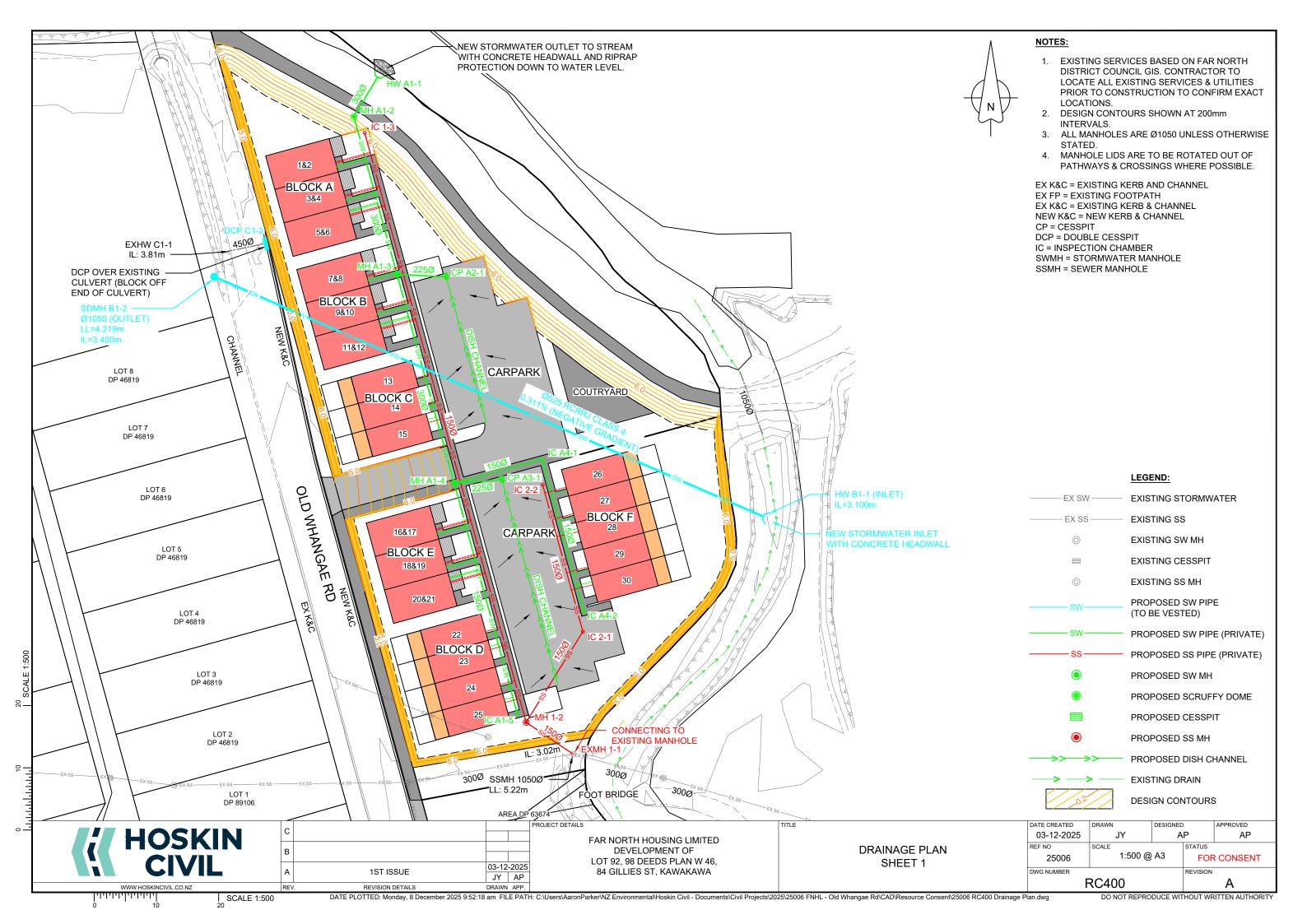
03-12-2025 JΥ NTS @ A3 25006 FOR CONSENT RC222

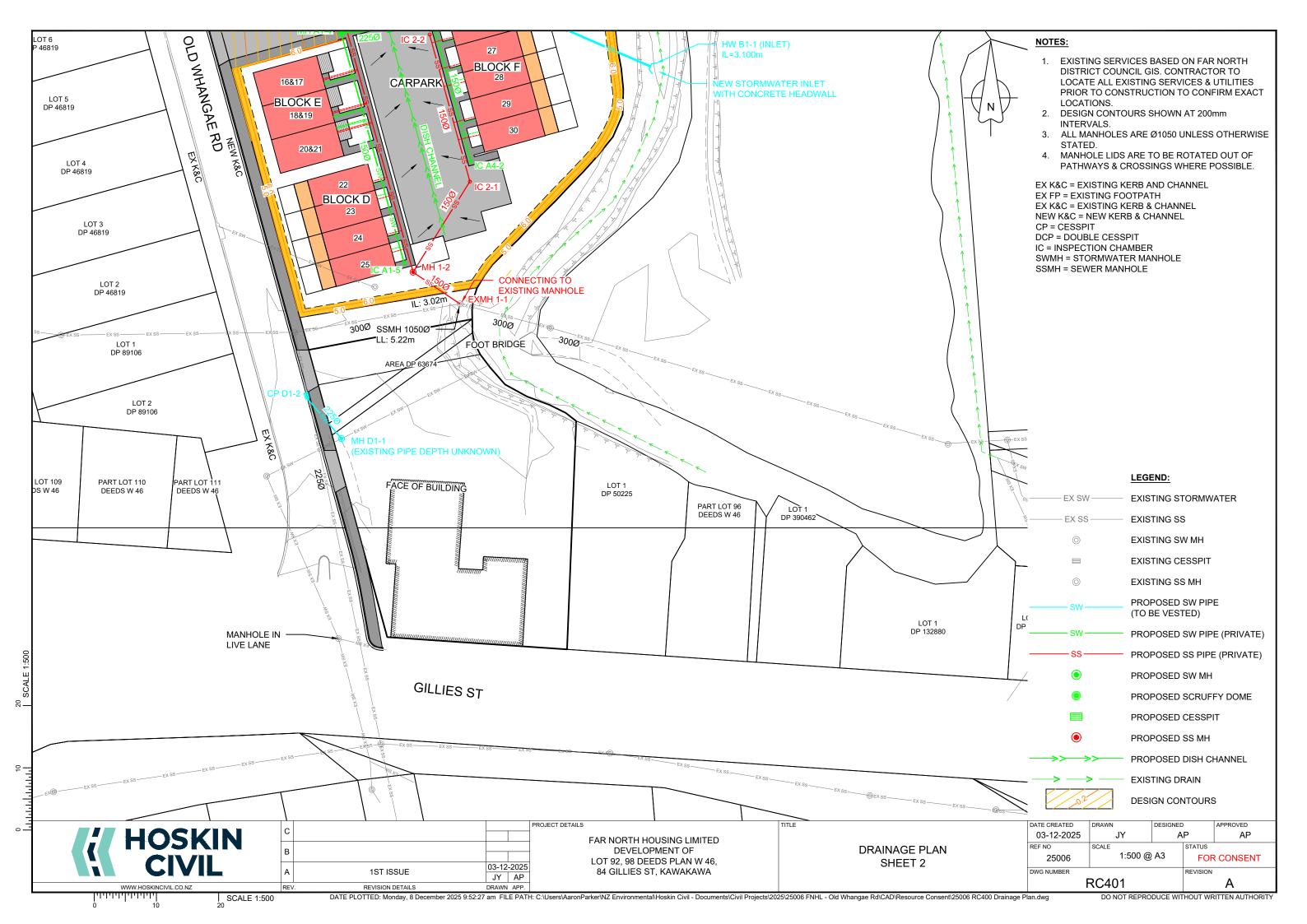




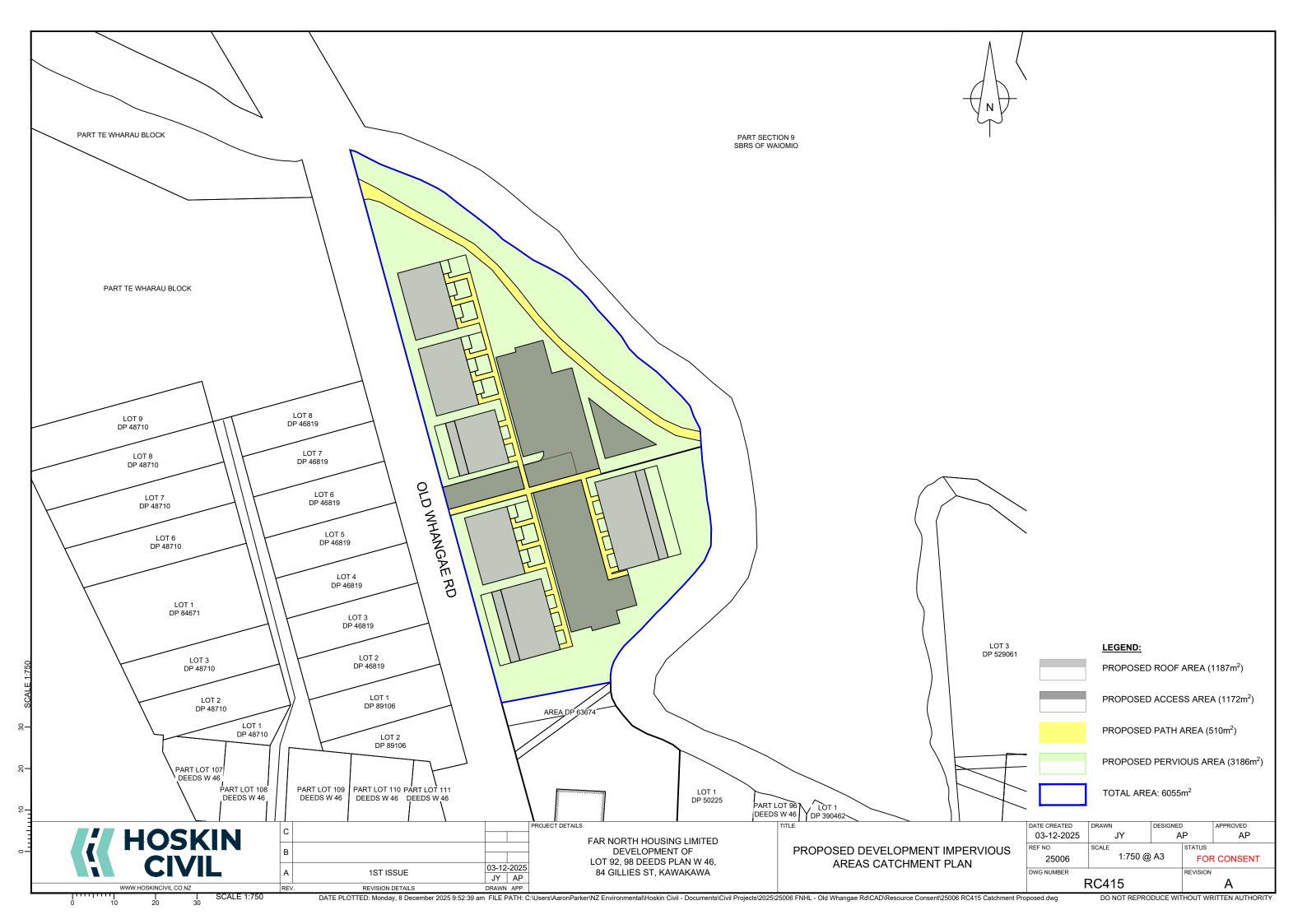


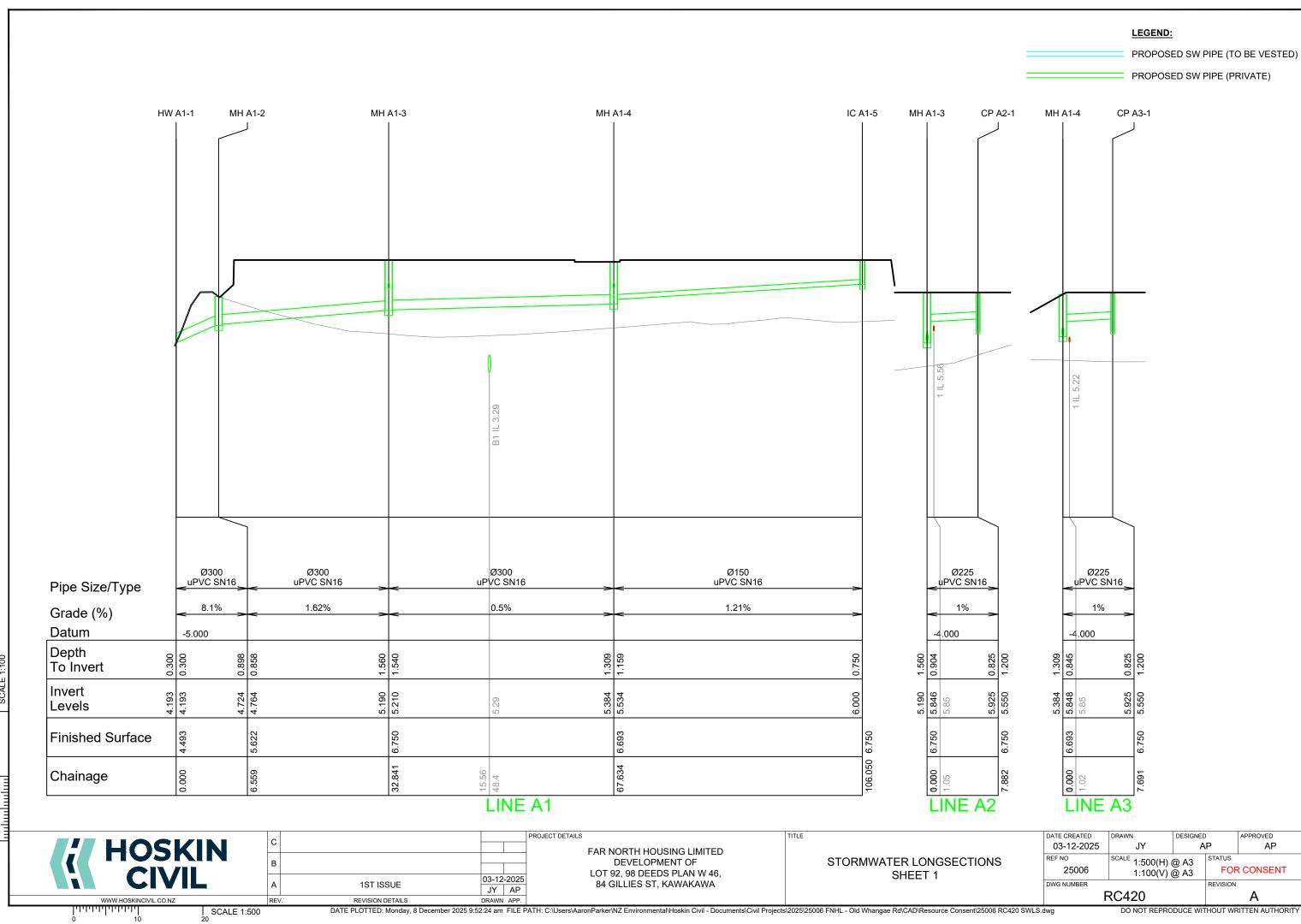


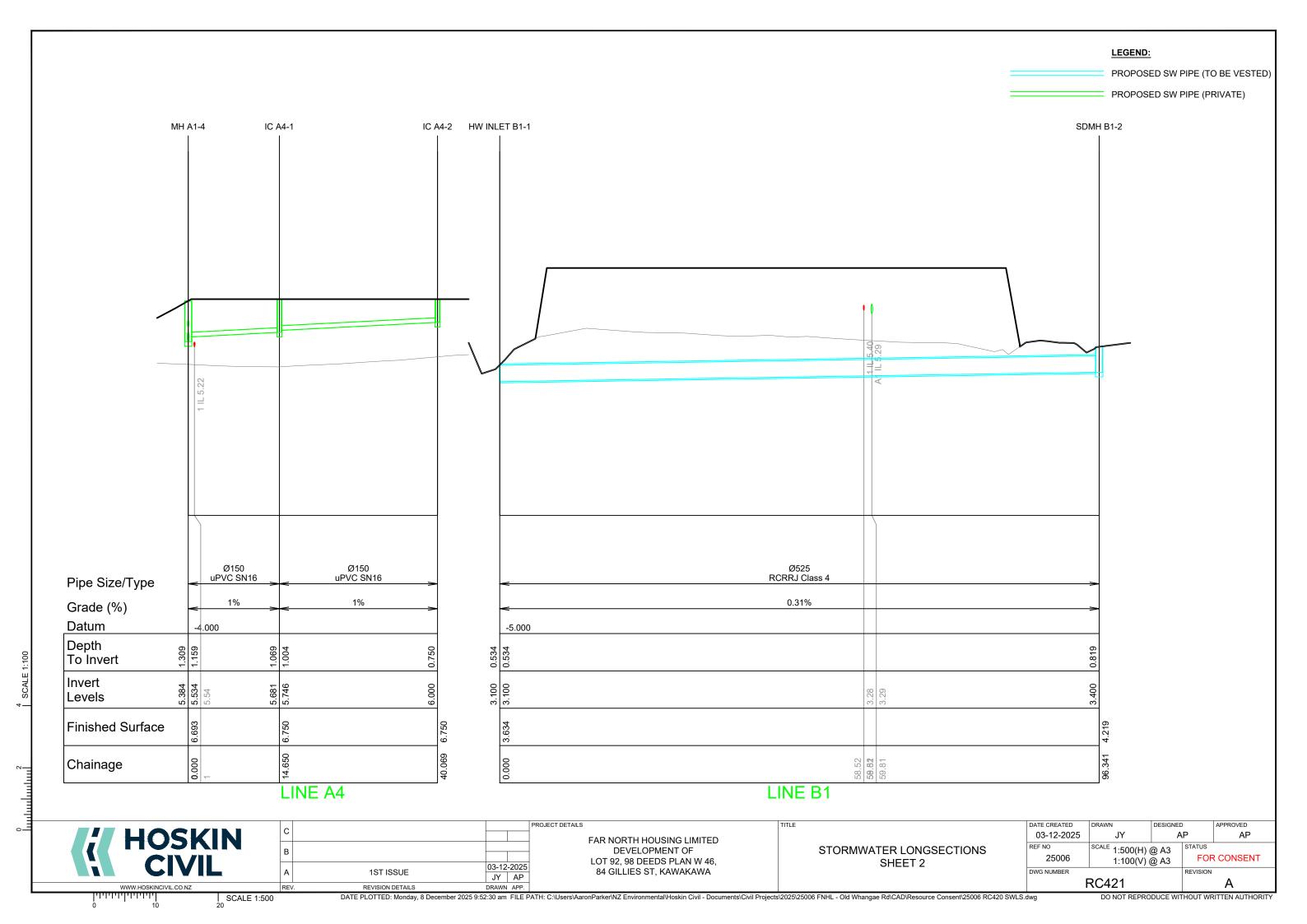






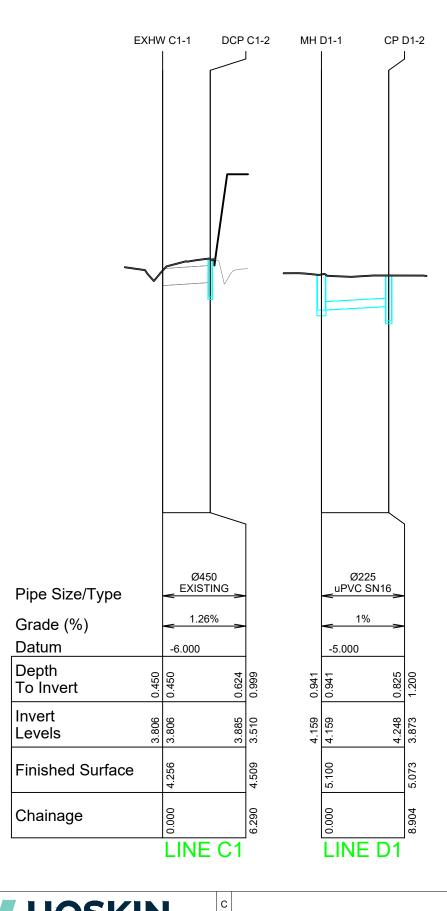






PROPOSED SW PIPE (TO BE VESTED)

PROPOSED SW PIPE (PRIVATE)



FAR NORTH HOUSING LIMITED DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46, 84 GILLIES ST, KAWAKAWA

03-12-2025

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STORMWATER LONGSECTIONS SHEET 3 | DATE CREATED | DRAWN | DESIGNED | APPROVED | APPROVED

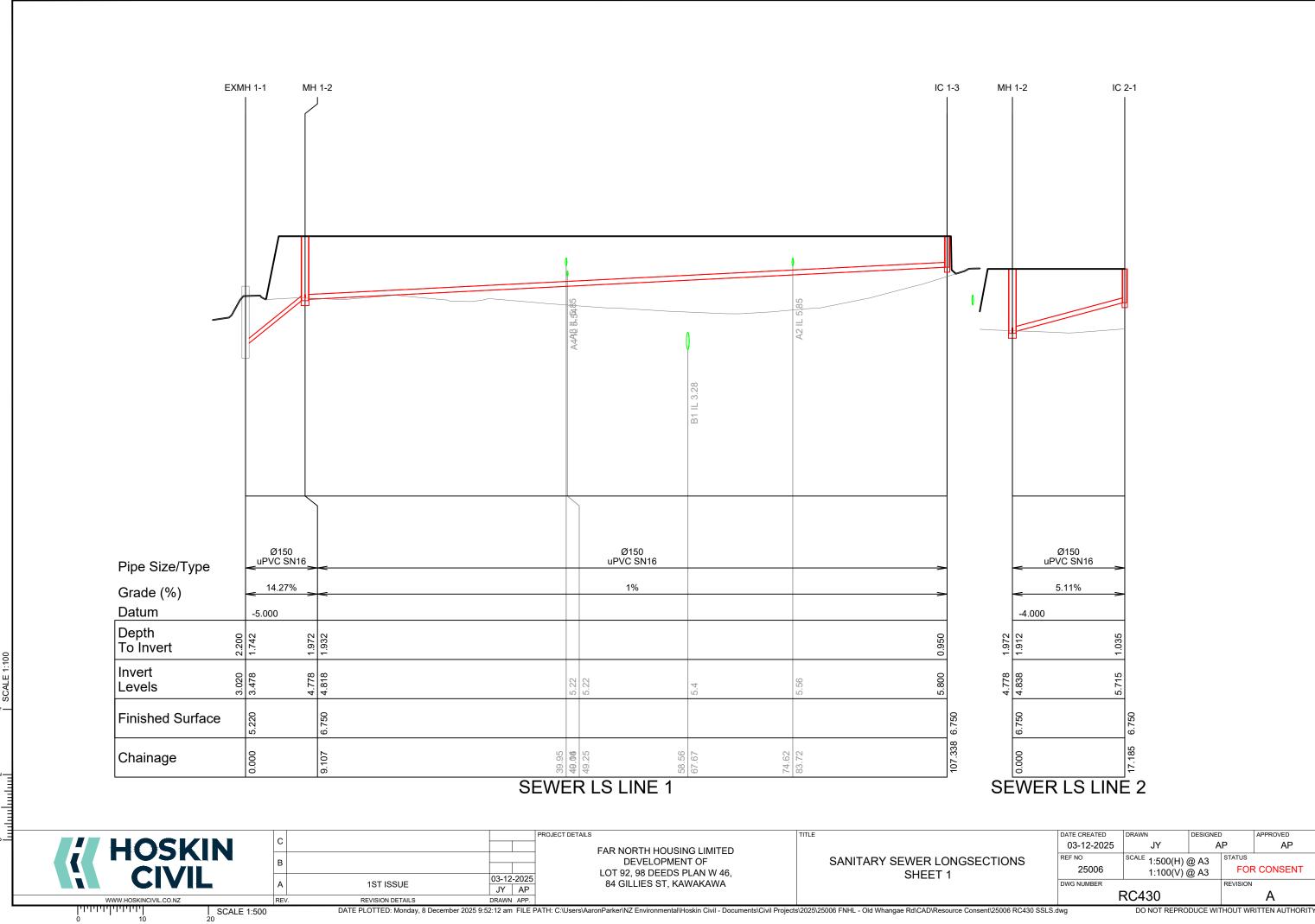
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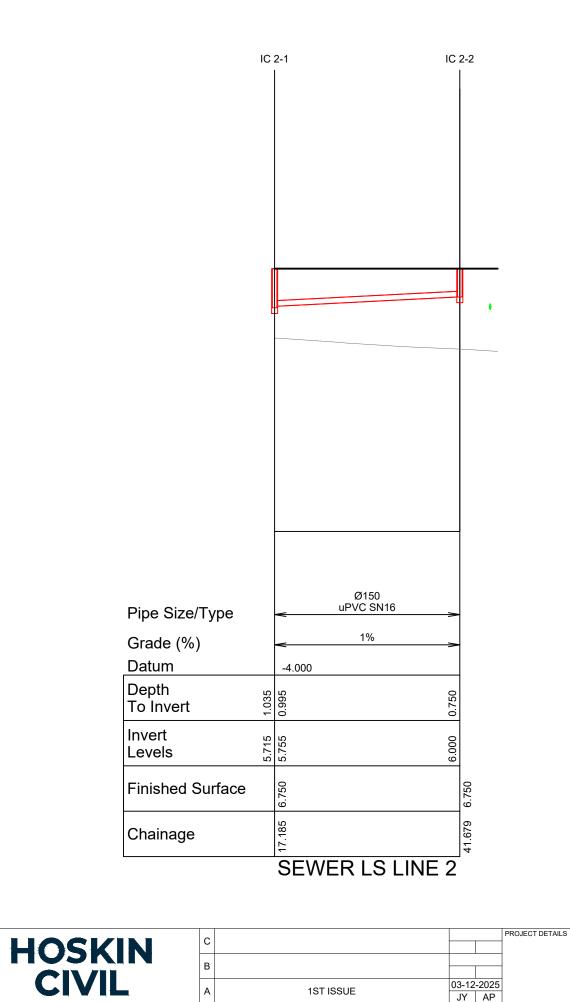
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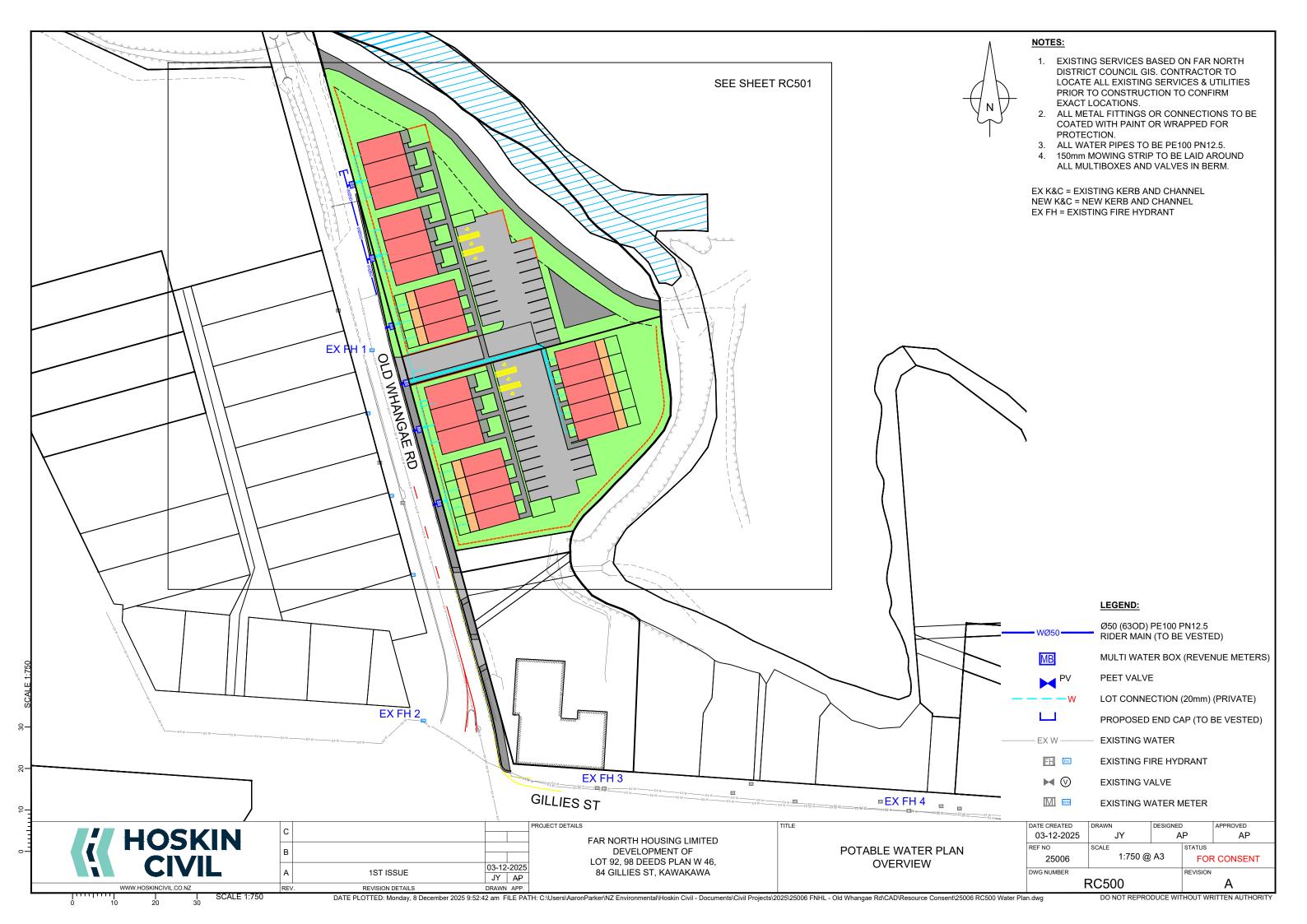
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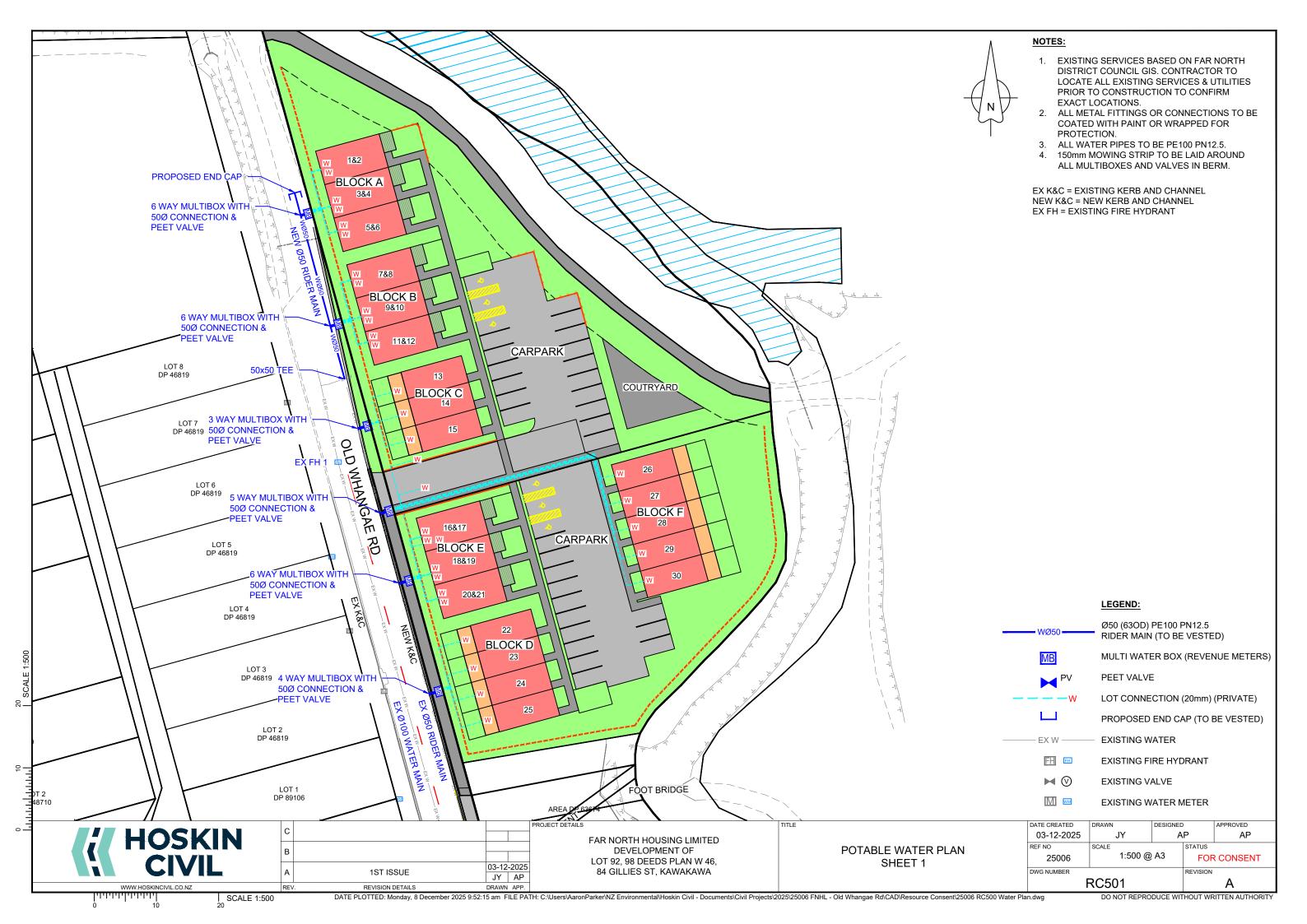
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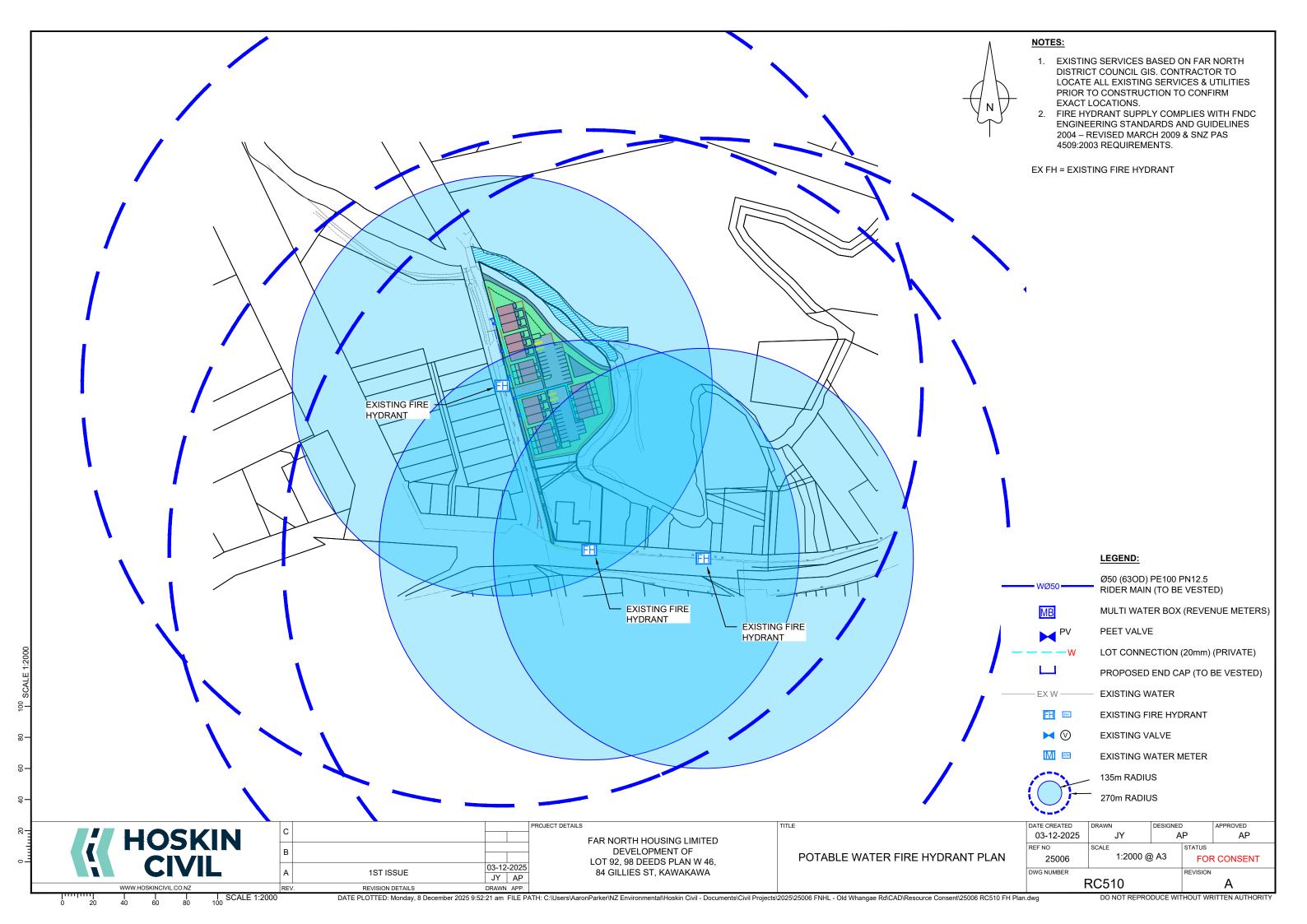
FAR NORTH HOUSING LIMITED

DEVELOPMENT OF LOT 92, 98 DEEDS PLAN W 46,

84 GILLIES ST, KAWAKAWA







Subject: DO NOT REPLY – Waka Kotahi NZ Transport Agency - A new Environmental Planning request has been

logged with Case Ref - Application-2025-1621 CRM:0093197409

Date: Monday, 1 December 2025 at 10:16:34 AM New Zealand Daylight Time

From: Environmental Planning

To: Steve Sanson

Dear Far North Holdings Limited,

Thank you for your application. Your reference number is:

Your application has been assigned to the Environmental Planning Team and you should expect to receive a response within the next 20 working days. If you have any further queries or concerns on this matter, please do not hesitate to contact us via email quoting case ref: Application-2025-1621 or visit our <u>website</u>.

Kind Regards,

# **Environmental Planning Team**

System Design and Delivery

E environmentalplanning@nzta.govt.nz / w http://www.nzta.govt.nz

This message, together with any attachments, may contain information that is classified and/or subject to legal privilege. Any classification markings must be adhered to. If you are not the intended recipient, you must not peruse, disclose, disseminate, copy or use the message in any way. If you have received this message in error, please notify us immediately by return email and then destroy the original message. This communication may be accessed or retained by NZ Transport Agency Waka Kotahi for information assurance purposes.





Supporting our people

Private Bag 752, Kaikohe 0440, New Zealand
ask.us@findc.govt.nz
0 0800 920 029
findc.govt.nz

# Concept Development Meeting Minutes

Date: 16-Jul-2025 Concept Number: CDM-2026-1

Address: 84 Gillies Street, Kawakawa 0210

**Duration of Meeting:** 

# 1. Meeting Attendees

# Council:

- Nikki Callinan Senior Planner
- Nick Williamson- Team Leader, Resource Consents
- Rinku Mishra Senior Resource Consents Engineer

## Applicant:

• Steve Sanson - BayPlan

# 2. Proposal & Documents Submitted for CDM

The application includes plans referenced as A101 (Proposed Site Plan - Option 3) and A A002 (3D Perspectives), both prepared by eclipse architecture / Far North Holdings Limited and dated 19/06/2024, along with A A211 (Typical Floor Plans), also by eclipse architecture / Far North Holdings Limited, dated 20/02/2024

# 3. Detail of Proposal - as outlined by the applicant at the meeting

Steven Sanson provided an overview of the proposed 30-unit medium-density housing development at 84 Gillies Street, Kawakawa, as detailed in the submitted plans. The proposal includes a mix of one-bedroom and two-bedroom units, with associated carparking. Detailed that recent stop bank works had been completed by NRC.

# 4. Discussion - at the meeting

# Infrastructure Development Fund

 Infrastructure development fund - this funding will support road extensions and significant water infrastructure upgrades for an expected 300 houses. This site makes up a potential site that could be developed to add to the 300 houses

### **Planning**

 ODP Zoning vs. PDP Zoning: Clarification sought on the implications of the Operative District Plan (ODP) zoning versus the Proposed District Plan (PDP) zoning for the site.

The existing site under the ODP is zoned Rural Production. However, it was noted that the site is cut off from wider farmland and rural use, sitting by itself opposite an industrial area. It was likely originally zoned this way to be low-zoned land and not highly developable for residential use. However, it will not be able to be used for rural purposes as it is not part of the wider farmland and is in close proximity to the main centre of Kawakawa and the industrial area which will be taken into consideration when assessing the proposal.

Under the PDP, the site is proposed to be zoned Mixed Use. The objectives of this zone were discussed, particularly that it is intended as a focal point for commercial, community, and civic activities, with residential development complementing these activities (MUZ-O2). It was noted that residential activity is typically encouraged above commercial activities to ensure active street frontages (MUZ-O5). The proposed development is entirely residential and does not include commercial components. It would be helpful to include an assessment of market demand with the application that why the residential use of the site and not including commercial aligns with the Mixed Use Zone and does not detract from the commercial focus of the Zone especially with the proximity to the town centre.

It was acknowledged that the proposed development demonstrates a more aligned approach to the Mixed Use zone under the PDP than the existing Rural Production zone, and this will be taken into account when weighing the proposal for the planner's assessment.

## Factors about design:

- The Mixed Use zone also focuses on active street frontages. Given the 2m retaining wall and current lack of landscaping shown along the boundary, the proposed dwellings do not currently demonstrate the active street frontage intended by the zone, especially with the pedestrian frontage overlay on this site. As this street also connects to the cycle trail, it would be beneficial for the application to clearly demonstrate efforts to enhance connectivity and create a more active street frontage, including appropriate landscaping along the retaining wall.
- In the application would be good to see if lighting has been considered for safety in the car parks and also safety considerations such as CPTED for pedestrians walking to dwellings, do they all have to enter from the front of the site alongside the retaining walls or are rear doors closer to the carparking areas included?
- Are there communal rubbish areas and are these fenced and hidden or is each unit dealing with own rubbish where will this be put?
- The dwellings are opposite an industrial area, how will reverse sensitivity effects be
  dealt with, is there acoustic ventilation or other mitigation included for noise
  attenuation and the effects from the close proximity of the industrial area.

### **Engineering – Resource Consent Engineer**

- Roading
  - Access to SH- Consultation from NZTA will be required.
  - Shared Access: Compliance with EES Table 3.7 and section 3 (e.g., Width, formation & gradient). Road name required for 4+ users.
  - o Road to vest- Consultation with roading will be required.

 Parking Flooding: Is it acceptable for car parks to be underwater during a 100-year flood event? Emergency vehicle entrance for any flood emergency time.

#### Water

- Infrastructure engineer approval required. Yes, demonstrate capacity and Fire Fighting Supply (FFS) cover.
- Onsite supply? Borehole supply? Shared supply? Not required.

#### Wastewater

- Are council services available? Low pressure zone / gravity. Public or privately owned? Infrastructure engineer approval required.
- o If yes, demonstrate capacity in detail in the Site Suitability report.
- Any risk of infiltration or cross-connection with floodwater been accounted for, to avoid any mixing of Stormwater (SW) and Wastewater (WW).
- o Onsite services? [No information provided for this point in your text]

#### Stormwater

- Are council services available? Infrastructure engineer approval required. Yes for half area, demonstrate capacity. For half area, it's out of area of benefit.
- Attenuation to comply with Section 4 in the EES. [No information provided for this point in your text]
- Onsite disposal / Discharge Strategy: How is stormwater being managed to prevent adding to downstream flood risk? Can the full site comply with EES Section 4 attenuation requirements? Are treatment devices or detention needed on-site? How above the attenuation device required to be on site to prevent from any flooding impact?
- Floodplain Compensation: Has any modelling or volume calculation been done to ensure floodplain storage lost to building platforms is fully compensated elsewhere on the site?
- Impervious Surface Management: Will all paved areas (courtyards, driveways, car parks) be permeable or require on-site storage and treatment?

## Site Suitability/Geotechnical Reports

- Land Stability (Low/Medium/High)
  - Site Stability: What is the geotechnical classification of each zone across the site? (Noted as potentially medium hazard). Will CPEng supervision be required during earthworks? Will retaining walls along the flood embankments require special design?
  - Earthworks Volume: What is the estimated cut/fill balance for achieving flood mitigation and platform raising? Will NRC consent be required for bulk earthworks, and when should this be applied for?
- o All reports are to comply with Section 2 in the EES.

#### • Other (Flooding)

- Flooding / Flood Site Engineering Questions: Flood hazard assessment and model (HecRas or any similar software) - by CPEng.
  - Flood Impact: What are the confirmed flood depths for the 10-year and 100-year events across the site? What mitigation methods are acceptable to Council for displacement of floodwaters? How will floodwaters interact with the proposed batters and raised building platforms? What will be the effect of the block platform, how it will divert water to the other property? Can updated hydraulic modelling confirm whether

- floodwaters will affect downstream or adjacent properties? What are the velocity and depth thresholds for safe evacuation and do the current designs meet them?
- Finished Floor Levels: What is the required minimum freeboard above the 100-year flood level? Will raised floor levels trigger accessibility issues or additional retaining structures? Can car park areas be used in a flood event if buildings are raised? Are cars protected?
- Emergency Access: What are the expected flood depths and velocities on Old Whangae Road during a 100-year flood—can fire and ambulance vehicles access the site? Has a functional emergency evacuation route been identified? Is there a need for an elevated internal driveway or an emergency exit route elevated above flood levels?

# Engineer - IAM

#### Wastewater

- A capacity assessment for both water and wastewater will need to be provided to confirm the current system will be able to accommodate the additional demand from the development.
- In the case that an upgrade is required to accommodate the additional demand, all upgrades will be at the cost of the applicant and a Development Agreement will need to be put in place to account for this.

# Water

Hydrant testing will be required to confirm capacity.

#### Stormwater

• Stormwater connection to Council's reticulated system is only available for the southern most units (3 X 1 Beds).

# **Reserves Planner**

An esplanade waiver would be required to be approved or esplanade reserve may be provided.

(iii) where any land use requires a resource consent for an activity or activities and the Council considers it necessary to require an esplanade reserve or strip for any of the purposes outlined in s229 of the Act, an esplanade reserve or strip may be required;



# 5. Conclusion and Next Steps

 Include all necessary supporting technical reports, such as a detailed Assessment of Environmental Effects (AEE), potentially a Market Demand Assessment, Traffic Impact Assessment (TIA), Stormwater Management Plan (SWMP), Geotechnical Report, and a Flood Hazard Assessment and Model.

### **Please Note:**

The views and opinions by Council Officers at the Concept Development Meetings and in these associated notes provide their preliminary view only. A final determination on whether Council can support the consent or not, and whether the resource consent application will be processed on a notified or non-notified base can only be made upon receipt of a formal application, site visit and review.



Chorus NZ Ltd 4 Graham Street Auckland CBD Auckland

Adrian Tonks Far North Holdings Limited 5449A State Highway 12 Kaikohe, 0472

01/12/2025

Hi Adrian,

Thank you for providing an indication of your development plans in the Kawakawa area. I can confirm that we have infrastructure in the general land area that you are proposing to develop at 84 Gillies Street, Kawakawa (Old Whangae Road). Chorus will be able to extend our network to provide connection availability. However, please note that this undertaking would of course be subject to Chorus understanding the final total property connections that we would be providing, roll-out of property releases/dates and what investment may or may not be required from yourselves and Chorus to deliver the infrastructure to and throughout the site in as seamless and practical way as possible.

The cost can only be finalised at the time that you are ready to proceed.

Chorus is happy to work with you on this project as the network infrastructure provider of choice. What this ultimately means is that the end customers (business and homeowners) will have their choice of any retail service providers to take their end use services from once we work with you to provide the physical infrastructure.

Please reapply with a detailed site plan once you are ready to proceed.

Kind Regards,

Merita Tagaloa Group Account Manager

Chorus NZ Ltd





Top Energy Limited

Level 2, John Butler Centre 60 Kerikeri Road P O Box 43 Kerikeri 0245 New Zealand PH +64 (0)9 401 5440 FAX +64 (0)9 407 0611

28 November 2025

Far North Housing Ltd PO Box 7 Opua 0241

Dear Sir / Madam

# RE: Proposed new connection – 84 Gillies Ave, Kawakawa Top Energy Reference 109189

Thank you for your application for a new connection at the above address. We have reviewed your application against our records and found that the current network arrangement cannot meet the needs of your application without an upgrade, extension, or alteration to the network.

Any upgrade, extension or alteration to the network requires an engineering design to identify a suitable solution and ensure that the work complies with the Top Energy standards and Electricity Regulations, which ensures that it is fit for purpose, safe and compliant.

The design shall allow for the required lines/cables and equipment to provide a suitable fused service connection point at or near the boundary of the above property, or at a location as agreed. The design shall be based on the capacity requested in your application.

Top Energy offer a design service and our quotation to provide a detailed engineering design solution for the preliminary proposal below is \$2,200, excluding GST.

Due to current workload and job complexity, we estimate the detailed design to take 12-14 weeks to produce. Should you engage Top Energy to undertake the design one of our staff will contact you and, if required, arrange a site meeting to discuss the design options. Once the design is completed a fixed price quotation will be prepared for the construction work.

If you wish to engage Top Energy to carry out the detailed engineering design for the above reticulation proposal, please contact our Estimating Team on 0800 867 363 or by email at <a href="mailto:ciw@topenergy.co.nz">ciw@topenergy.co.nz</a> who will issue an invoice for the quoted amount.

#### **Term and Conditions**

Our design quotation is firm for 30 days from the date of this letter. Our normal terms are payment in full prior to material procurement and commencement of work.

**Preliminary design proposal** (subject to detailed design investigation):

- Review the existing transformer T04015 and, if required, upgrade to provide the capacity requested in the application
- Extend approx. 100m of low voltage underground cable from the above transformer to a new fused service connection pillar on the roadside boundary of lot 1 and lot 2
- Provide for a 3 phase 160 amp per phase fuse connection point per lot at the above pillar.

An estimate for the above proposed works is between \$100,000 & \$120,000 (GST exclusive)

### Ownership

Top Energy will retain ownership of the new lines/cable, transformer and associated equipment up to and including the fuse service connection pillars and therefore undertake the required inspection and maintenance tasks as required by the Electricity Regulations.

Should no reply be received within 90 days this job will be closed. A new application fee will be required after the job is closed.

If you have any queries or wish to discuss the proposal further, please contact our Estimating Team on 0800 867 363.

Regards
Top Energy Estimating Team